# INDEX OF SHEETS

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 SIGNATURE SEAL



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### 10' Lt. Sta. 4715+27.54 REHABILITATE KTA Bridge No. 43.930 SB 30.3'-50.1'-50.5'-29.9', Weathering Steel Beam Composite, Continuous (WMCC) 40°36'39" Skew Lt., 42'-6" Roadway

### Sta. 4712+30.00 BEGIN KTA Proj. 8082

# DESIGN DESIGNATION

AADT (2022)	=	14,300
AADT (2042)	=	25,800
D	=	50%
Т	=	26%
V	=	75 MPH
C of A	=	Full
Clear Zone	=	46'

### CONVENTIONAL SIGNS

COUNTY LINE	CENTER LINE OF PROJECT	50	
CITY LIMITS	TERRACE		
STATE OR NATIONAL LINE	CULVERTS		$\equiv$
TOWNSHIP, SECTION or GRANT LINE	DROP INLET & STORM SEWER		
PROPERTY LINE	ACCESS CONTROL		
HIGHWAY FENCE	POWER POLE		
EXISTING FENCE	TELEPHONE POLE		
GUARDRAIL	MARSH		
CONSTRUCTION LIMITS	HEDGE		
RIGHT OF WAY LINE	TREES	9 A) A)	1172.18
TRAVELED WAY	PROFILE ELEVATION	$\sim$ $\sim$ $\sim$	117
RAILROADS	STREAM or CREEK		

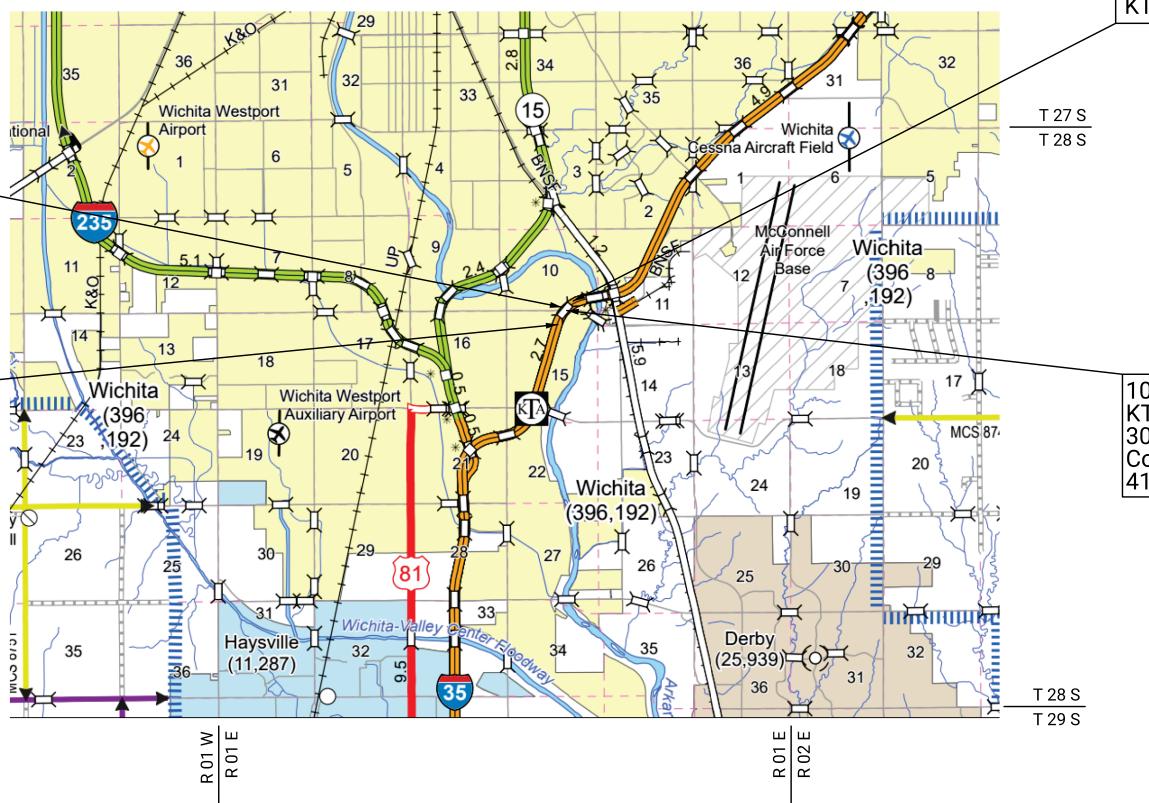
		_
	ВҮ	DATE
SURVEY	CLEVENGER - GARVER	2024
CADD TECHNICIAN	BROUILLETTE - GARVER	2024
DESIGNERS	ALBRITTON/NIEBAUM - GARVER	2024
SQUAD		

Plotted by : JEHarris 13-SEP-2024 File : 2302047rti-01.dgn

28

Ц С

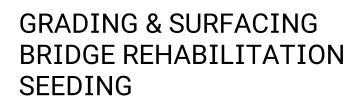
# Kansas Turnpike Authority Contract No. 8082 Sedgwick County, Kansas Bridge No. 43.930 Re-Deck & Widen

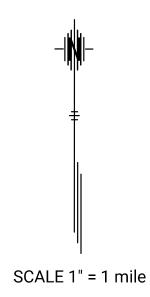


NET LENGTH OF PROJECT650.00FT.0.123MILESNET LENGTH OF BRIDGES158.62FT.0.030MILESNET LENGTH OF ROAD344.65FT.0.093MILES

STATE	PROJECT NO.	YEAR	SHEET NO.	TOTAL SHEETS
KANSAS	8082	2024	1	134
K	ANSAS TURNPIKE AUTHORI	ΓY		

CONTRACT NO. 8082





Sta. 4718+80.00 END KTA Proj. 8082

10' Rt. Sta. 4715+66.11 REHABILITATE KTA Bridge No. 43.930 NB 30.8'-51.3'-51.4'-30.4', Weathering Steel Beam Composite, Continuous (WMCC) 41°46'12" Skew Lt., 42'-6" Roadway

> NOTE: TRAFFIC TO BE CARRIED THROUGH PHASED CONSTRUCTION.

David E. Jacobson, P.E. Director of Engineering Kansas Turnpike Authority

<u>09/16/2024</u> Date

																				STATE	PROJECT	NO. YE	EAR SHEET NO.
																				KANSAS	8082	20	024 29
										SUMI	MARY OF Q	UANTITIES											
Item	Class III Excavation		crete (Grade 4.0) (AE)		ing Steel (Grade 60) (Epoxy Coated)	Structui (A709) (Grade 50W)	ral Steel (M270) (Grade 50WT 3)	Welded Stud Shear Connectors	Bearing (Steel Reinforced Elastomeric)		(Steel) (HPI4xI02)	Test Piles (HPI2x53)		Cast Steel Pile Points	Bridge Deck Grooving	Abutment Strip Drain	Bridge Backwall Protection System	Flowable Fill (High Strength)	Drilling and Grouting	Slope Protection Removal and Replacement	Temporary Shoring	Environmental Protection	l Falsework Inspection
Location	Cu. Yds.	Cu. Yds.	Cu. Yds.	Lbs.	Lbs.	Lbs.	Lbs.	Each	Each	Lin. Ft.	Lin. Ft.	Lin. Ft.	Lin. Ft.	Each	Sq. Yds.	Sq. Yds.	Sq. Yds.	Cu. Yds.	Each	Sq. Yds.	Lump Sum	Lump Sum	Lump Sur
Abutment No. /	/59./	**	38.2		3 <b>,</b> 437*					106.0				2		50.5	55.7	88.8		3/			
Pier No. I			7.4	933					2		105.0			2					12				
Pier No. 2	17.3		/3.7	1,294					2		52.0		59.0	2					20				
Pier No. 3			7.5	933					2		101.0			2					12				
Abutment No. 2	176.2	**	41.6		3,879*					48.0		58.0		2		55.1	63.2	97.1		30			
Substr. Total	349.0		108.4	2,227	7,3/6				6	154.0	258.0	58.0	59.0	10		105.6	//8.9	185.9	44	6/			
Superstr. Total		299.5			73,869	6,538	62,717	5,820							719.2								
Total	349	299.5	108.4	2,230	81,190	6,540	62,720	5,820	6	154 <del>†</del>	258 ††	58	59	10	719	106	119	185.9	44	61	Lump Sum	Lump Sum	Lump Sui
Abutment No. 1	/59./	**	40.7		3,693*					52.0		62.0		2		49.0	60.7	88.5		26			
Pier No. I			7.9	949					2		105.0			2					12				
Pier No. 2	17.3		4.	1,310					2		51.0		64.0	2					20				
Pier No. 3			7.9	949					2		105.0			2					12				
Abutment No. 2	169.4	**	42.6		3,930*					102.0				2		53.0	59.5	96.3		32			
Substr. Total	345.8		//3.2	2,259	7,623				6	154.0	261.0	62.0	64.0	10		102.0	120.2	184.8	44	58			
Superstr. Total		297.6			72,527	6,517	61,692	5,740							706.1								
Total	346	297.6	//3.2	2,260	80,150	6,520	61,690	5,740	6	154 👁	261 🔊 🔊	62	64	10	706	102	120	184.8	44	58	Lump Sum	Lump Sum	Lump Sui

\* Reinforcing steel placed in the abutment above the construction joint is included in the superstructure total quantity.

\*\* Quantities are included in the superstructure total quantity.

Plotted By: JEHarris	Plot Location:
Plot Date: 12-SEP-2024 21:34	

INDEX OF BRIDGE DRAWINGS					
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29		Bridge Quantities, Index & General Notes			
30		General Notes			
31		Construction Sequence Details			
N.B.	S.B.				
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		Standards			
86		Bridge Excavation			
87		Standard Pile Details			
88		Supports and Spacers for Reinforcing Steel			

LFD RATING FACTORS					
Location	Ro Truck	ating Level	Inventory	Operating	
N.B. Bridge	HS-20	(36T)	2.31	3.86	
N.D. DI luge	Type HET	( <i>110</i> T)	$\left \right\rangle$	2.01	
S.B. Bridge	HS-20	(36T)	2.39	3.99	
S.D. DITUye	Type HET	( <i>110</i> T)	$\left  \right\rangle$	2.07	
2002 LFD Rating. 17th Edition AASHTO					

L
N.2
S.I

*† This includes 2 @ 53' and 1 @ 48'.* 

- *tt This includes I @ 54', 2 @ 52', I @ 51' and I @ 49'.*
- 🕲 This includes I @ 52' and 2 @ 51'.
- $\mathfrak{SS}$  This includes 2 @ 54' and 3 @ 51'.

TRAFFIC [	ATA
(Br. No. 43.930	NB & SB)
AADT (2022)	14,300
AADT (2042)	25,800
D	50%
Τ	26%

(					
	LRFR RATING FACT	ORS			
Location	Rating Level	Inventory	Operating		
N.B. Bridge	HL–93 Loading	2.41	3./3		
S.B. Bridge	HL–93 Loading	2.46	3.20		
2018 Manual for Bridge Evaluation					

# DESIGN DATA

DESIGN SPECIFICATIONS: AASHTO LRFD Bridge Design Specifications, 9th Edition (2020).

ORIGINAL DESIGN SPECIFICATIONS: AASHO Specifications, 1953 Edition.

DESIGN LOADING: HL-93

> Design Dead Load includes an allowance of 15 psf for a future wearing surface.

UNIT STRESSES: Concrete (Grade 4.0)(AE)(SA)(MPC) f'c = 4 ksi Concrete (Grade 4.0)(AE) f'c = 4 ksi fy = 60 ksi Reinforcing Steel (Grade 60) Structural Steel (A709 Gr. 50W)  $Fy = 50 \ ksi$ Structural Steel (M270 Gr. 50WT3) Fy = 50 ksi Steel Piles (Grade 50)  $Fy = 50 \ ksi$ Existing Structural Steel (A373–54T) fy = 33 ksi Existing Concrete f'c = 3 ksi Existing Reinforcing Steel fy = 40 ksi Existing Steel Pile fy = 33 ksi

LRFD DESIGN PILE LOAD:

Pile Loads are factored and are given in t

N.B. BRIDGE	<u>Strength I</u>	<u>Service</u>
Abutments	50	36
Piers	143	96
S.B. BRIDGE	<u>Strength I</u>	<u>Service</u>
Abutments	50	36
Piers	43	96

# GENERAL NOTES

CONCRETE: Superstructure concrete is bid as Concrete (Grade 4.0) (AE)(SA)(MPC). Substructure concrete is bid as Concrete (Grade 4.0)(AE). Bevel all exposed edges of all concrete with a  $\frac{3}{4}$ " triangular molding, except as otherwise noted on the plans.

REINFORCING STEEL: All reinforcing steel dimensions are to the centerline of bars unless otherwise noted. All reinforcing steel shall conform to the requirements of ASTM A615, Grade 60.

DIMENSIONS: All dimensions shown on the design plans are horizontal dimensions unless otherwise noted. The Contractor shall make necessary allowances for roadway grade and cross slope.

TEMPERATURE: The design temperature for all dimensions is 60°F.

QUANTITIES: Items not listed separately in the Summary of Quantities are <u>subsidiary</u> to other items in the proposal.

CONTRACTOR CONSTRUCTION STAKING: Contractor Construction Staking for clear span bridges requires two independent surveys. See KDOT Specifications.

TONS.							
		4					
ervice I	<u>Phi</u>	3					
		2					
36	0.65	I					
96	0.65	NO.	DATE		REVISIONS	BY	APP'D
<u>ervice I</u> 36 96	<u>Phi</u> 0.65 0.65		No. 43.	.930 BRIDGE QI	URNPIKE AUTHO JANTITIES, INDE IERAL NOTES		
		SHEET		SCALE		1	
		DESIG		DETAILED	JTK QUANTITIES	CADD	
		DESIG	<u>N CK.</u>	DETAIL CK.	JMB QUAN. CK.	CADD CK	<u>(.                                    </u>

	EXISTING STRUCTURE: Plans of the existing structure are on file and available for inspection by qualified bidders at the KTA.	PILING: Drive all p shall stop whe damage the p
	EXISTING DIMENSION VERIFICATION: Dimensions of the existing structure are based on old plans. Verify, by field measurement, the as-built dimensions of the existing structure and submit such verification in writing to the Engineer. The verification will include sketches, drawings, photographs and descriptions that will be	of 50 tons and As a minimum case shall the Formula Drive
	incorporated in the new construction. REMOVAL OF EXISTING STRUCTURE:The roadway bid item "Removal of Existing Structure", Lump Sum, includes the removal of the	experienced, p Load occurs may request ti
	concrete deck, barriers, and abutments as shown on the plans. Clearly mark the location of the existing beam top flanges on top of the existing deck concrete. Mark the entire length of all beams before sawing or removing any concrete. Concrete sawing shall be limited to a maximum depth of 3 inches directly above any beam and within 3 inches of either edge of a beam top flange. Do not	TEST PILE SPEC the Engineer/ Analyzer (PD, Specifications piling, Drive f Strength I loa
	use drop-type pavement breakers. Do not use a hoe ram directly above any beam or within I'-O" of either edge of a beam top flange. Use a jackhammer no heavier than 15 lb. to remove concrete above and within I'-O" of either side of a beam top flange.	PILING SPLICE L criteria for th Sheet (BRIIO)
	Damage to the existing structural steel caused by procedures not conforming to the above requirements shall be repaired as directed by the Engineer at the Contractor's expense (no cost to the KTA). Any costs incurred for testing or Engineering evaluations will be	CAST STEEL PIL shall be a one the pile as sp for pile point
	included in the Contractor's expense for repair. All materials removed from the existing structure shall become the property of the Contractor and removed from the site.	TEMPORARY SHO labor and mai <u>the temporary</u> supporting of
	DEMOLITION PLANS: This is a Category C Demolition. Submit detailed Demolition Plans to the KTA at least <u>4 weeks</u> before the beginning of the demolition process. Portions of the submitted details shall bear the seal of a Licensed Professional Engineer. Identify, on the plans, the Demolition Supervisor meeting the requirements of the KDOT Specifications. The Demolition Supervisor will attend the required pre-demolition meeting before these operations begin, as described in KDOT Specifications. No Demolition work will begin without approved Demolition Plans.	<u>bridge.</u> The s or lowering the the bottom fla provided by the Engineer auth be designed of Submit design for review 6 not begin unti
	BROKEN CONCRETE:Waste the broken concrete from the existing bridge on sites provided by the Contractor and approved by the Engineer. Protruding reinforcing in the broken concrete shall be cut off and removed. This work shall not be paid for directly but shall be <u>subsidiary</u> to other bid items of the contract.	FALSEWORK PLA System of un FALSEWORK PLA falsework det Professional E
	ENVIRONMENTAL PROTECTION: After concrete deck removal, the Contractor will test the remaining paint on the top flange for lead content. If necessary, use environmental protection procedures as shown in the KDOT Specifications. If required, the Environmental Protection Structure Classification is Class B.	105 of the Si KDOT Specifi FALSEWORK INSF which are cor falsework des
	TEMPORARY CONSTRUCTION LOADS: The Contractor will not stock pile construction materials, debris/rubble or place equipment weighing more than 20 tons or greater than bridge posted load limits on the bridge without prior written approval by the KTA Engineer. For	built falsewor compensation specifications DRILLING AND G
Plot Location: 35	bridges with highway traffic on or under the bridge the Contractor will provide plans showing the location, quantity and weight of the proposed materials, debris or equipment weighing more than 20 tons or greater than the posted load limits. These plans will bear the Seal of the Contractor's Engineer before approval is granted. The Contractor's Engineer will use AASHTO Specifications for limitations on structural capacities, as the structure is found in the field.	reinforcing s existing conc grout. Follow Special Provis mixing, applic incidentals ne each by the b
y: JEHarris 1-02-GenNotes.dgn : 12-SEP-2024 21:35	EMBANKMENT: Complete the embankment at the abutments as shown on the Bridge Excavation sheet prior to driving the abutment piling or commencing with the abutment footing excavation.	ABUTMENT STRI "Abutment Stri
By: JEHarris 44-02-GenNot e: 12-SEP-20	BACKFILL COMPACTION: Compact backfill at the abutments.	BRIDGE BACKWA
Plotted By File: KTA44 Plot Date:	BRIDGE EXCAVATION: All structural excavation shall be Class III. See the Bridge Excavation sheet for the limits of pay excavation.	BRIDGE DECK GI groove the de grooving shall
	SLOPE PROTECTION REMOVAL AND REPLACEMENT:This item shall consist of the removal and replacement of existing Slope Protection necessary to complete abutment construction. Furnishing all concrete, reinforcing steel and expansion joint filler material are <u>subsidiary</u> to the bid item, "Slope Protection Removal and Replacement". Replace	ANCHOR BOLTS: Specification exception:the
	Slope Protection to the existing limits and thicknesses or as directed by the Engineer.	CONSTRUCTION J the Contractor shown or at l

piling to bear in the Wellington Shale formation. Driving nen in the opinion of the Engineer additional driving may piling. Drive all piling to the Pile Driving Formula Load t the abutments and 143 tons at the piers.

m drive each pile to the load and penetration, but in no pile be driven to more than 110% of Pile Driving ing Load. At any location where problems are pile damage is suspected, or the Pile Driving Formula significantly above the design tip elevation, the Engineer that the Pile Driving Analyzer (PDA) equipment be used.

CIAL: Drive test pile special at the locations directed by Geologist or as shown on the plans. Use Pile Driving A) equipment and methods compliant with KDOT s. The test piling shall remain in place as permanent the test pile special piling to the resistance value of the ad divided by Phi shown on the plans.

OCATION: Integral pile splice locations and weld testing the abutments will follow the "Standard Pile Details"

LE POINTS: Pile points are required for all piles and e-piece unit of cast steel. Weld the cast steel pile point to pecified by the manufacturer. See KDOT Specifications requirements.

DRING: The bid item "Temporary Shoring" includes all aterial necessary to furnish shoring at the abutments for bracing of the embankment during excavation and the beam ends at the abutments during work on the shoring at the beam ends shall provide means of raising the beams to provide the required elevations. Stability of lange against twisting at the shoring location shall be the Contractor. Maintain the temporary shoring until the thorizes its removal. The temporary shoring plans are to and sealed by a registered Professional Engineer. calculations and shoring plans to the Field Engineer weeks before work is scheduled to begin. Work shall til the Engineer grants approval.

ANS AND SHOP DRAWINGS: Use the U.S. Customary nits on falsework plans and shop drawing details.

NS: A licensed Professional Engineer shall design the tails. Details shall bear the seal of a licensed Engineer. Submit electronic plans conforming to Section tandard Specifications with details in compliance with *fications to the Field Engineer for review.* 

PECTION: This project has falsework plan requirements nsidered "Category I" by KDOT specifications. The signer of record will conduct an inspection of the ask. The bid item, "Falsework Inspection" is full for all materials, labor and equipment. See KDOT

ROUTING: This item shall consist of arouting steel, anchor bolts, tie bars, or dowel bars into the crete, where required by the Engineer, with an epoxy w KDOT Specifications 842 and any associated isions. Follow the manufacturer's directions for cation and curing. The tools, materials, labor and ecessary to complete the work shall be paid for per bid item "Drilling and Grouting".

IP DRAIN: See the General Notes on the ip Drain" sheet.

LL PROTECTION SYSTEM: See the General Notes on t Strip Drain" sheet.

ROOVING: After the bridge deck has cured, transversely eck in accordance with KDOT Specifications. All II be perpendicular to the centerline of the bridge.

Anchor bolts will adhere to KDOT Standard Section 1600 (Grade 55) with the following threads may be rolled or cut.

JOINTS: The construction joints shown are optional with or. If used, place the construction joints only at locations locations approved by the Engineer.

- STRUCTURAL STEEL: The rolled beams and splice plates shall meet AASHTO M270 Gr. 50WT3 requirements. All other structural steel shall meet ASTM A709 Gr. 50W, unless noted otherwise. Shop and Field Splices shall be made only where shown on the Contract Plans as a "splice" or as an "optional splice". Elimination of any "splice" may be requested.
- FABRICATION OF FIELD SPLICES: Prepare joints for the field splices in accordance with KDOT Specifications. Use Type "B" shop laydown.
- WELDING: Material, Fabrication and Construction shall conform to KDOT Specifications. On the shop drawings, show a code or symbol in the tail of the weld symbol that refers to an approved, pre-qualified weld procedure.
- WELDED STUD SHEAR CONNECTORS: Weld Shear Stud Connectors with automatically timed stud welding equipment connected to a suitable power source. All stud welding shall conform to KDOT Specifications. Length of the Shear Stud Connectors to be attached to the existing beams in the field is based on theoretical fillet thickness. Revise the length of those Shear Stud Connectors as required to meet embedment requirements shown in the plans following calculation of actual fillet thickness.
- BOLTS: All bolts, nuts and hardened flat washers shall conform to the heavy hex structural requirements of ASTM F3125 Grade A325, Type 3, and KDOT Specifications unless otherwise noted. Direct Tension Indicators (DTIs) are to comply with the requirements of the latest edition of ASTM F959. No allowance will be made for high strength bolts used for permanent or temporary connections. This work is subsidiary to the bid item, "Structural Steel". The number of bolts is shown for the convenience of the Contractor.
- BOLTED CONNECTIONS: Beam Connections: Use  $\frac{7}{8}$  inch diameter heavy hex structural bolts for the main member connections. Use  $^{15}/_{16}$  inch diameter bolt holes. Do not ream during field erection. Accurately align all connections by driving  $^{15}/_{16}$  inch diameter drift pins in all corners and in  $\frac{1}{4}$  of the remaining holes in each plate. See KDOT Specifications.

Diaphragm Connections: Use  $\frac{7}{8}$  inch diameter heavy hex structural bolts for the secondary member connections. Use  $\frac{15}{16}$  inch diameter bolt holes. Oversized or slotted holes as specified in the KDOT Specifications, may be used in only one of the two members connected and must be shown in the approved shop drawings. Oversized or slotted holes may require additional standard hardened washers or plate washers. Report to the Engineer prior to any required field reaming that will remove more than 1/4 inch of material from one ply of the connected parts. Field drill holes in bolted bent plate (existing beam) for connection to new steel diaphragm.

Use Direct Tension Indicators (DTIs) on all high strength bolts. Place the DTI under the bolt head and turn the nut to tighten. This method is preferred whenever possible. Face the protrusions on the DTI to the underside of the bolt head. Place a hardened flat washer under the nut. See KDOT Specifications.

- ERECTION PLANS: This is a Category B Structure. Submit detailed Erection Plans to the KTA at least 4 weeks before beginning the erection process. Portions of the submitted details shall bear the seal of a licensed Professional Engineer. Identify, on the Erection Plans, the Erection Supervisor required by KDOT Specifications. No structural erection work will begin without approved erection plans.
- ERECTION ELEVATION CHECKS: Record existing top of beam elevations at *ℓ* bearing prior to demolishing abutments. After the abutment and pier concrete has cured and before setting any structural steel, present verification to the Engineer that the elevations at the bearings match plan elevation  $(\pm 1/4")$ .
- FILLETS: After the existing concrete deck has been removed and new beams placed, profile each beam. Construct the finished deck to plan grade by varying the depth of the fillet over the beam to provide for concrete dead load deflection. Correct any variation between the actual profile and the concrete dead load deflection shown in the plans by varying the depth of the concrete fillets over the beams so that the finished floor is constructed to the theoretical grade. The minimum depth of the deck over the beam shall be  $8^{1/2}$  inches.

The theoretical amount of concrete required for the fillets is 5.6 C.Y. for the NB Bridge and 7.6 C.Y. for the SB Bridge. This amount of concrete is included in the Summary of Quantities. Any additional concrete required to construct the fillets will be subsidiary.

STATE	PROJECT NO.	YEAR	SHEET NO.	TOTAL SHEETS
KANSAS	8082	2024	30	134

PAINTING OF EXISTING STRUCTURAL STEEL: Repaint the following existing structural steel in conformance with KDOT Specifications for "Repainting Steel Bridges - Change Paint System": top of girder top flanges, all surfaces of abutment diaphragms, and girder ends that will be embedded in new concrete.

Blast clean the tops of the top flanges to SSPC-SP6 Specifications (latest Revision) before the studs are applied. After the studs are applied, blast clean the tops of the top flanges and the studs to SSPC-SP6 Specifications and paint with an approved organic zinc primer to a minimum dry film thickness of 3 mils.

Existing structural steel embedded in new concrete shall be blast cleaned to SSPC-SP6 Specifications and painted with an approved organic zinc primer to a minimum dry film thickness of 3 mils.

Prepare and paint any areas of existing paint that are damaged during construction, including the pier piles and areas of the existing beams where new stiffeners are welded to the existing beams. The new paint system shall be an approved organic zinc primer with a waterborne acrylic finish coat. The finish coat will be Kansas Green. The color will match Federal Standard #24097.

All painting of the existing structural steel shall not be paid for directly but shall be <u>subsidiary</u> to other bid items.

PAINTING OF NEW WEATHERING STEEL: Blast clean all surfaces of all weathering steel, including all contact surfaces of bolted connections, to meet SSPC-SP6 Specifications (latest Revision). Blast clean to meet SSPC-SPI0 Specifications and prime coat the embedded portion of the beams, including the abutment diaphragms; the top flanges, including the shear studs; and the top flange splice plates. The shop and field coats shall conform to an inorganic zinc primer with a waterborne acrylic finish coat. The finish coat will be Kansas Brown. The color will match Federal Standard #20045.

PAINTING OF STEEL PILING: All exposed portions of new pier piling shall be painted with an approved organic zinc primer and a waterborne acrylic finish coat. The finish coat will be Kansas Green. The color will match Federal Standard #24097.

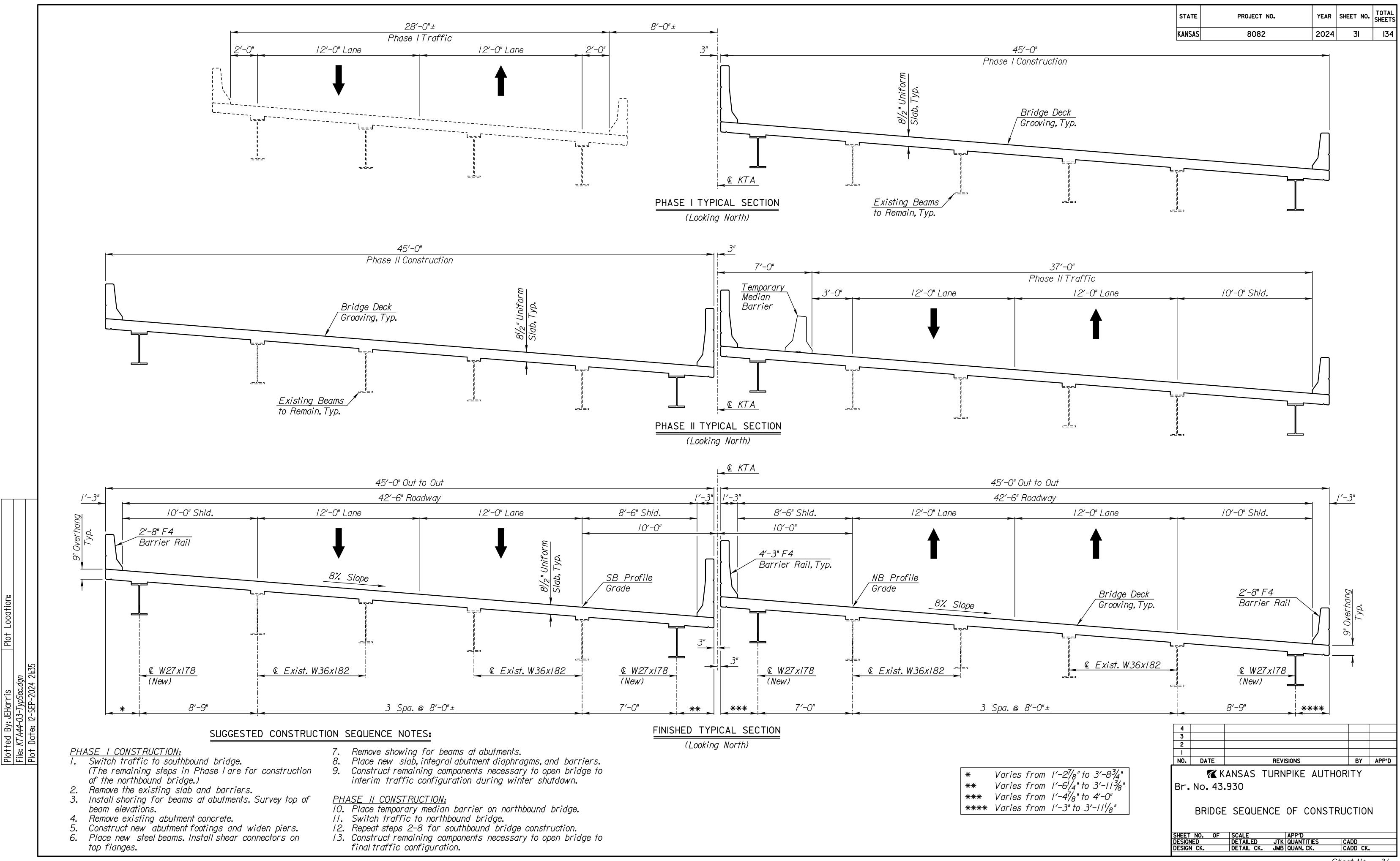
CONCRETE PLACING SEQUENCE: The sequence of placing concrete in the slab and curbs shall be as shown, or the Contractor may submit an alternate placing sequence for review. Submit the alternate placing sequence to the Engineer at the Preconstruction Conference. Include the proposed rate of concrete placement in C.Y./h, the plant capacity, placement direction, construction joint location, a description of the equipment used in placing the concrete, proposed admixtures, and the quantity of concrete in each placing segment. Any additional cost for the Contractor's alternate plan of placing concrete, including admixtures, shall be at the Contractor's expense and shall be considered <u>subsidiary</u> to the bid item, "Concrete (Grade 4.0)(AE) (SA)(MPC)". Approval of the Contractor's alternate sequence is required prior to placement of concrete in the deck.

Place and hand vibrate all concrete for the abutments above the existing footings to the bottom of the deck elevation just prior to the normal paving train operations. Do this work in a manner to avoid cold joints in either the slab or in the abutment.

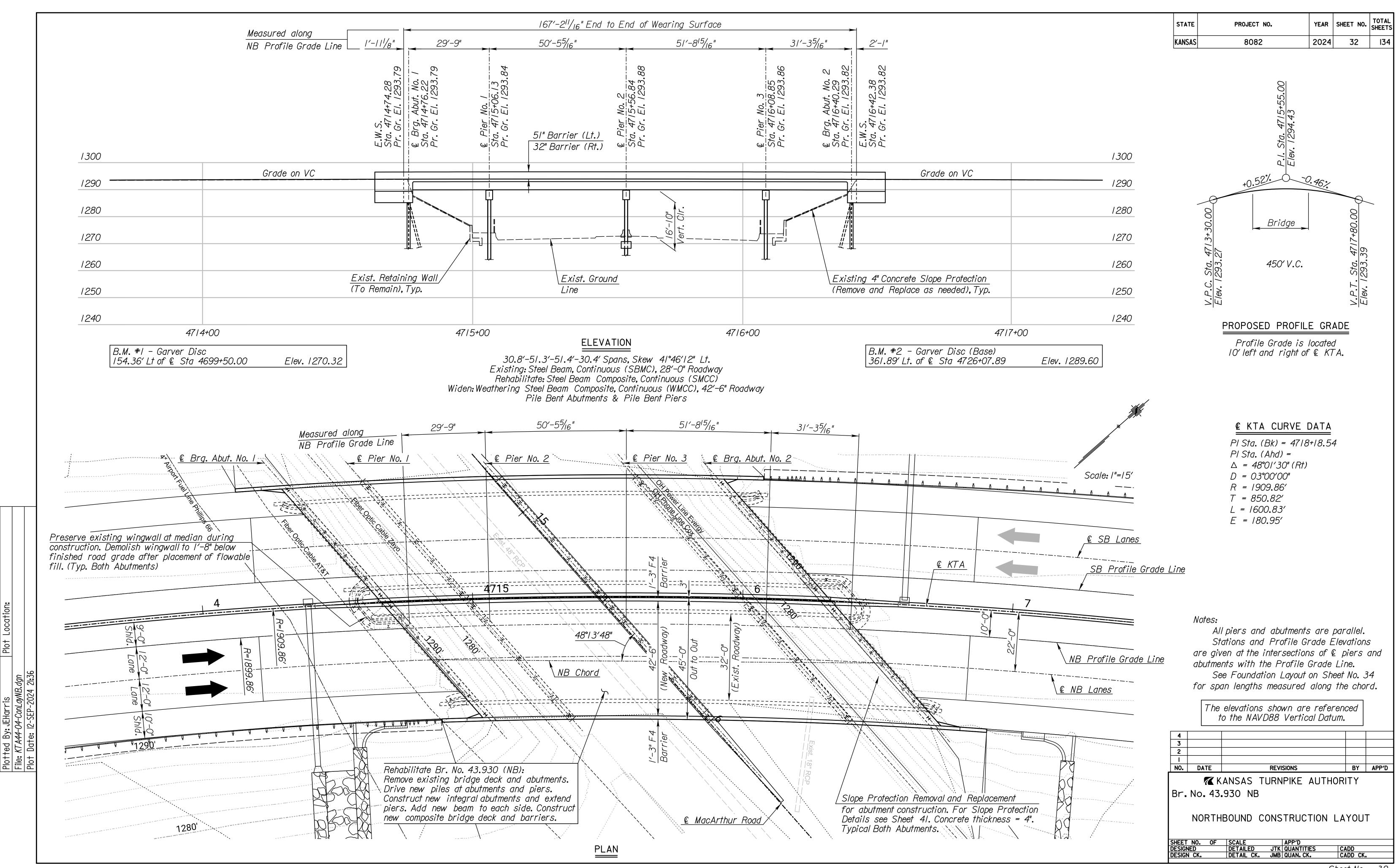
CONCRETE PLACING: At the Contractor's option, the finishing machine may be set normal to the centerline of the structure; however, the concrete must be placed along the skew. This requires placing concrete ahead of the finishing machine; consequently, a set retarder may be advisable. Note both requirements on any alternate placing sequence.

CONSTRUCTION LOADS: Limited traffic is permitted on the new deck during the curing period. Keep any exposed deck wet during the curing period. See KDOT Specifications Section 710 tables 710-1 and 710-2 for additional information.

APP'D									
NO. DATE REVISIONS BY APP'D KANSAS TURNPIKE AUTHORITY Br. No. 43.930 GENERAL NOTES									

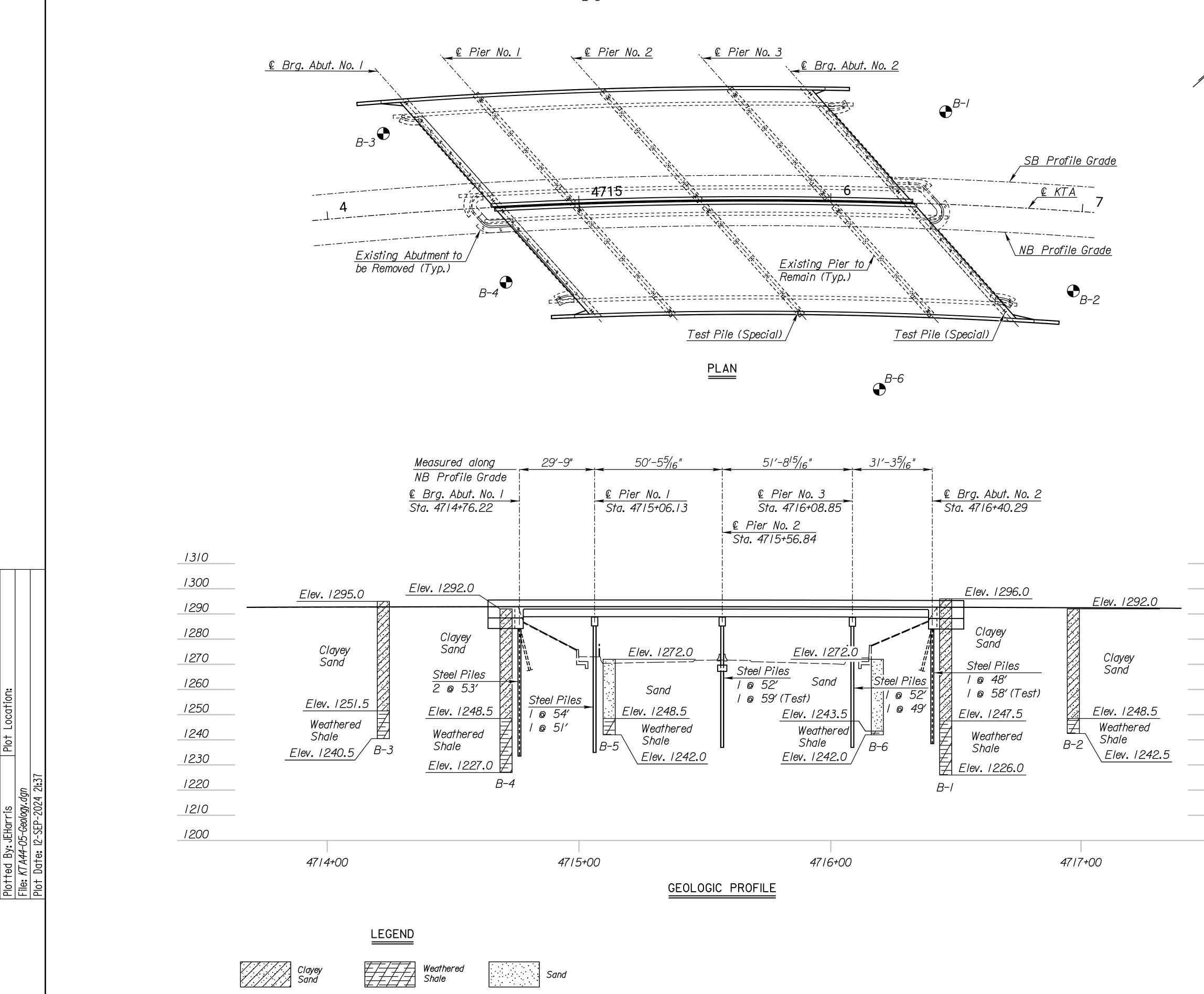


Sheet No. 3/



Sheet No. 32

• JZ





Location:

Plot

STATE	PROJECT NO.	YEAR	SHEET NO.	TOTAL SHEETS
KANSAS	8082	2024	33	134

### PILING:

Scale: /"=20'

HPI2x53 Piles shall be used at the abutments. HPI4xI02 Piles shall be used at the piers. All new piles shall use case steel pile points. All steel piles will be Grade 50.

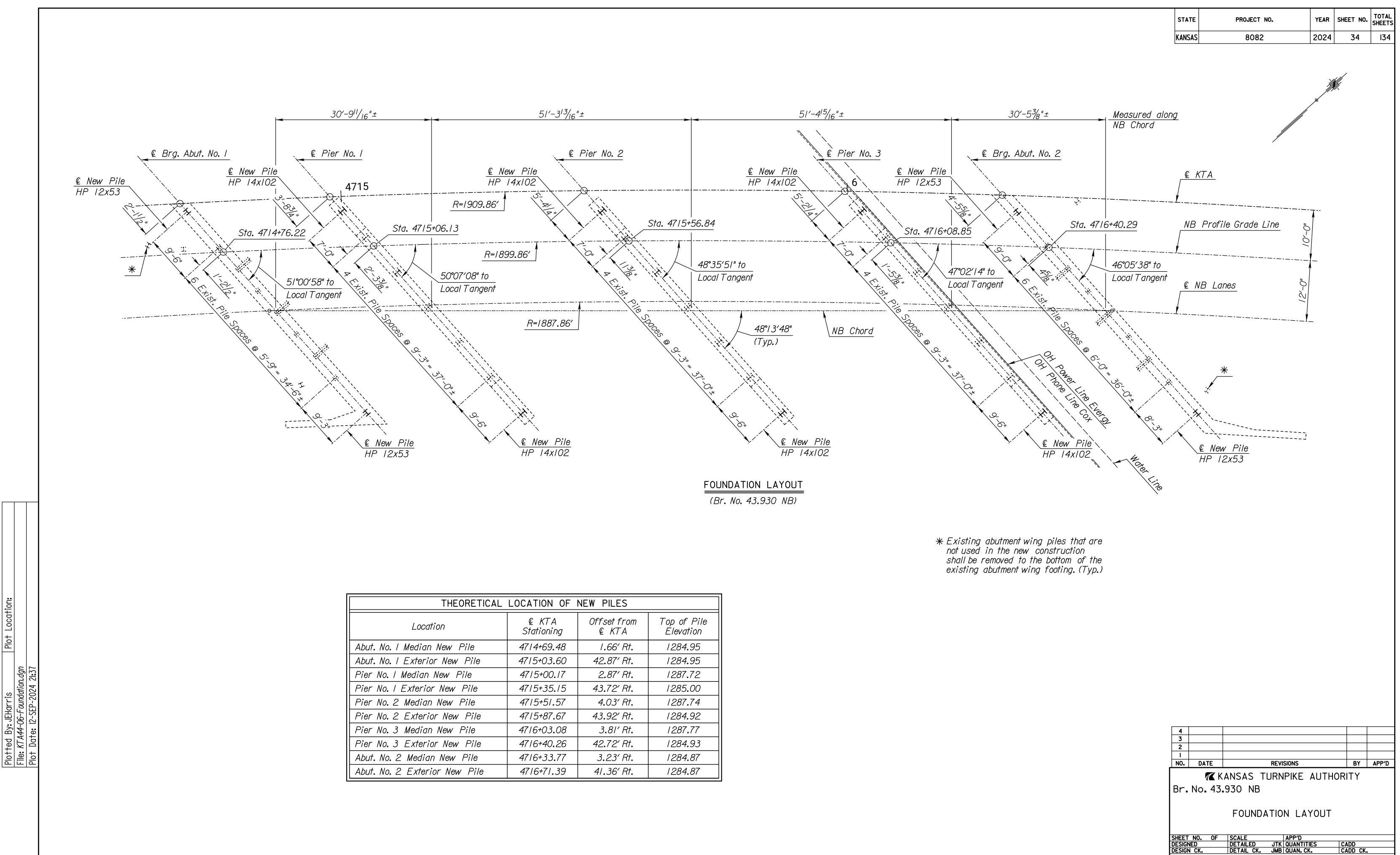
Drive all piling to penetrate the mantle and achieve bearing in the weathered shale. Once sufficient resistance and penetration into competent bedrock material are achieved, driving must cease to avoid damage to the pile. Final pile tip elevations should be determined in the field using resistance calculations.

TEST PILE (SPECIAL):

One Test Pile (Special) shall be driven at Pier No. 2 and Abutment No. 2 as shown. Test piles shall be driven prior to production piles and furnished IO feet longer than estimated tip elevations of the production piles shown in the plans. Test piles shall remain in place and be used as production piles. All restrikes should be performed a minimum of 24 hours after the initial advancement of the pile has ceased.

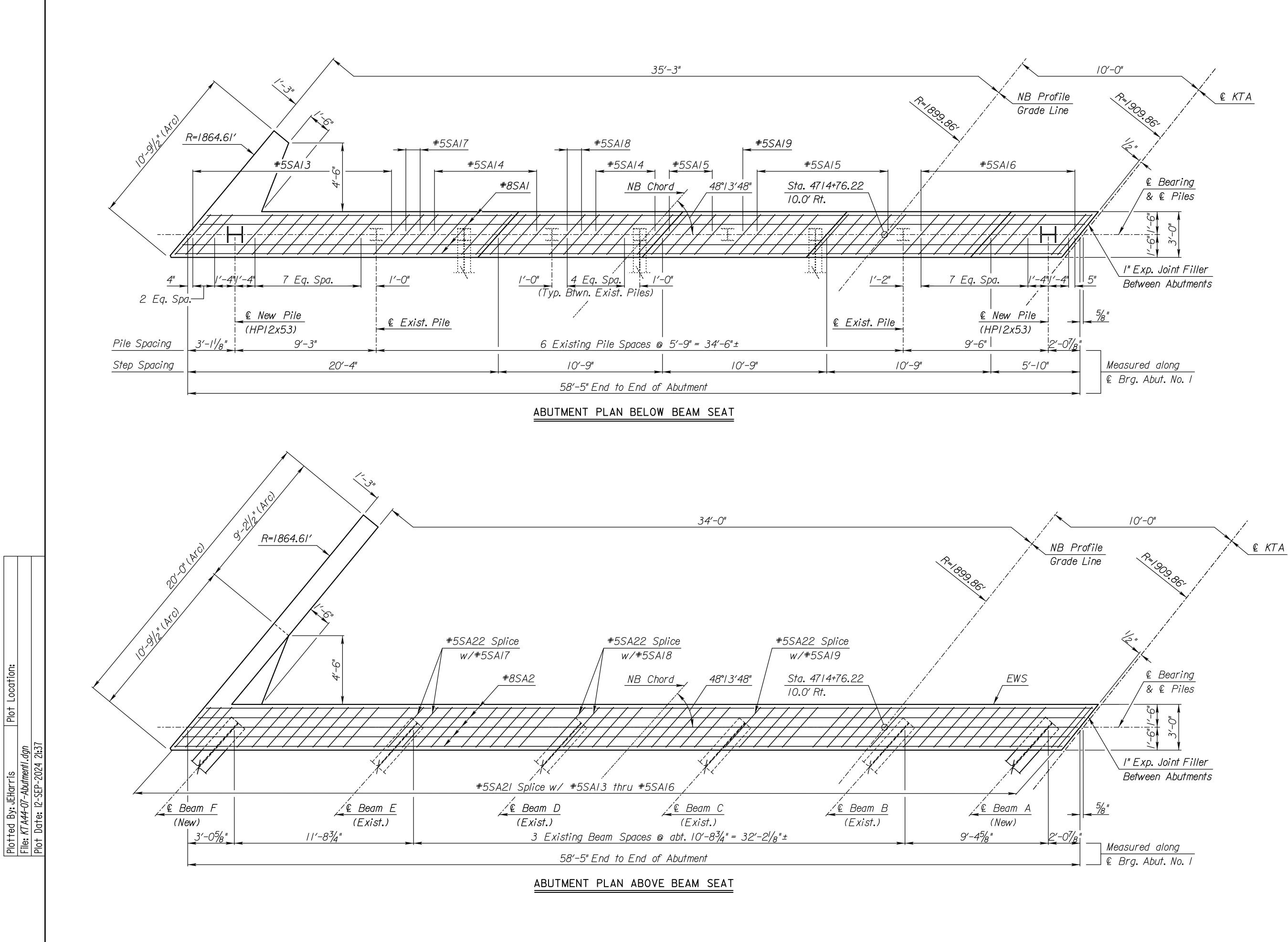
PILE DRIVING ANALYZER (PDA): All PDA testing for this project shall be performed by an independent testing firm to be hired by the Contractor. PDA testing shall be performed on each Test Pile (Special) to confirm nominal compressive resistance and develop driving criteria for production piles.

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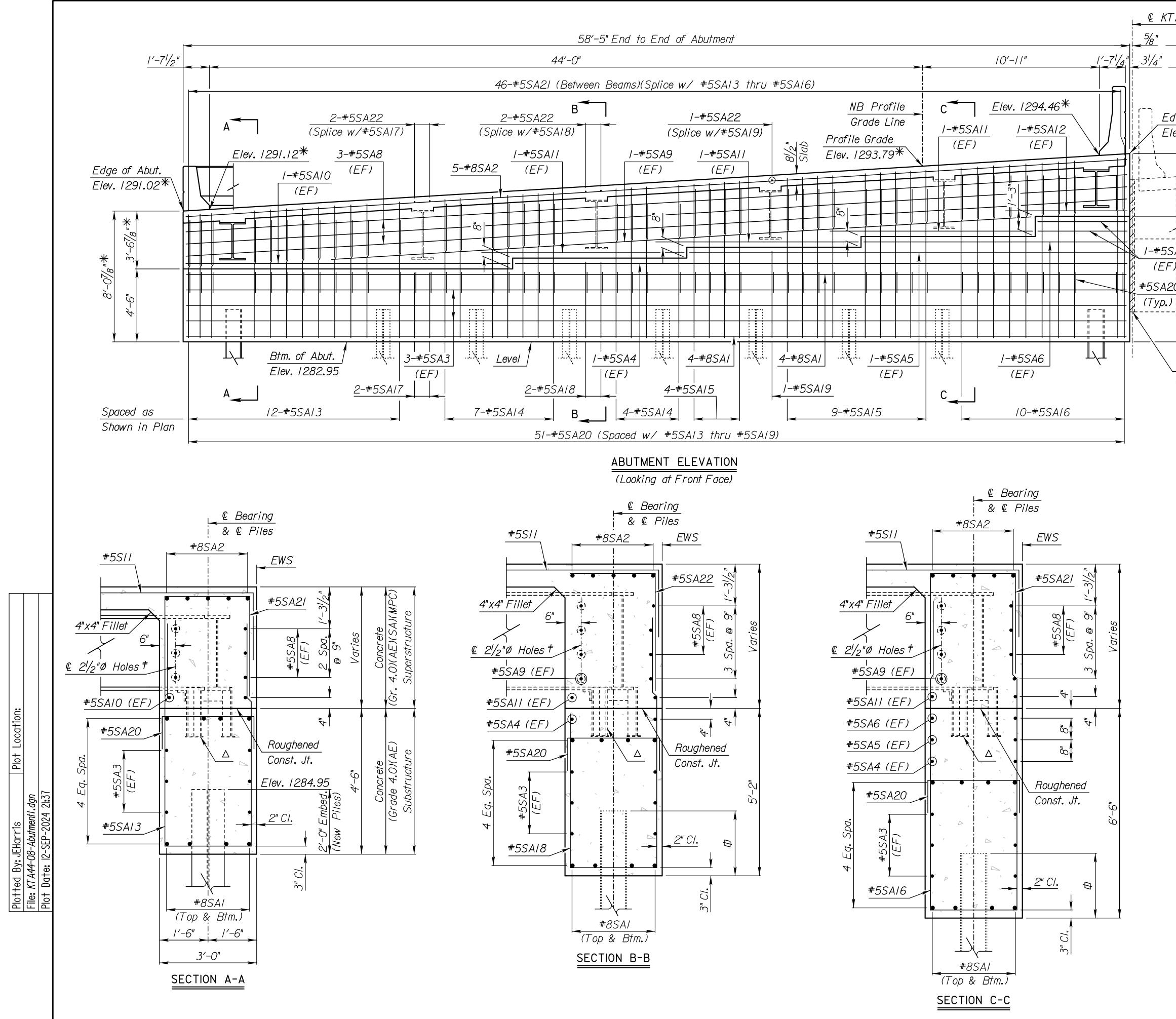
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KANSAS	8082	2024	35	134

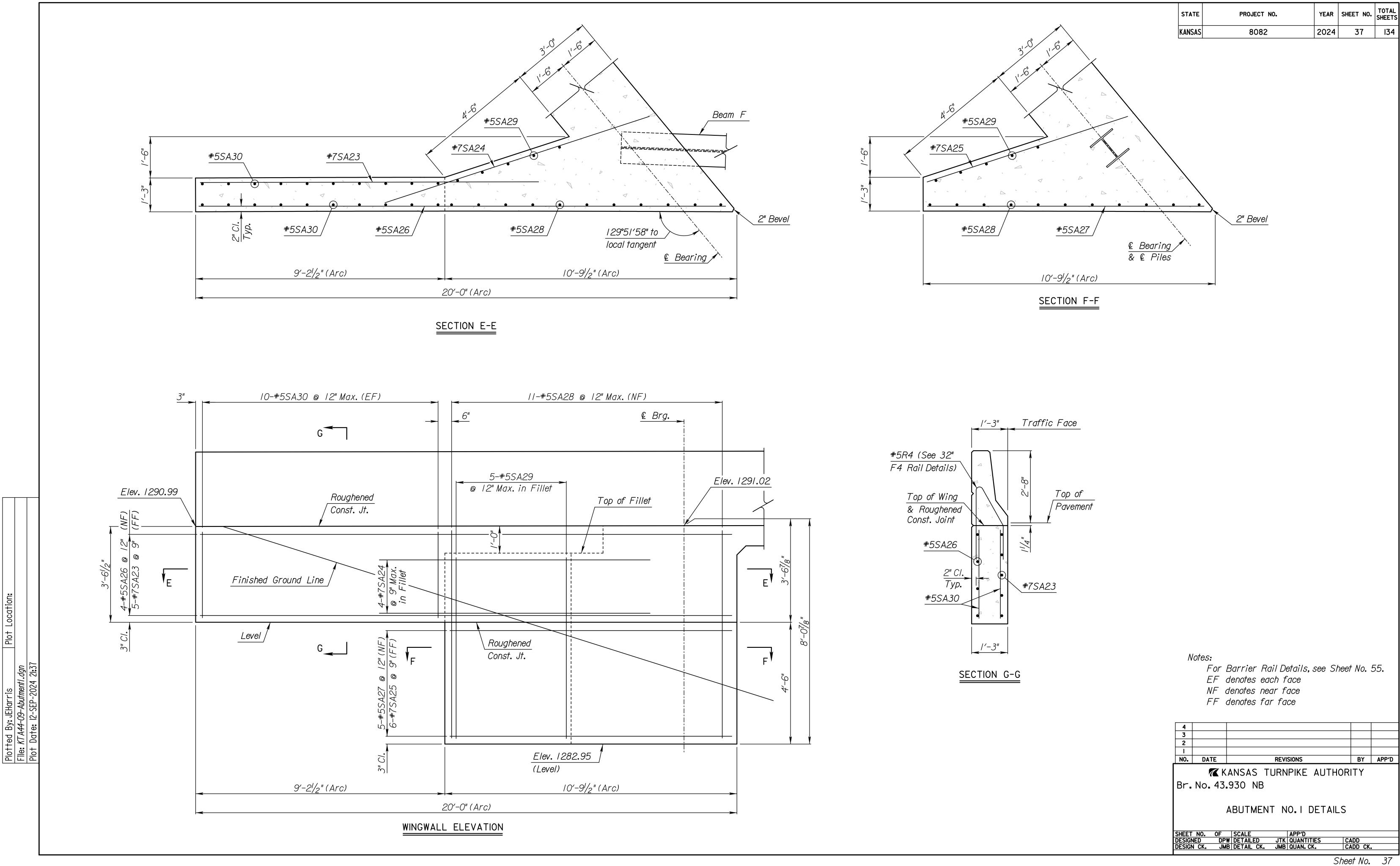
Notes: Stirrup spacing is measured along € Bearing. Place stirrups parallel to © Beams. For Wingwall Details, see Sheet No. 37. See Sheet No. 41 for additional abutment drainage details and limits of Bridge Backwall Protection System.

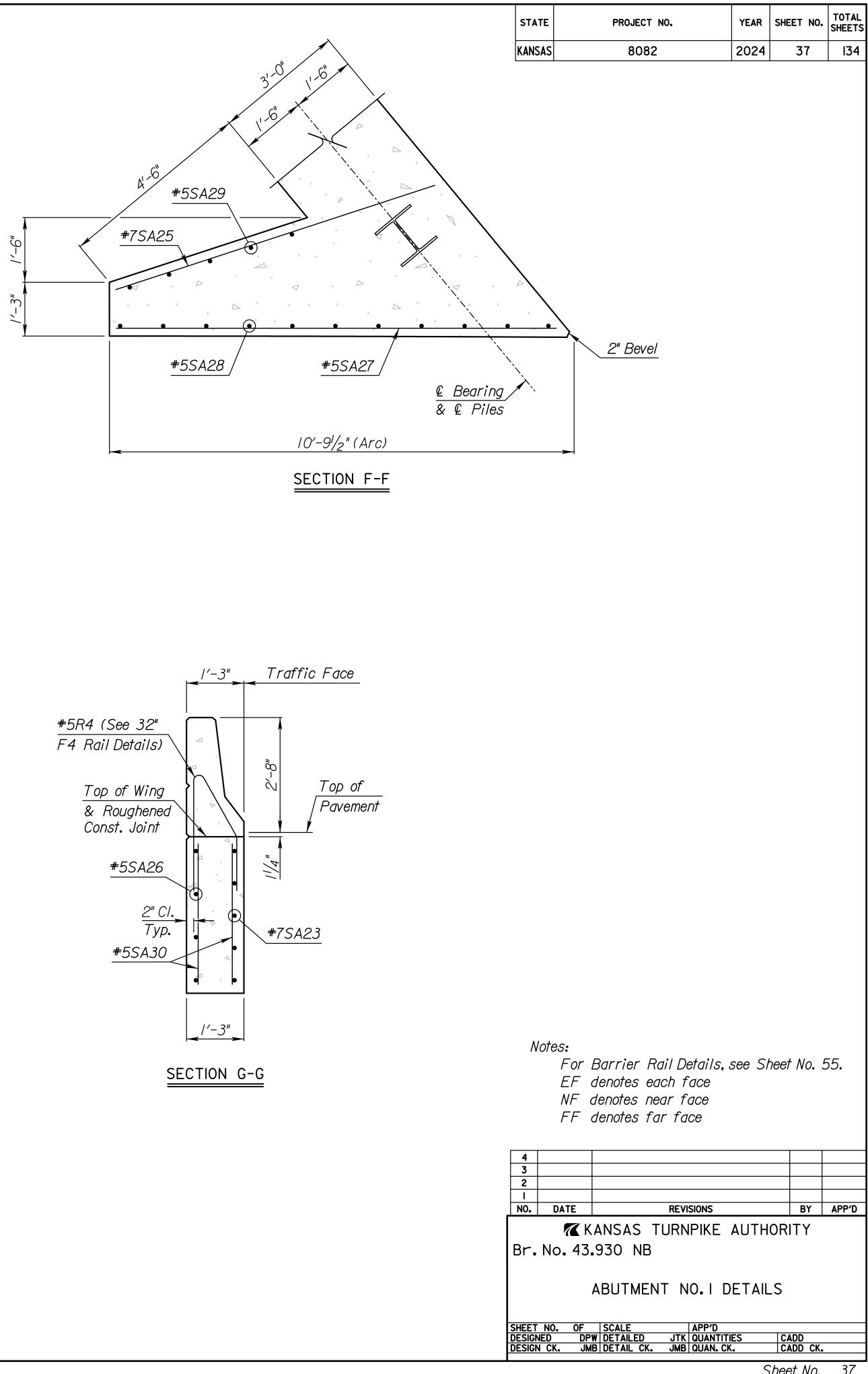
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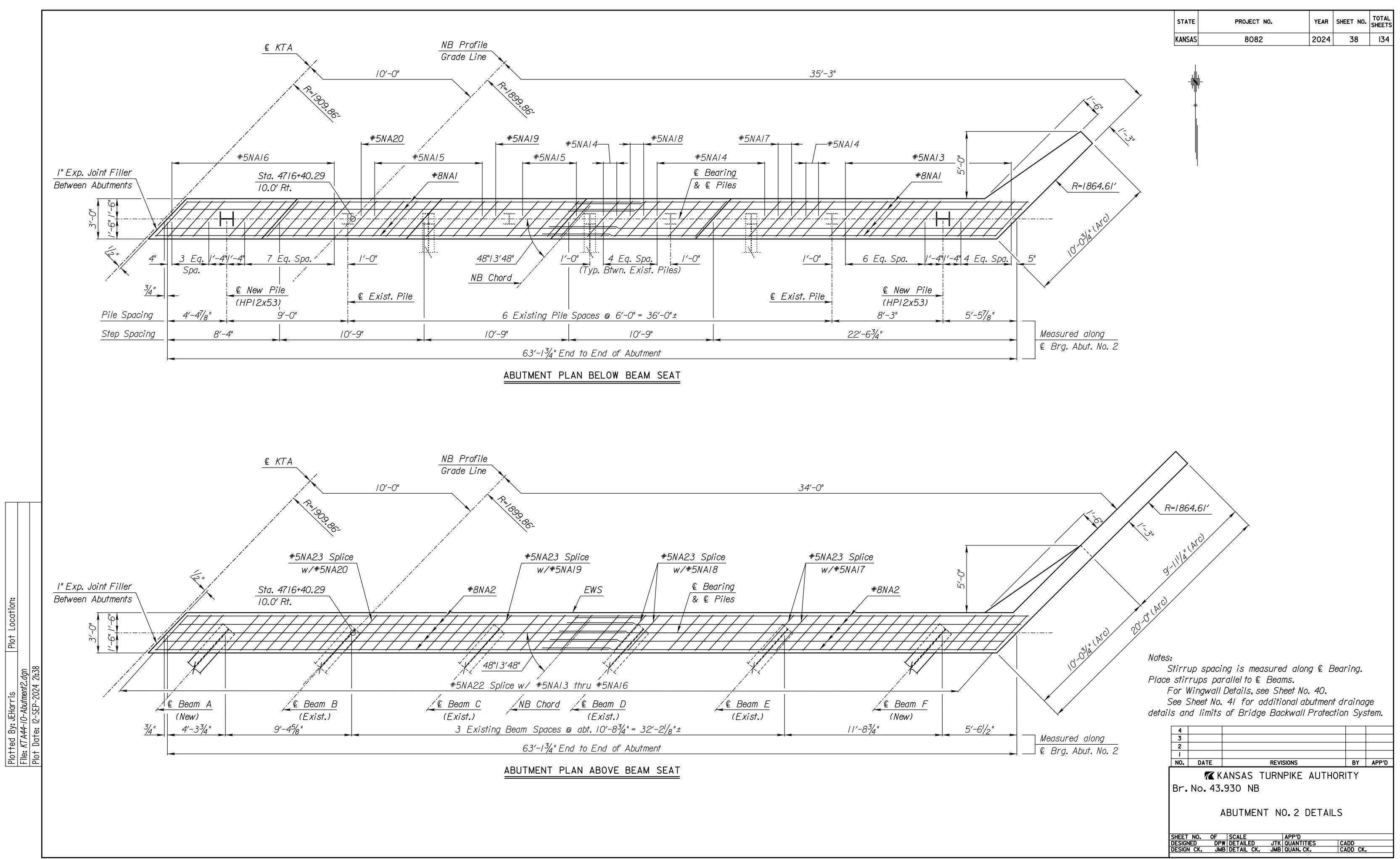


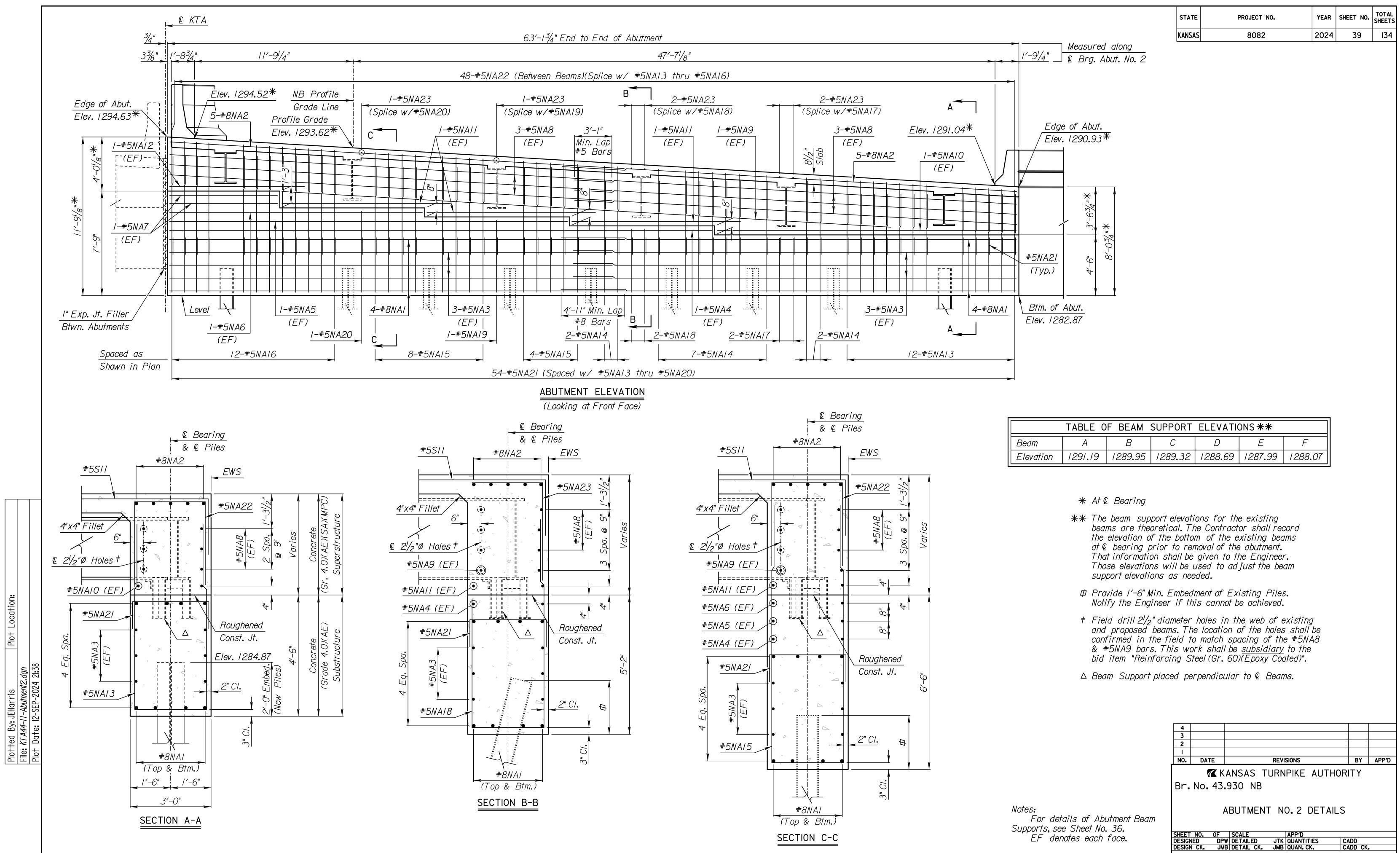
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	TABLE O	F BEAM	SUPPORT	ELEVATIONS	**		
¥ ¥	Beam A	B	C	D	E	F	
∖ I" Exp. Jt. Filler	Elevation 1291.25	1289.95	1289.29	1288.69 128	88.05	1288.0	)/
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	lote: EF denotes each face.	SHEET NO					
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Sheet No. 36

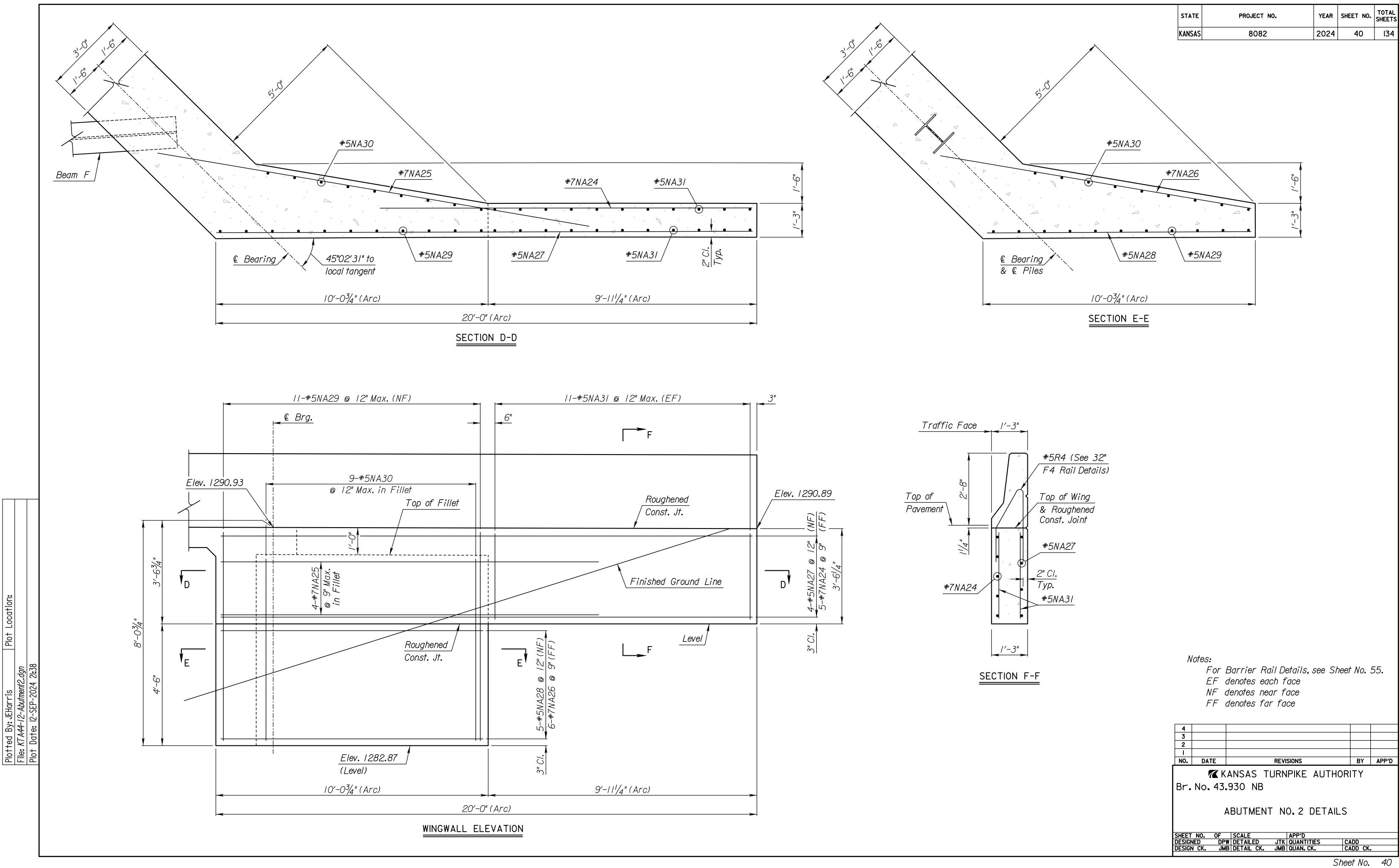


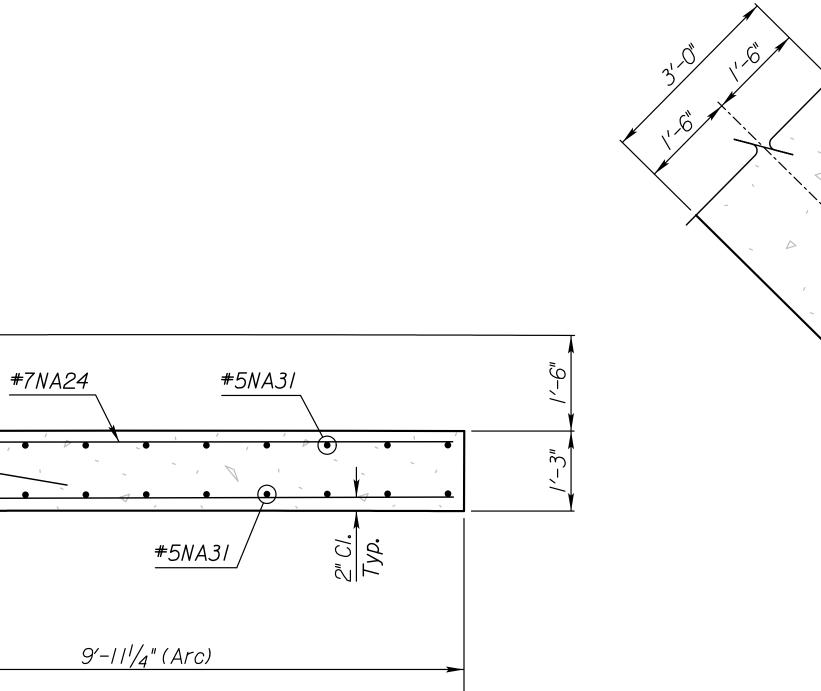


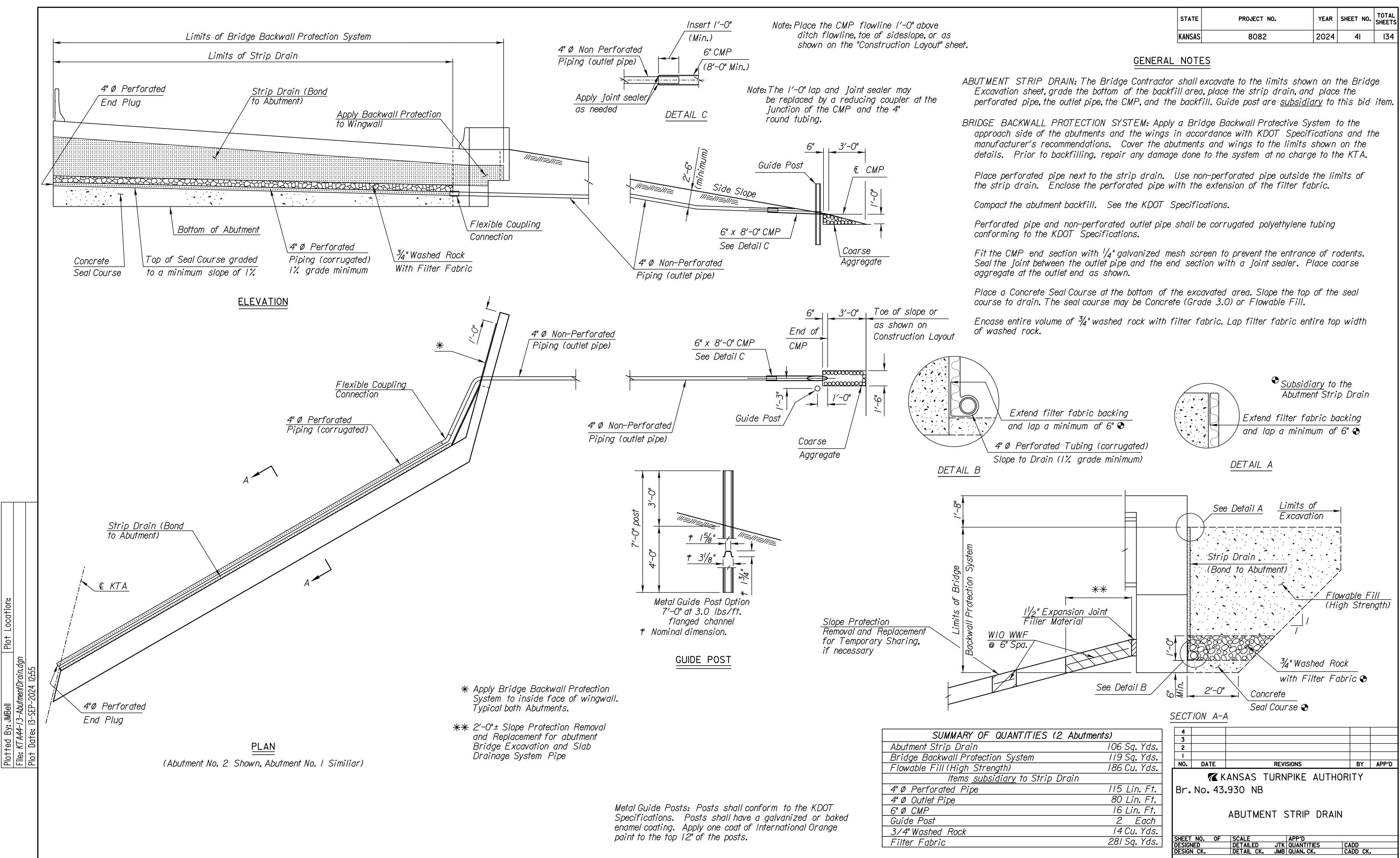




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; For details of Abutment Beam prts, see Sheet No. 36.			ABUTMEN	ΓΝ	0.2	DETAIL	S	
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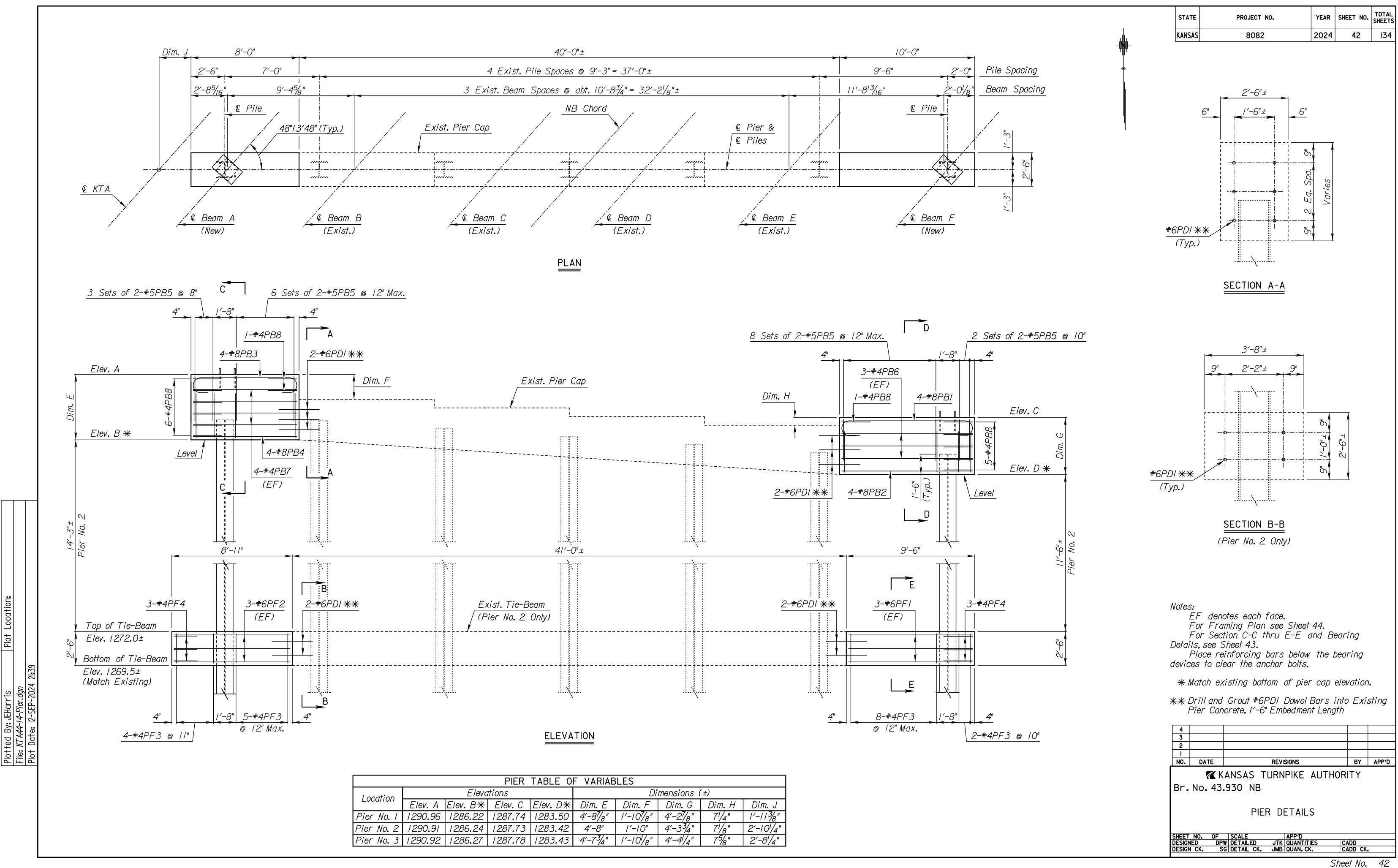




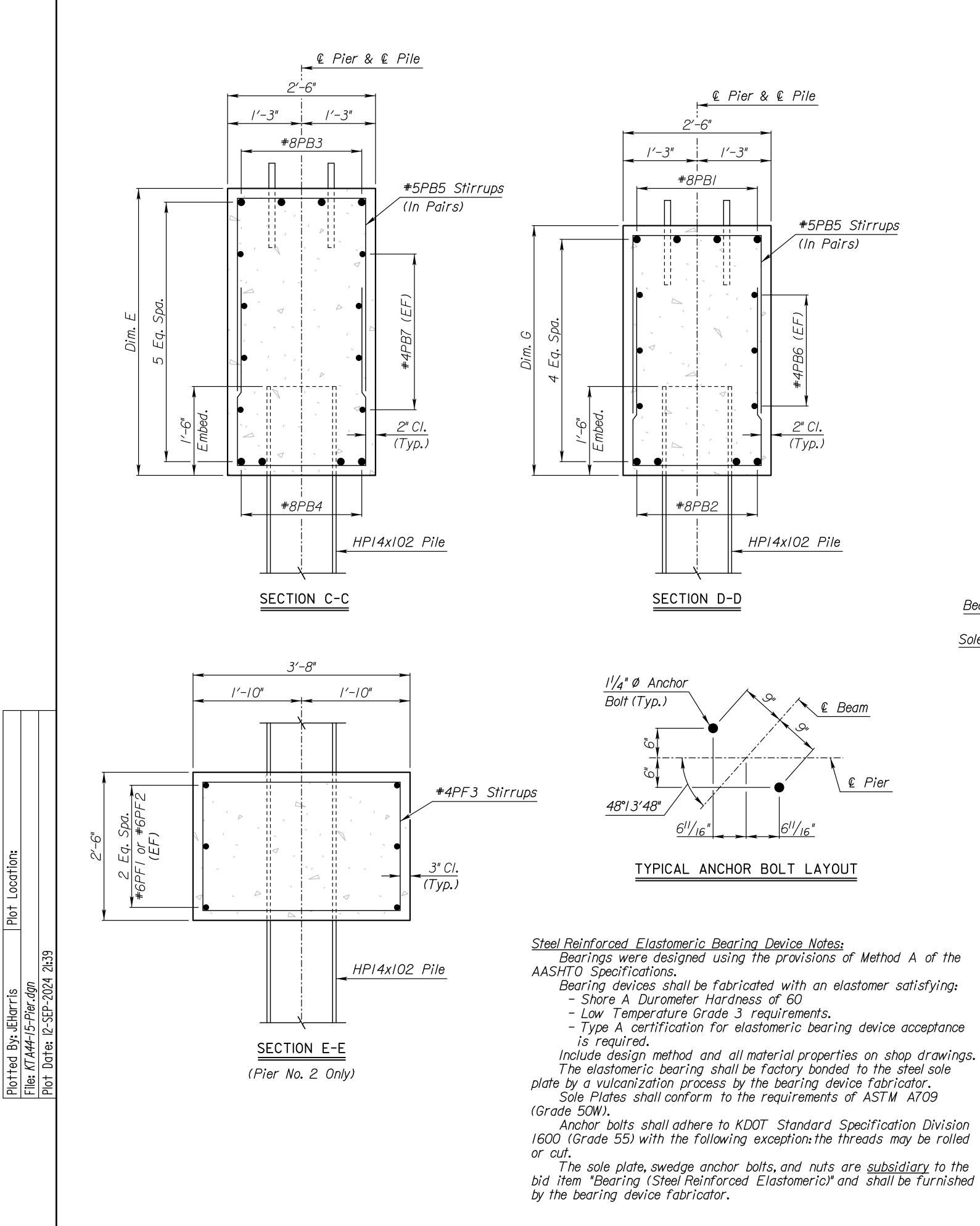


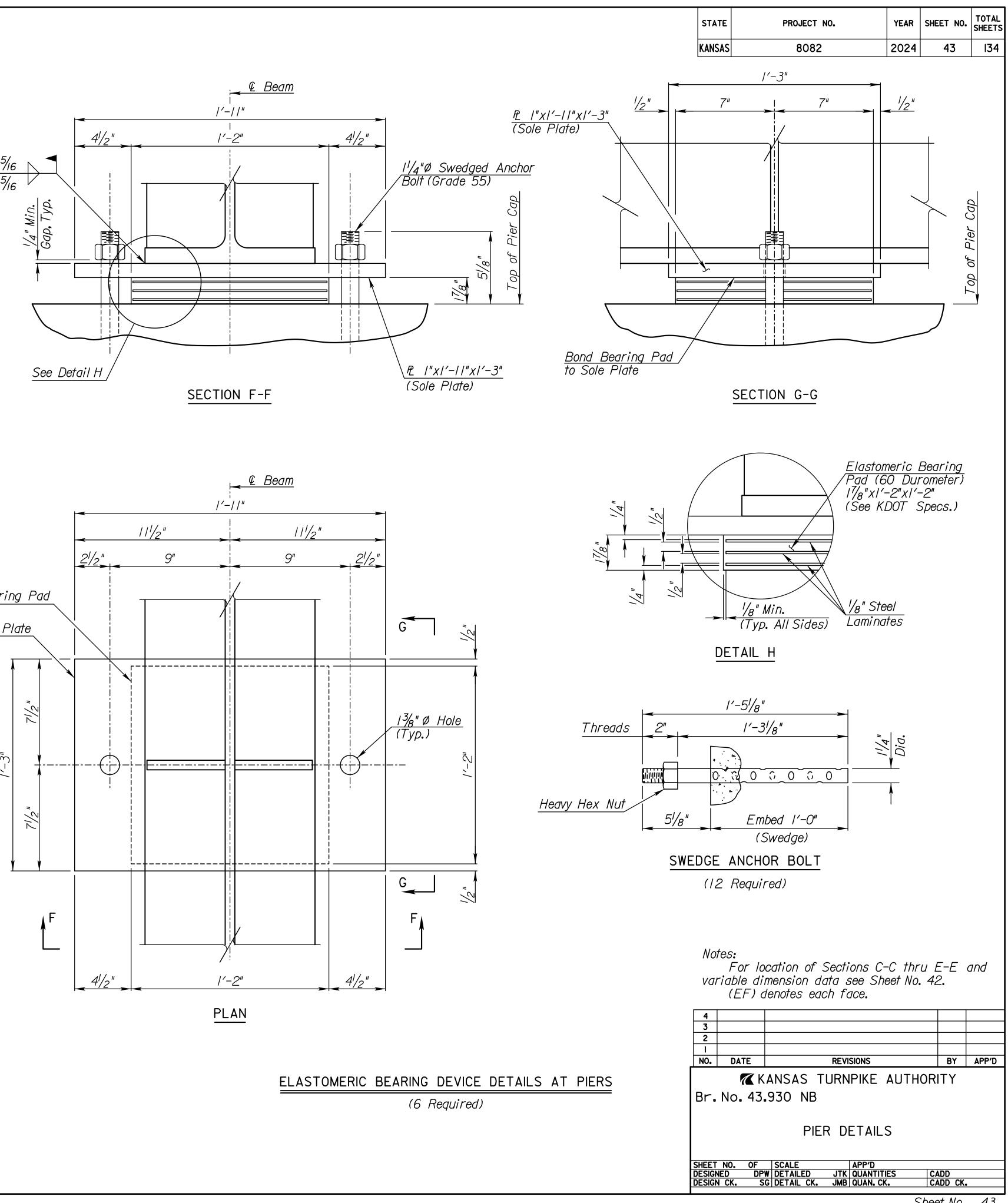
STATE	PROJECT NO.	YEAR	SHEET NO.	TOTAL SHEETS
KANSAS	8082	2024	41	134

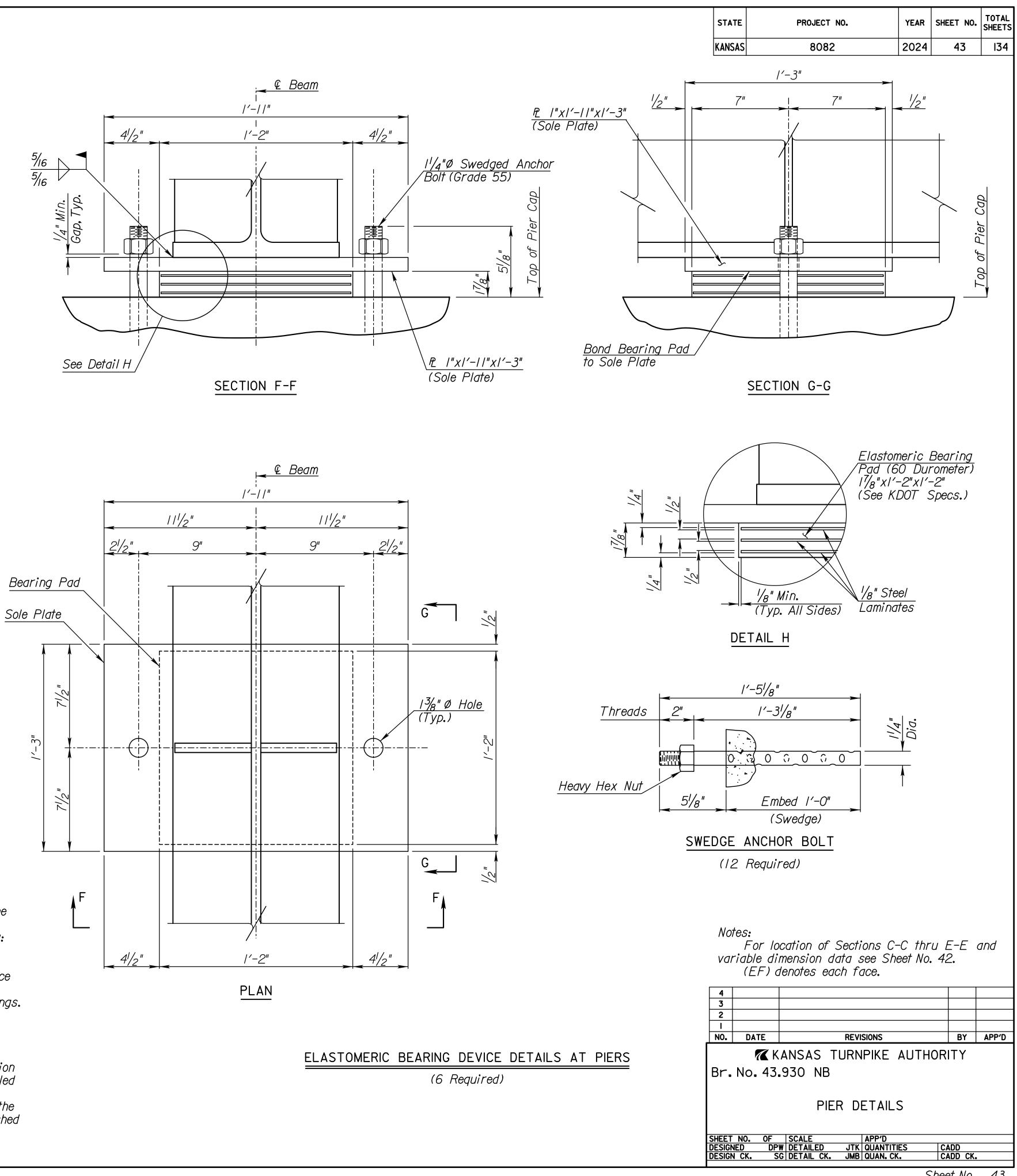
Sheet No. 41



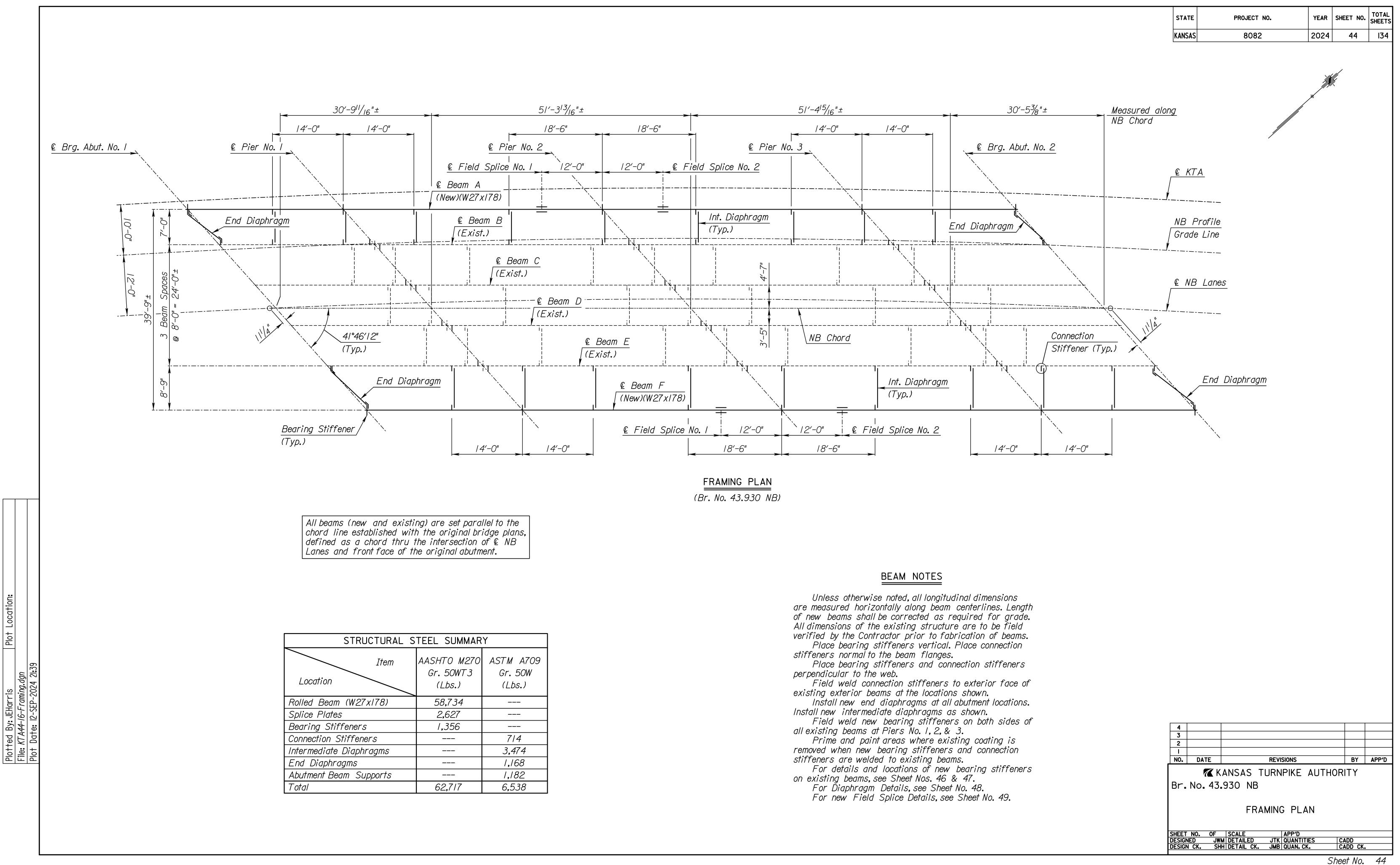
	PIER TABLE OF VARIABLES										
Elevations (±)											
<i>∕. B</i> ₩	Elev. C	Elev. D*	Dim. E	Dim. E Dim. F Dim. G Dim. H L							
36.22	1287.74	1283.50	4′-87⁄8"	'- 07/8"	4'-2 <mark>7/</mark> 8"	71/4"	'-   <sup>3</sup> /8"				
86.24	1287.73	1283.42	4′-8″	/'-/0"	4'-3 <sup>3</sup> /4"	7 <sup> </sup> /8"	2'-101/4"				
86.27	1287.78	1283.43	4'-7 <sup>3</sup> /4"	'- 0 <mark> /</mark> 8"	4'-4 <sup> </sup> / <sub>4</sub> "	7 <sup>5</sup> ⁄8"	2'-81/4"				





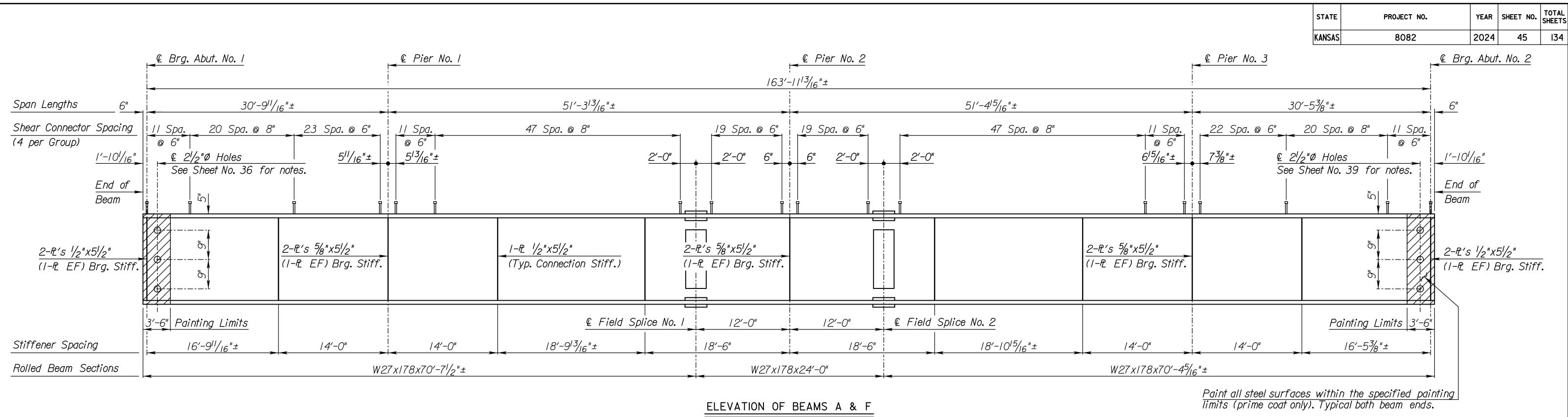


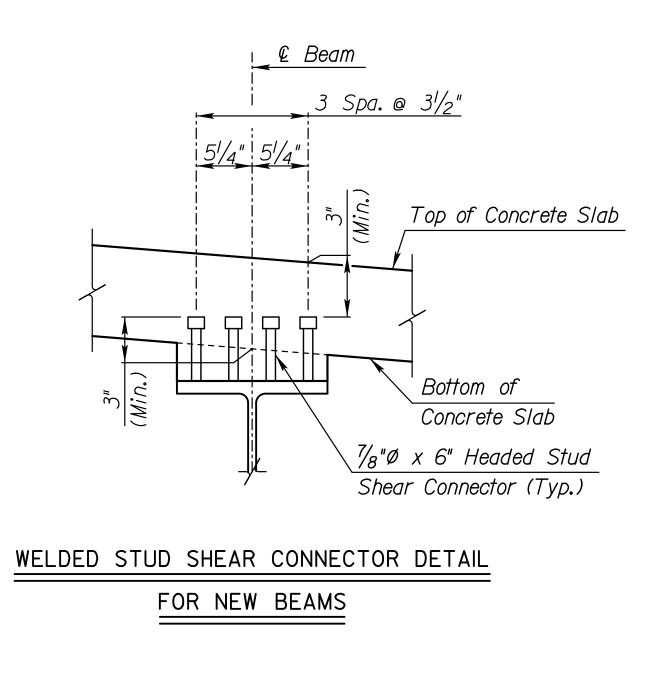
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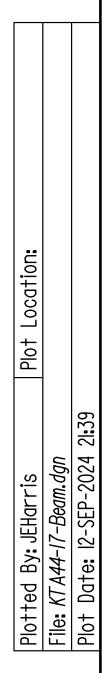


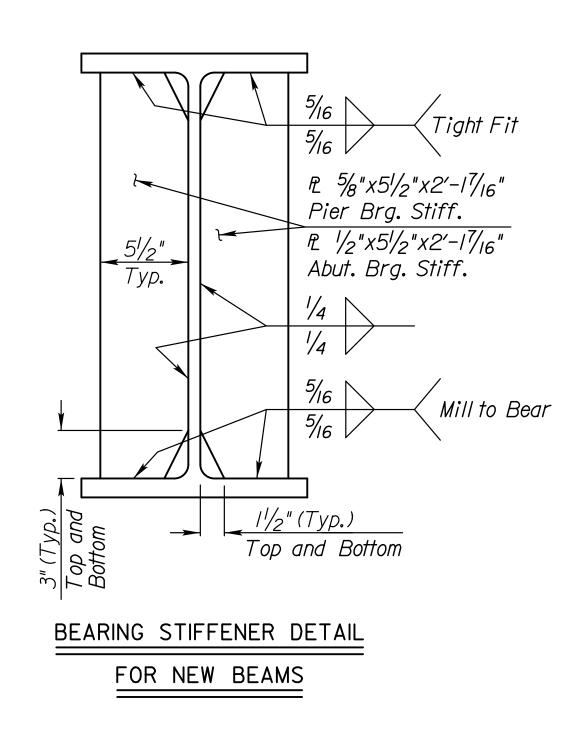
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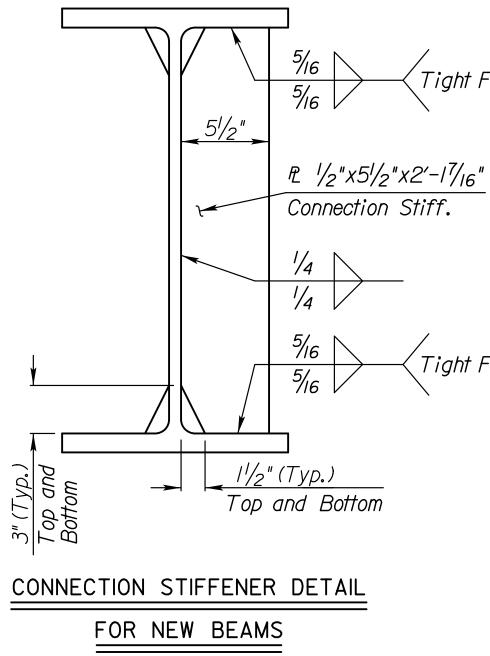
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	6,538











, Tight Fit

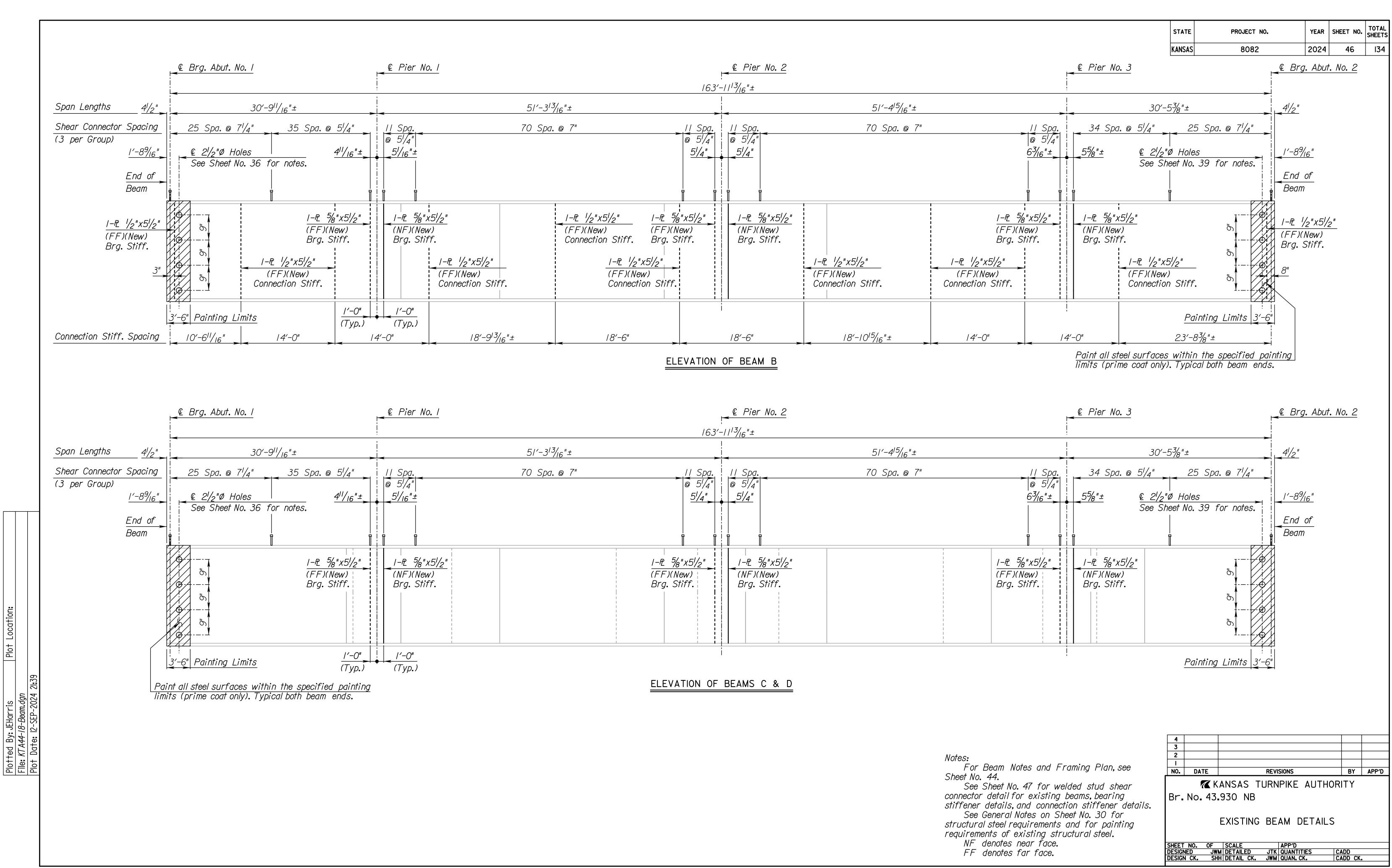
Tight Fit

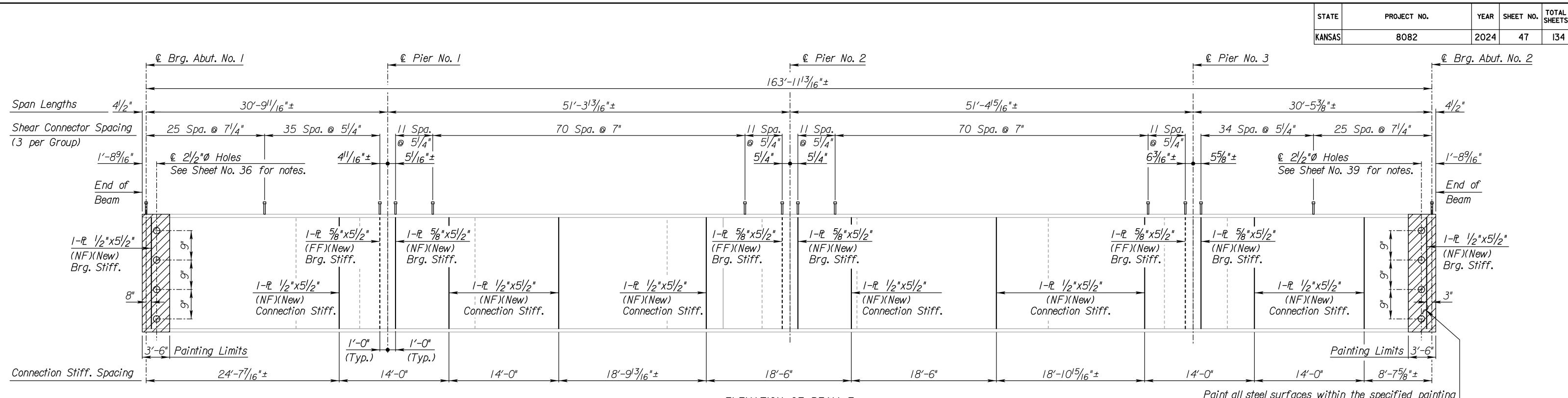
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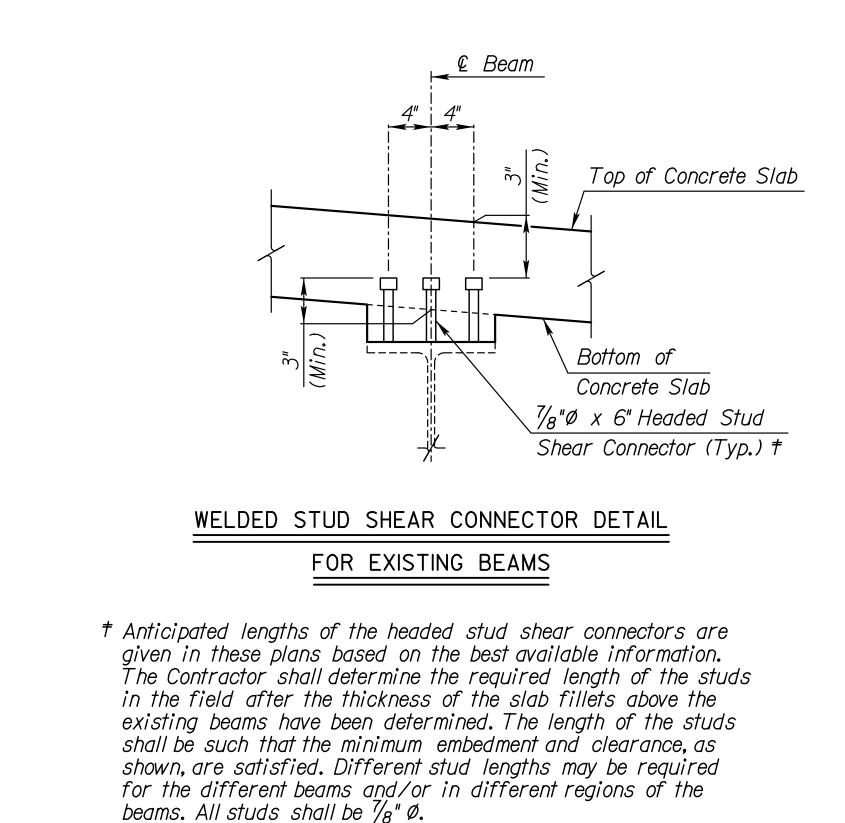
Connection stiffeners are located on the side of the web indicated on the Framing Plan. For Beam Notes and Framing Plan, see Sheet No. 44.

For Field Splice Details, see Sheet No. 49. Field splices shall be made only where shown on the Contract Plans as a "splice". Elimination of any "splice" may be requested. See General Notes on Sheet No. 30 for structural steel requirements and for painting requirements of new weathering steel. EF denotes each face.

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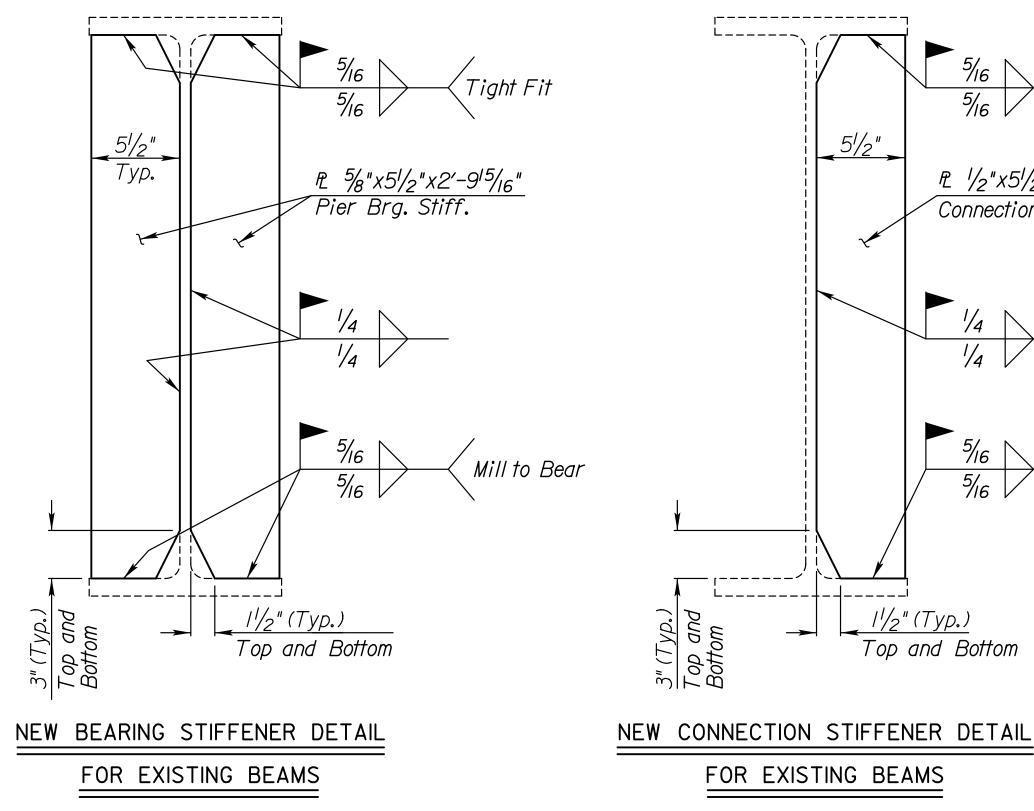






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# ELEVATION OF BEAM E

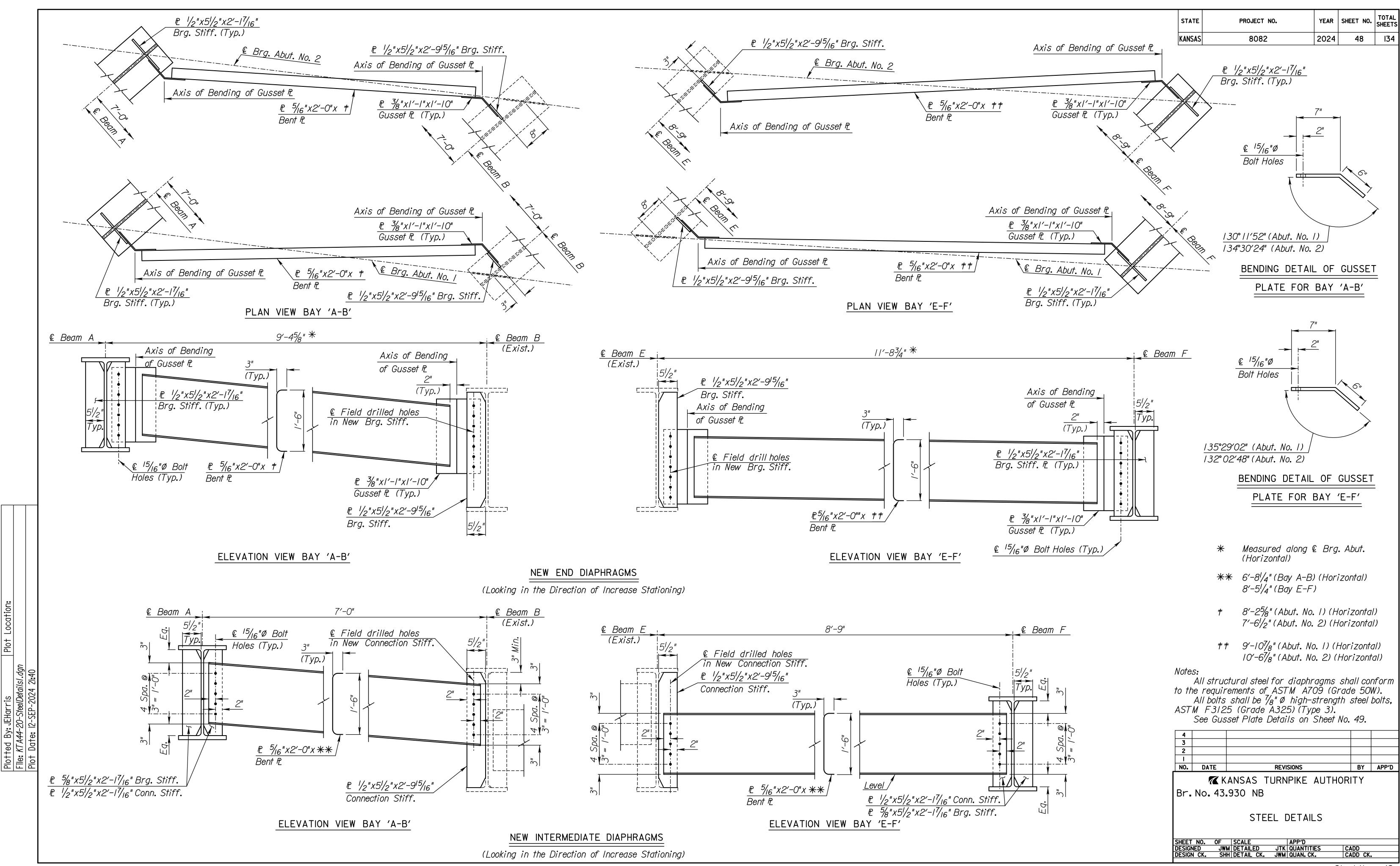


Paint all steel surfaces within the specified painting limits (prime coat only). Typical both beam ends.

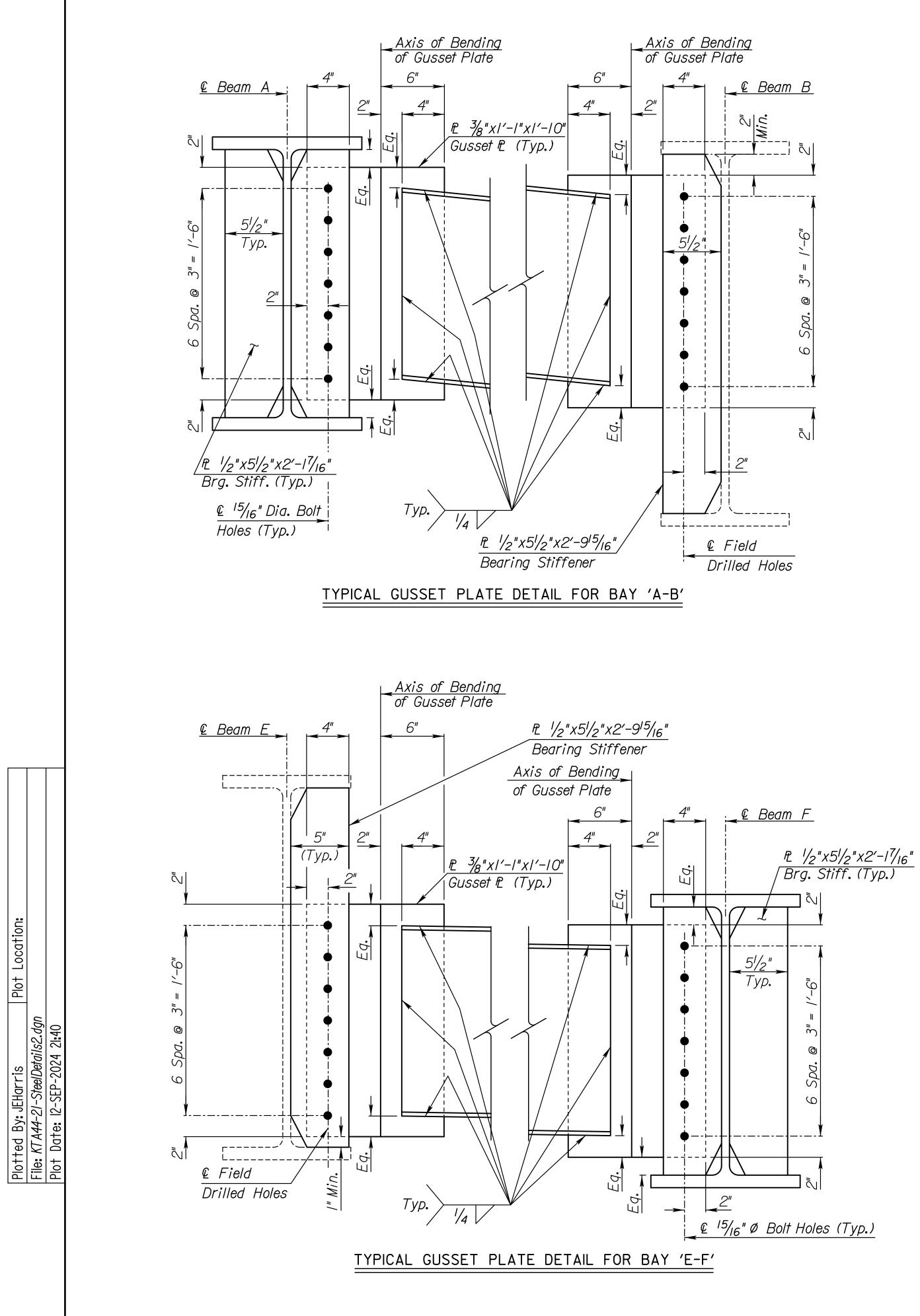
PL 1/2"x51/2"x2'-915/16" Connection Stiff.

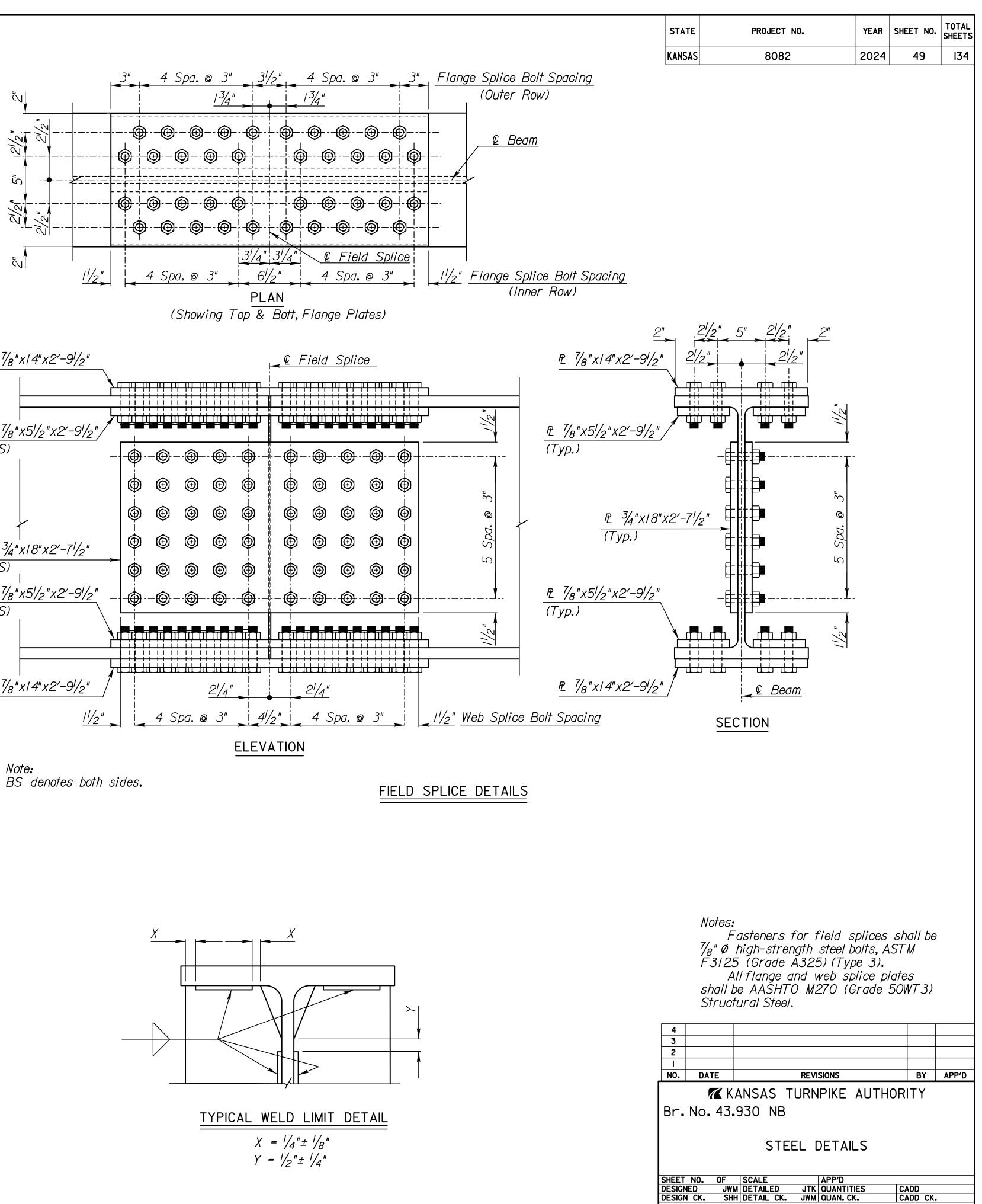
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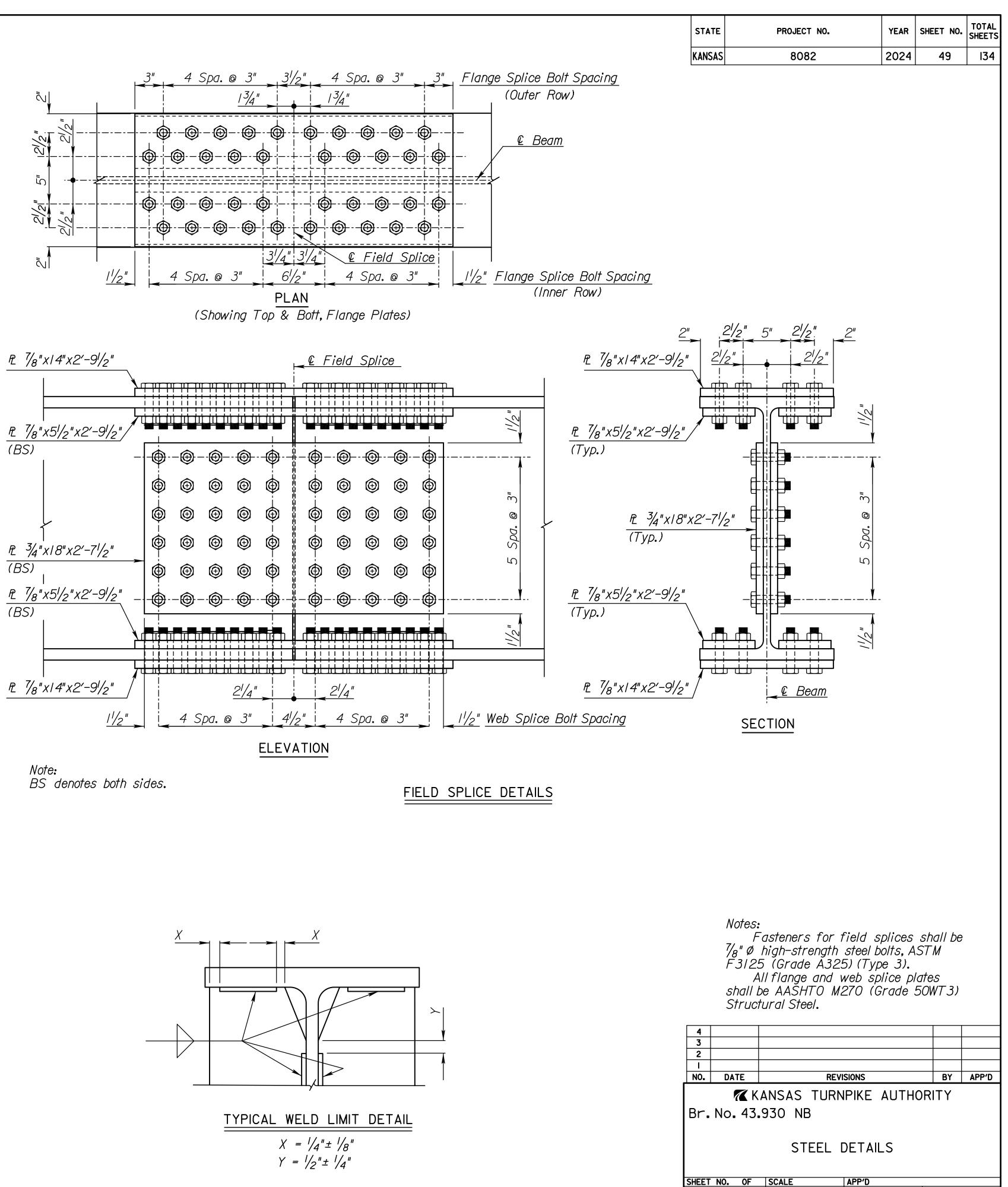
She str	Notes: For Beam Notes and Framing Plan, see Sheet No. 44. See General Notes on Sheet No. 30 for structural steel requirements and for painting requirements of existing structural steel. NF denotes near face. FF denotes far face.													
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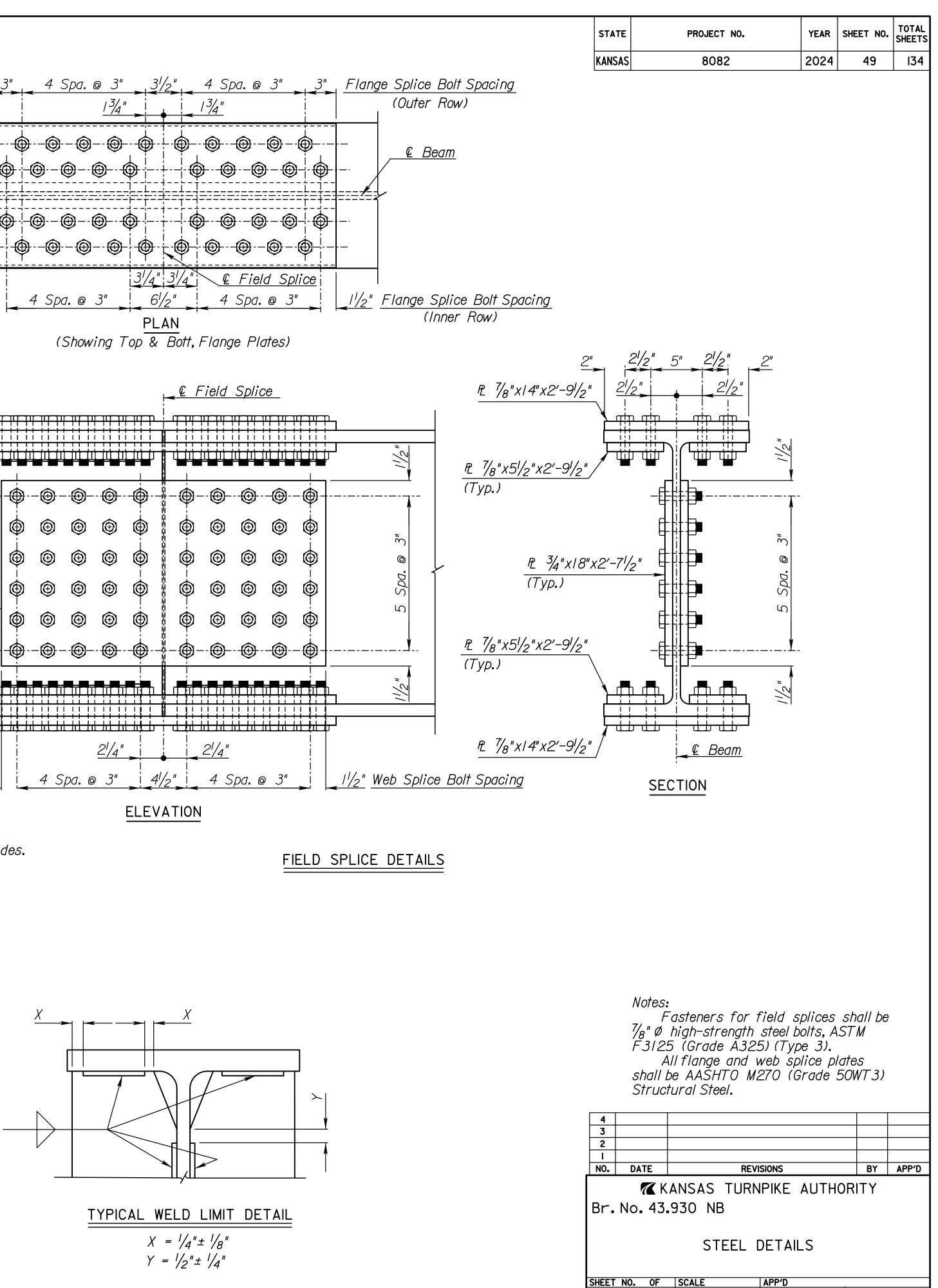


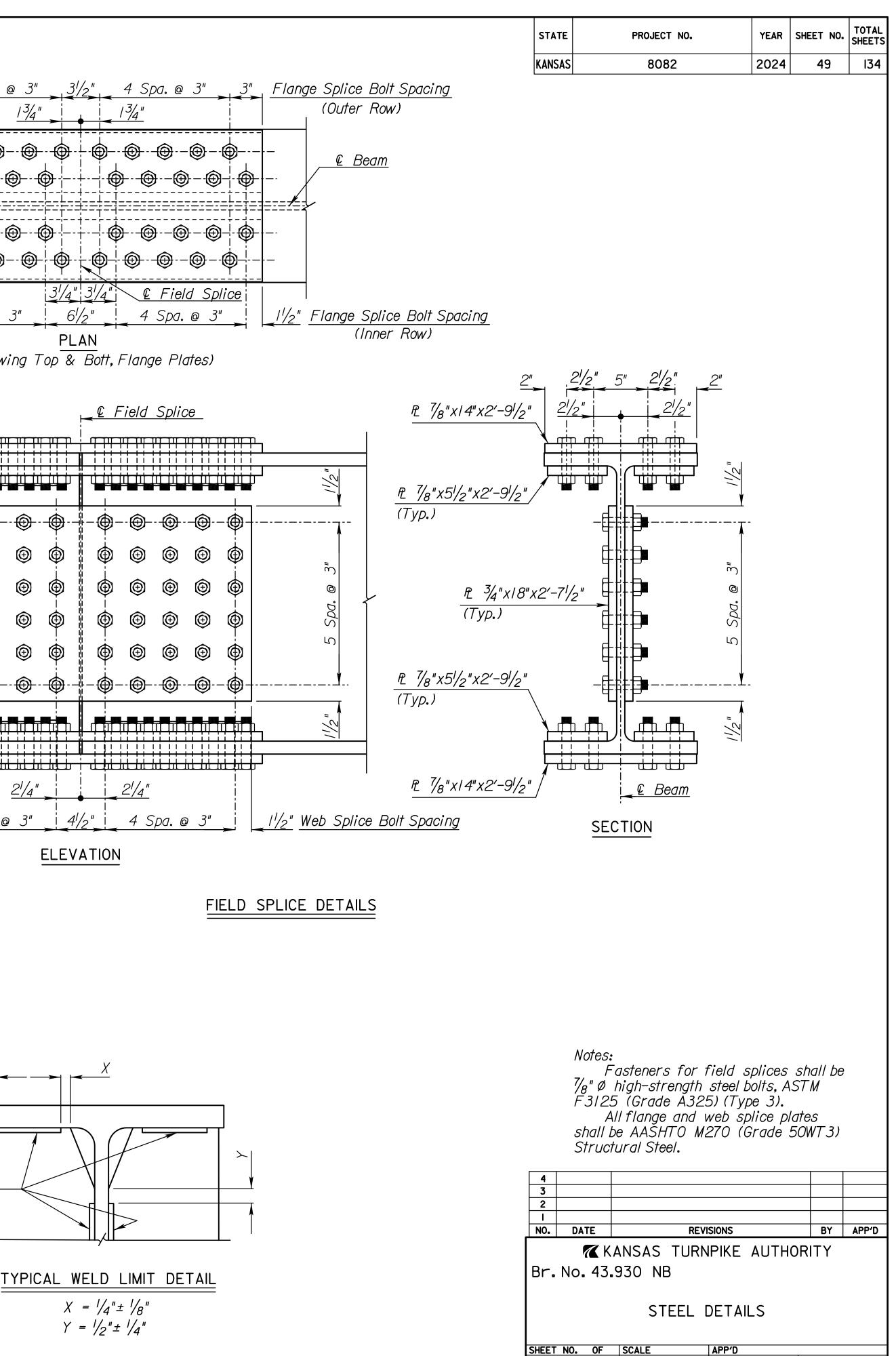
Sheet No. 48

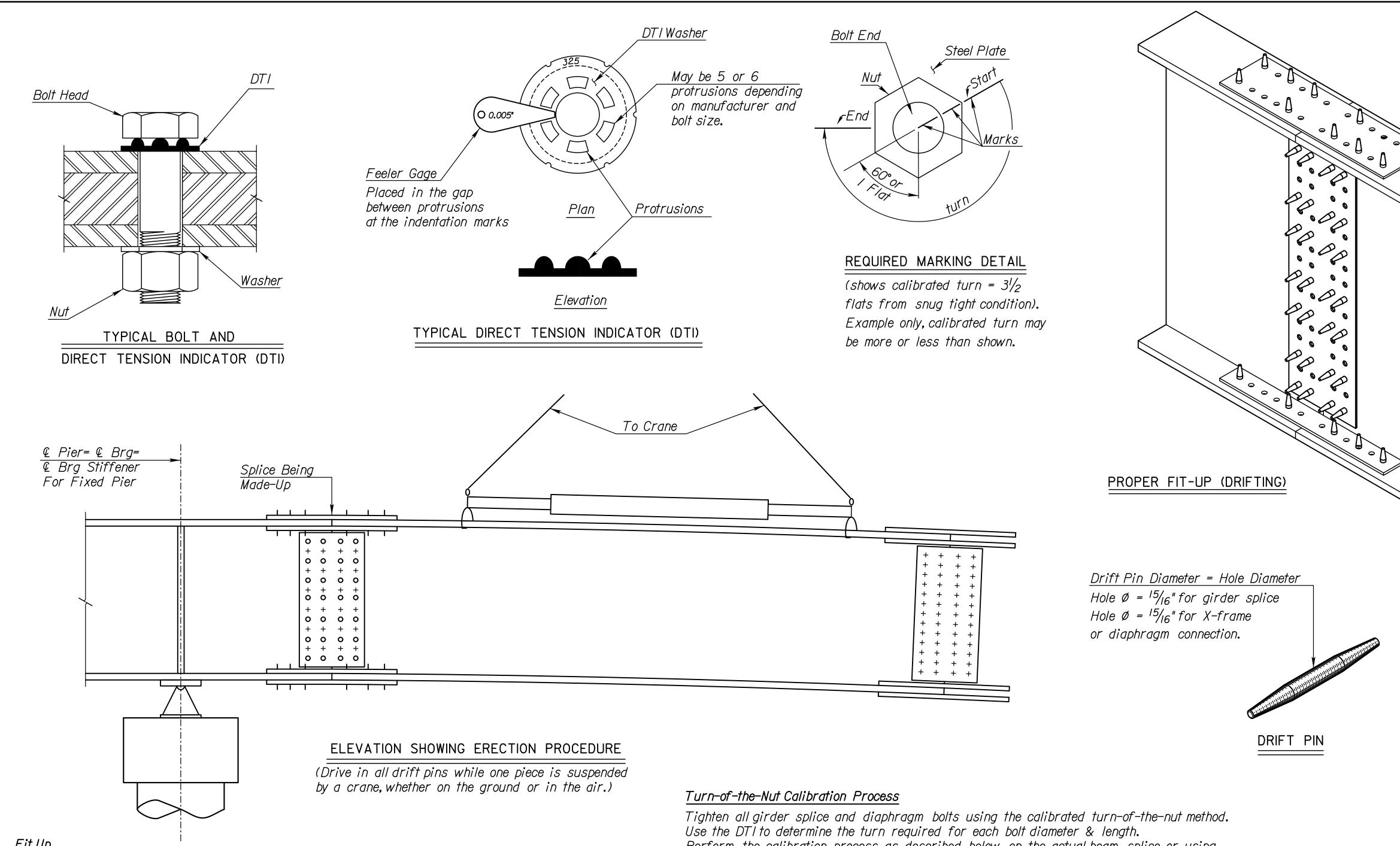












### Fit Up

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Plot

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During the fit up, install drift pins in all corner bolt holes, plus 25 percent of the bolt holes (as a min.), evenly distributed throughout the splice. Fill at least 25 percent of the bolt holes with high strength bolts. Fully tighten these bolts by the calibrated turn-of-the-nut method before removing any drift pins or moving the members. These bolts may be either erection bolts or production bolts. Erection bolts are used during fit up, to compress the plies of the splice to achieve a snug condition. Erection bolts are the property of the Contractor and do not remain in the bridge permanently. Erection bolts must be A325, and can be reused. Erection bolts are required when the abutting plates are of different thickness and no fill plate is provided. This situation usually results in a slight bending of the splice plates. If erection bolts are not used, the DTI's may fully compress before the plates are in firm contact. This would be cause for rejecting the splice. Clearly mark the erection bolts so that they are not left in the splice.

### Erection

Two independent crews will survey the bearing seat elevations. The Engineer will verify that the results of those surveys show that the bearing seat elevations are within  $\pm \frac{1}{4}$  inch of the plan elevations before erection begins. Use the blocking diagram, as shown on the shop drawings, when erecting the beams/girders on the ground. Do not lift the assembled pieces into position until at least 25 percent of the holes are filled with fully tightened bolts. Locate the centerline of the bearing stiffener with the centerline of bearing device. Secure the beams/girders to the top of the pier cap prior to placement of the bearing device anchor bolts.

Perform the calibration process as described below on the actual beam splice or using 3 plies of steel plate with the same thickness as the actual splice.

I. Bring at least 25 percent of the bolts in the splice to a "snug-tight-condition". "Snug tight condition" is defined as (with all plies in firm contact) "the full effort of a man on a spud wrench". Usually a smaller impact gun  $\left(\frac{1}{2}\right)$  drive) is used to snug the splice and a larger impact gun (1" drive) is used for final tightening. This is preferred over the use of a spud wrench. Production bolting and calibration must use the same tools and lubricating procedures. If an impact wrench is used to "iron the plates" and snug the bolts for calibration, then an impact wrench must be used during the snugging process during production bolting.

2. See "Required Marking Detail" (choose a bolt at the center of the splice and recheck snug on ad jacent bolts)

- a. Mark the outside of the socket at one of the corners.
- b. Mark the bolt, plate, and nut at a corner with a start line.
- Align the mark on the socket with the start mark on the bolt end.
- d. While holding a backup wrench on the head of the bolt, turn the nut  $\frac{1}{2}$  turn (3 flats).
- Record the number of refusals. е.
- f. If all of the gaps refuse, go to another bolt and turn the nut 2 flats (1/3 turn).
- g. If there are fewer than 3 refusals turn the nut an additional  $\frac{1}{4}$  of a flat (15 degrees).
- h. Repeat step g, turning the nut 1/3 of a flat or less each time, until all of the gaps refuse the feeler gage. Record the amount required to cause all of the gaps to refuse the feeler gage. This is the target rotation.

3. Repeat this process for each bolt diameter and length.

STATE	PROJECT NO.	YEAR	SHEET NO.	TOTAL SHEETS
KANSAS	8082	2024	50	134

### Production Bolt Tightening

I. Install bolts and tighten to "snug tight" in a pattern, starting at the center of the splice and working toward the edge. On large girders this may have to be done twice, as the center bolts will become loose as plates are "Ironed out". This step is important because typically, any variation in results during production bolting is the result of a change in the materials, lubricant or equipment used to take the bolts to a "snug tight" condition during the calibration process.

2. Mark all of the bolts, nuts and the plate as shown in the marking detail. Mark the socket with a start and stop point. The stop point corresponds to the target rotation determined earlier.

3. Align the start mark on the socket with the line on the plate. While the bolt is being backed up, turn the nut until the stop mark on the socket lines up with the start mark on the plate.

4. Repeat with all bolts of the same length in the splice.

### Acceptance and Rejection of Bolts

I. The Engineer will check all bolts with a feeler gage.

2. All nuts must be turned at least the target rotation beyond "snug tight".

3. All DTI's must have at least 3 refusals of the 0.005" gage.

4. If all gaps refuse the 0.005" gage, and the nut, plate and bolt are not marked, reject the bolt.

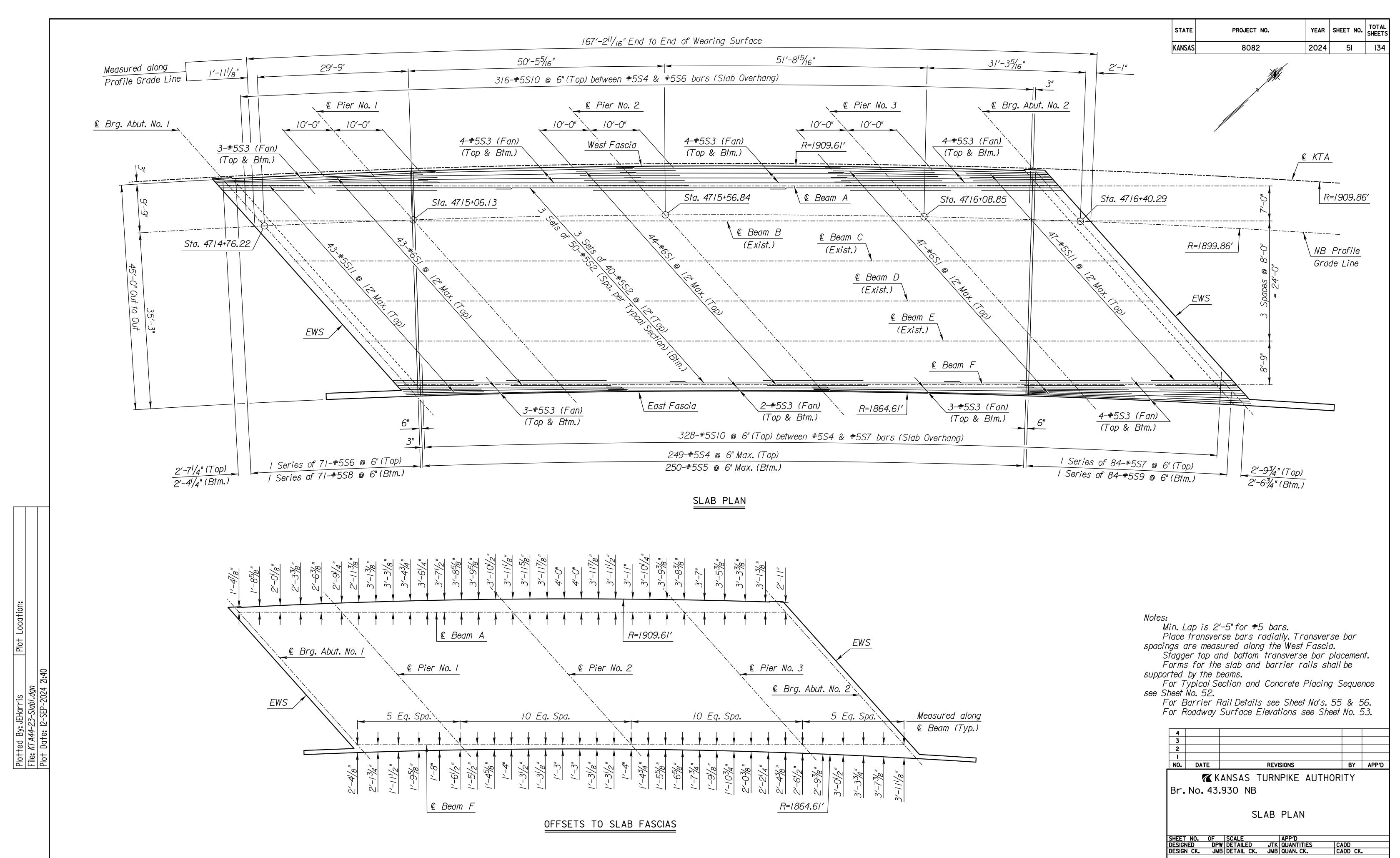
5. If all gaps refuse the 0.005" gage, and the turned element has not been rotated more than 45° beyond the calibrated turn, accept the bolt.

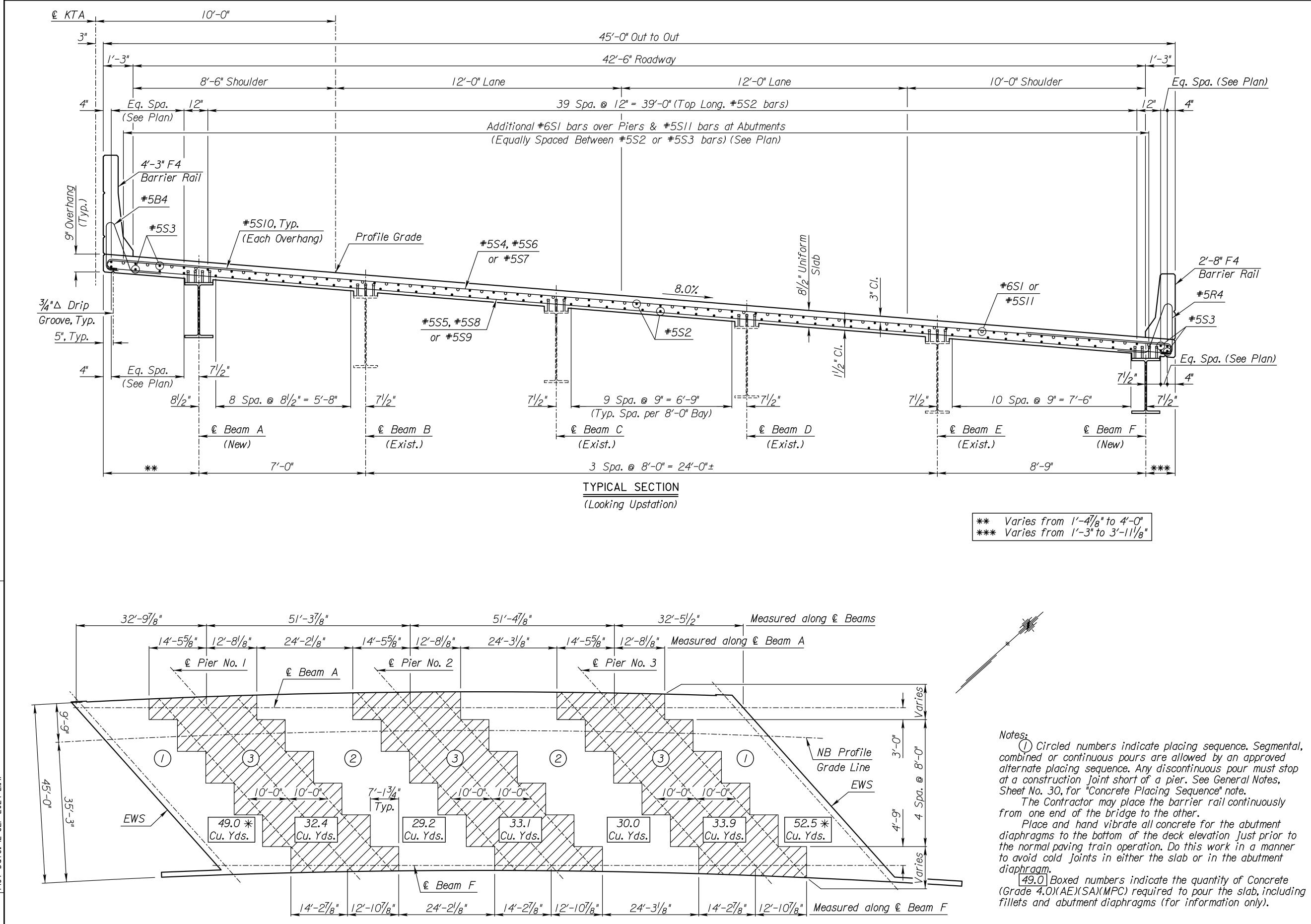
6. If all gaps refuse the 0.005" gage, and the turned element has been rotated more than 45° beyond the calibrated turn, reject the bolt.

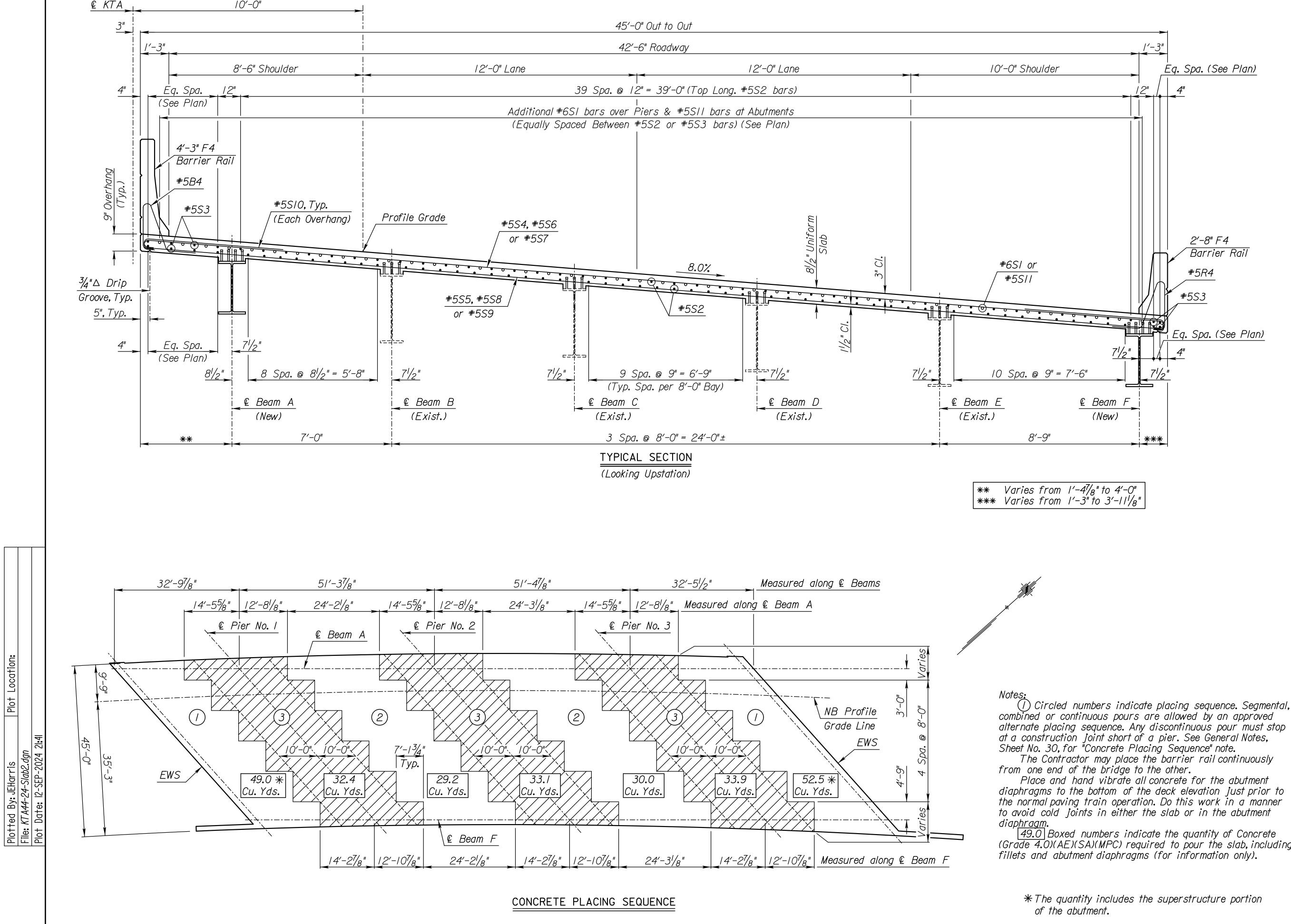
For additional information see the structural steel section of the Bridge Construction Manual.

Suggested Impact wrench models: CP 611 IR 2940 Cleco WS2110 ATP 1011/1040 Norbar PT1500

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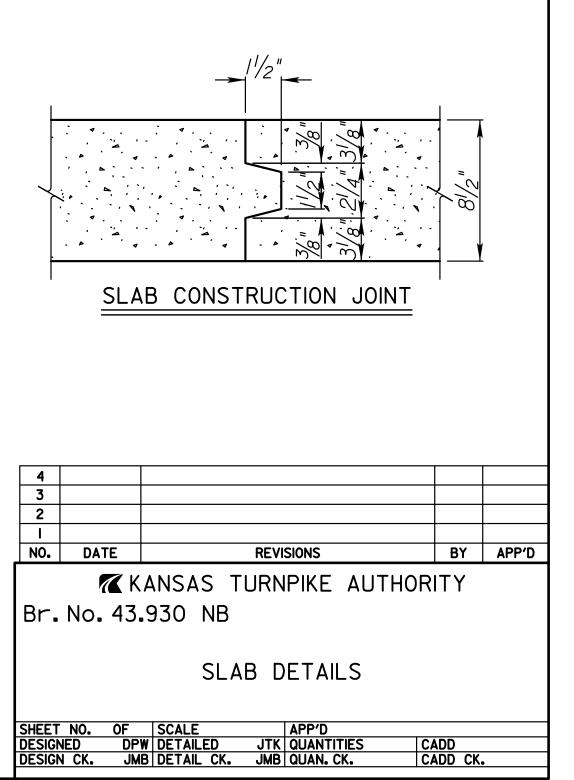




YEAR SHEET NO. SHEETS STATE PROJECT NO. 2024 52 KANSAS 8082 134 1,250 1,250 1,250 1,250 (Lbs) (Lbs) (Lbs) (Lbs) 2'-0" 2'-0" 4'-0" ASSUMED FINISHING MACHINE VALUES LOADING DIAGRAM

Note: Rotation (maximum = 1°) in the exterior girder was calculated assuming screed wheel loads as shown and placed 3" beyond the outside of the deck. The maximum overhang bracket spacing was assumed at 4 ft. The actual screed loadings or bracket spacing will be reflected in the design calculations for a torsional analysis of the exterior girder and bracing. The design calculations shall bear the seal of a licensed Professional Engineer. Submit according to KDOT Specifications Section 700 for falsework and formwork.

Note: Provide temporary bracing at the top and bottom flanges of the exterior beams during paving operations for the deck. Place the bracing at three equal spaces between permanent diaphragms. The top flange bracing members shall be a 1/2" Ø steel rod or greater (Min. Fy = 36 ksi). The bottom flange bracing members shall be a 4" x 4" timber post or greater. The temporary bracing and labor for installation is subsidiary to the bid item "Concrete (Grade 4.0)(AE)(SA)(MPC)". Details of proposed bracing shall be submitted with falsework plans.



				TOF	P OF SLAB	ELEVATIONS				
	Tenth Point		Fascia (West)	Beam A	Beam B	Beam C	Beam D	Beam E	Beam F	Fascia (East)
€ Brg.	1.0	Station	4714+68.34	4714+69.47	4714+75.38	4714+82.19	4714+89.05	4714+95.98	4715+03.63	4715+05.63
Abut. No. 1	7.0	Elevation	1294.56	1294.45	1293.87	1293.22	1292.57	1291.92	1291.21	1291.02
	1.1	Station	4714+71.31	4714+72.55	4714+78.47	4714+85.29	4714+92.17	47/4+99.//	4715+06.78	4715+08.71
	/•/	Elevation	1294.56	1294.44	1293.87	1293.21	1292.56	1291.91	1291.20	1291.02
	1.2	Station	4714+74.27	4714+75.63	4714+81.56	4714+88.40	4714+95.29	4715+02.25	4715+09.93	4715+11.80
	1•2	Elevation	1294.57	1294.43	1293.86	1293.21	1292.56	1291.91	1291.20	1291.03
Γ	1.3	Station	4714+77.24	4714+78.71	4714+84.66	4714+91.51	4714+98.41	4715+05.38	47/5+/3.08	47/5+/4.89
	1.5	Elevation	1294.57	1294.43	1293.86	1293.20	1292.55	1291.90	1291.19	1291.03
. [	1.4	Station	4714+80.20	4714+81.79	4714+87.75	4714+94.61	4715+01.54	4715+08.52	47/5+/6.23	47/5+/7.98
ONE	1.	Elevation	1294.58	1294.42	1293.85	1293.20	1292.55	1291.90	1291.19	1291.04
	1.5	Station	4714+83.17	4714+84.88	4714+90.84	4714+97.72	4715+04.66	4715+11.65	4715+19.38	4715+21.06
4/	1.5	Elevation	1294.58	1294.42	/293.85	1293.19	1292.54	1291.90	1291.19	1291.04
SPAN	1.6	Station	47/4+86./3	4714+87.96	4714+93.94	4715+00.83	4715+07.78	4715+14.79	4715+22.53	4715+24.15
,	7.0	Elevation	1294.59	1294.41	1293.84	1293.19	1292.54	1291.89	1291.18	1291.04
	1.7	Station	4714+89.10	4714+91.04	4714+97.03	4715+03.94	47/5+/0.90	4715+17.93	4715+25.68	4715+27.24
	1•1	Elevation	1294.60	1294.41	1293.84	/293./9	1292.54	1291.89	1291.18	1291.04
ſ	1.8	Station	4714+92.06	4714+94.12	47/5+00./3	4715+07.05	47/5+/4.02	4715+21.06	4715+28.83	4715+30.32
		Elevation	1294.60	1294.40	1293.83	1293.18	1292.53	1291.89	1291.18	1291.05
ſ	1.9	Station	4714+95.03	4714+97.21	4715+03.22	4715+10.15	4715+17.15	4715+24.20	47/5+3/.99	47/5+33.4/
		Elevation	1294.60	1294.40	1293.83	1293.18	1292.53	1291.88	1291.18	1291.05
€ Pier	2.0	Station	4714+97.99	4715+00.29	4715+06.32	4715+13.26	4715+20.27	4715+27.34	4715+35.14	4715+36.50
No. /	2.0	Elevation	1294.61	1294.39	1293.82	1293.17	1292.53	1291.88	1291.17	1291.05
	2.1	Station	4715+03.02	4715+05.43	4715+11.48	4715+18.44	4715+25.47	4715+32.56	4715+40.39	4715+41.74
	۲. ۱	Elevation	1294.62	1294.38	1293.82	1293.17	1292.52	1291.88	1291.17	1291.05
Ē	2.2	Station	4715+08.05	4715+10.56	4715+16.63	4715+23.62	4715+30.68	4715+37.79	4715+45.64	4715+46.98
	۷.۲	Elevation	1294.62	1294.38	1293.81	1293.16	1292.52	1291.87	1291.17	1291.06
	2.3	Station	4715+13.07	4715+15.70	4715+21.79	4715+28.81	4715+35.88	4715+43.02	4715+50.89	4715+52.22
	2.J	Elevation	1294.63	1294.37	1293.81	1293.16	1292.51	1291.87	1291.17	1291.06
	2.4	Station	4715+18.10	4715+20.84	4715+26.95	4715+33.99	4715+41.09	4715+48.24	4715+56.15	4715+57.46
OML	2.4	Elevation	1294.64	1294.37	1293.80	1293.15	1292.51	1291.87	1291.16	1291.06
	2.5	Station	4715+23.12	4715+25.98	4715+32.11	4715+39.17	4715+46.29	4715+53.47	4715+61.40	4715+62.70
SPAN	2.J	Elevation	1294.64	1294.36	1293.80	1293.15	1292.51	1291.86	1291.16	1291.06
S I	2.6	Station	4715+28.15	4715+31.12	4715+37.27	4715+44.35	4715+51.50	4715+58.70	4715+66.65	4715+67.94
j	2.0	Elevation	1294.65	1294.36	1293.79	1293.15	1292.51	1291.86	1291.16	1291.06
Ē	2.7	Station	4715+33.18	4715+36.27	4715+42.43	4715+49.54	4715+56.70	4715+63.93	4715+71.90	4715+73.19
	د. ۱	Elevation	1294.65	1294.35	1293.79	1293.15	1292.50	1291.86	1291.16	1291.06
Ī	2.8	Station	4715+38.20	4715+41.41	4715+47.59	4715+54.72	4715+61.91	4715+69.16	4715+77.16	4715+78.43
	2.0	Elevation	1294.65	1294.35	1293.79	1293.14	1292.50	1291.86	1291.16	1291.06
ſ	2.9	Station	4715+43.23	4715+46.55	4715+52.76	4715+59.90	4715+67.11	4715+74.39	4715+82.41	4715+83.67
	<b>L.</b> J	Elevation	1294.66	1294.35	1293.78	1293.14	1292.50	1291.86	1291.16	1291.06
⊈ Pier	3.0	Station	4715+48.25	4715+51.69	4715+57.92	4715+65.09	4715+72.32	4715+79.61	4715+87.66	4715+88.91
No. 2	5.0	Elevation		1294.35	1293.78	1293.14	1292.50	1291.86	1291.16	1291.06

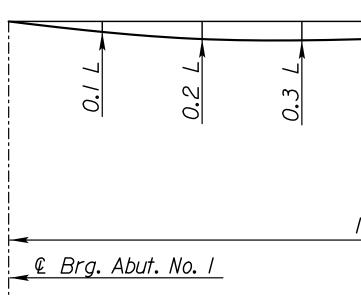
Plotted By: JEHarris Plot Location: File: KTA44-25-SlabElevations.dgn Plot Date: 12-SEP-2024 21:41

				TOF	OF SLAB	ELEVATIONS				
	Tenth Point		Fascia (West)	Beam A	Beam B	Beam C	Beam D	Beam E	Beam F	Fascia (East)
⊈ Pier	3.0	Station	4715+48.25	4715+51.69	4715+57.92	4715+65.09	4715+72.32	4715+79.61	4715+87.66	4715+88.91
No. 2	0.0	Elevation	1294.66	1294.35	1293.78	1293.14	1292.50	1291.86	1291.16	1291.06
	3./	Station	4715+53.41	4715+56.85	4715+63.09	4715+70.28	4715+77.54	4715+84.85	4715+92.92	4715+94.29
	0.1	Elevation	1294.66	1294.34	1293.78	1293.14	1292.50	1291.86	1291.17	1291.05
	3.2	Station	4715+58.56	4715+62.00	4715+68.26	4715+75.48	4715+82.75	4715+90.09	47/5+98./8	4715+99.68
	<b>)</b> •	Elevation	1294.66	1294.34	1293.78	1293.14	1292.50	1291.86	1291.17	1291.05
	3.3	Station	4715+63.72	4715+67.15	4715+73.43	47/5+80.67	4715+87.97	4715+95.32	4716+03.45	4716+05.06
	5.5	Elevation	1294.66	1294.34	1293.78	/293./4	1292.50	1291.87	1291.17	1291.05
FE	3.4	Station	4715+68.87	4715+72.30	4715+78.60	4715+85.86	47/5+93./8	4716+00.56	4716+08.71	4716+10.45
THREE	5.7	Elevation	1294.66	1294.34	1293.78	/293./4	1292.51	1291.87	1291.17	1291.04
	3.5	Station	4715+74.02	4715+77.45	4715+83.77	4715+91.05	4715+98.39	4716+05.80	4716+13.96	4716+15.83
4N	5.5	Elevation	1294.66	1294.34	1293.78	1293.15	1292.51	1291.87	1291.18	1291.04
SPAN	3.6	Station	4715+79.18	4715+82.61	4715+88.95	4715+96.25	4716+03.61	4716+11.03	4716+19.22	4716+21.22
- )	5.0	Elevation	1294.66	1294.34	1293.78	/293./5	1292.51	1291.88	1291.18	1291.03
	3.7	Station	4715+84.33	4715+87.76	4715+94.12	4716+01.44	4716+08.82	4716+16.27	4716+24.48	4716+26.60
-	J.1	Elevation	1294.66	1294.34	1293.79	1293.15	1292.52	1291.88	1291.19	1291.02
	3.8	Station	4715+89.48	4715+92.91	4715+99.29	4716+06.63	4716+14.03	4716+21.50	4716+29.74	4716+31.99
	J.0	Elevation		1294.35	1293.79	/293./5	1292.52	1291.89	1291.19	1291.02
	3.9 -	Station	4715+94.64	4715+98.06	4716+04.46	4716+11.82	4716+19.25	4716+26.73	4716+35.00	4716+37.37
		Elevation	1294.65	1294.35	1293.79	1293.16	1292.52	1291.89	1291.20	1291.01
⊈ Pier	10	Station	4715+99.79	4716+03.21	4716+09.63	4716+17.01	4716+24.46	4716+31.97	4716+40.25	4716+42.76
No. 3	4.0	Elevation		1294.35	1293.80	1293.16	1292.53	1291.90	1291.21	1291.00
	A 1	Station	4716+02.90	4716+06.26	4716+12.69	4716+20.08	4716+27.54	4716+35.07	4716+43.36	4716+46.02
	4.1	Elevation		1294.35	1293.80	1293.17	1292.53	1291.90	1291.21	1290.99
	4.0	Station	4716+06.02	4716+09.31	4716+15.75	4716+23.16	4716+30.63	4716+38.16	4716+46.47	4716+49.28
	4.2	Elevation		1294.36	1293.80	1293.17	1292.54	1291.90	1291.22	1290.99
	1 2	Station	4716+09.13	4716+12.36	4716+18.81	4716+26.23	4716+33.72	4716+41.26	47/6+49.59	4716+52.54
	4.3	Elevation		1294.36	1293.80	1293.17	1292.54	1291.91	1291.22	1290.98
0-	AA	Station	47/6+/2.25	4716+15.41	4716+21.87	4716+29.30	4716+36.80	4716+44.36	4716+52.70	47/6+55.80
FOUR	4.4	Elevation		1294.36	1293.81	1293.17	1292.54	1291.91	1291.23	1290.98
FC		Station	47/6+/5.36	4716+18.46	4716+24.93	4716+32.38	4716+39.89	47/6+47.46	47/6+55.8/	4716+59.06
NI	4.5	Elevation		1294.36	1293.81	/293./8	1292.55	1291.92	1291.23	1290.97
SPAN	4.0	Station	4716+18.47	4716+21.51	4716+27.99	47/6+35.45	4716+42.97	4716+50.55	4716+58.92	4716+62.32
~)	4.6	Elevation		1294.37	1293.81	/293./8	1292.55	1291.92	1291.24	1290.96
	A 7	Station	4716+21.59	4716+24.56	4716+31.05	4716+38.52	47/6+46.05	4716+53.65	4716+62.03	4716+65.58
	4.7	Elevation		1294.37	1293.82	1293.19	1292.56	1291.93	1291.24	1290.96
	4.0	Station	4716+24.70	4716+27.61	47/6+34.//	4716+41.59	4716+49.14	4716+56.75	4716+65.14	47/6+68.84
	4.8	Elevation		1294.37	1293.82	1293.19	1292.56	1291.93	1291.25	1290.95
		Station	4716+27.81	4716+30.66	4716+37.17	4716+44.66	4716+52.22	4716+59.84	4716+68.25	4716+72.10
	4.9	Elevation		1294.38	1293.82	1293.19	1292.57	1291.94	1291.25	1290.94
(). Rra		Station	4716+30.93	4716+33.71	4716+40.23	4716+47.74	4716+55.30	4716+62.94	4716+71.35	4716+75.35
∉ Brg. Abut. No. 2	5.0	Elevation		1294.38	1293.83	1293.20	1292.57	1291.94	1291.26	1290.93

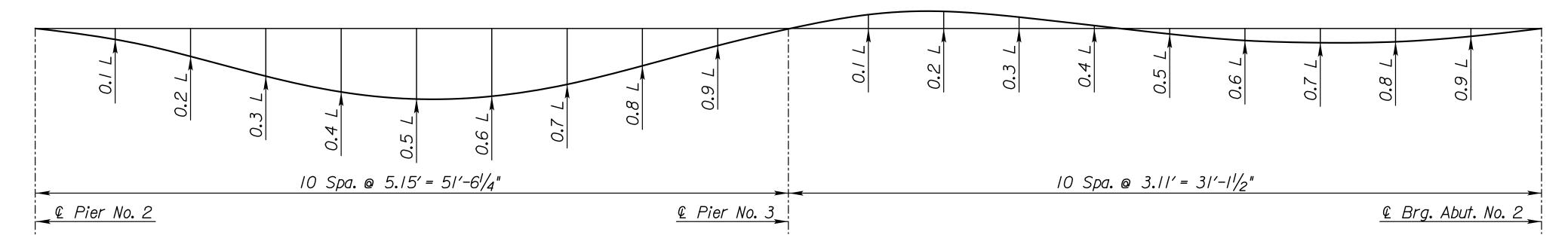
STATE	PROJECT NO.	YEAR	SHEET NO.	TOTAL SHEETS
KANSAS	8082	2024	53	134

4							
3							
2							
NO.	DATE		REVI	SIONS		BY	APP'D
Br.	No. 43	ANSAS .930 ne Adway s	3				
SHEET	NO. OF	SCALE		APP'D			
DESIGN	<u>IED JW</u>	M DETAILED	JTK	QUANTI	TIES	CADD	
DESIGN	ICK. JM	IB DETAIL CK	. JWM	QUAN.	CK.	CADD CK.	•

									DEA	D LOAD	DEFLECT	IONS									
Beam	€ Brg. Abut. No. I	0.1 L	0.2 L	0.3 L	0.4 L	0.5 L	0.6 L	0.7 L	0.8 L	0.9 L	⊈ Pier No. I	0.1 L	0.2 L	0.3 L	0.4 L	0.5 L	0.6 L	0.7 L	0.8 L	0.9 L	© Pier No. 2
A	0.000	-0.00/	-0.00/	-0.00/	-0.00/	-0.00/	0.000	0.00/	0.001	0.00/	0.000	-0.004	-0.009	-0.0/4	-0.0/7	-0.017	-0.016	-0.0/2	-0.007	-0.002	0.000
В	0.000	-0.00/	-0.00/	-0.00/	-0.00/	-0.00/	0.000	0.000	0.00/	0.00/	0.000	-0.002	-0.006	-0.009	-0.0//	-0.0//	-0.0/0	-0.007	-0.004	-0.00/	0.000
С	0.000	-0.00/	-0.00/	-0.00/	-0.00/	-0.00/	0.000	0.000	0.00/	0.00/	0.000	-0.002	-0.006	-0.009	-0.0//	-0.0//	-0.0/0	-0.008	-0.004	-0.00/	0.000
D	0.000	-0.00/	-0.00/	-0.00/	-0.00/	-0.00/	0.000	0.000	0.00/	0.00/	0.000	-0.002	-0.006	-0.009	-0.0//	-0.0//	-0.0/0	-0.008	-0.004	-0.00/	0.000
Ε	0.000	-0.00/	-0.00/	-0.00/	-0.00/	-0.00/	0.000	0.000	0.00/	0.00/	0.000	-0.003	-0.006	-0.009	-0.0//	-0.0/2	-0.0/0	-0.008	-0.005	-0.002	0.000
F	0.000	-0.00/	-0.001	-0.002	-0.002	-0.002	-0.00/	0.000	0.000	0.00/	0.000	-0.003	-0.007	-0.0//	-0.0/4	-0.0/4	-0.0/3	-0.0/0	-0.005	-0.002	0.000
		0.1 L	0.2 L	0.3 L	0.4 L	0.5 L	0.6 L	0.7 L	0.8 L	0.9 L		0.1 L	0.2 L	0.3 L	0.4 L	0.5 L	0.6 L	0.7 7	0.8 L	7 6.0	
		0.1 L	0.2 L	0	14.0 10 Spa. @		I	0.7 L	0.8 L	0.9 L		0.1 L		0.3 L	0	7 5.03' =	I	0.7 T	0.8 L	7 6.0	



	DEAD LOAD DEFLECTIONS																				
Beam	⊈ Pier No. 2	0.1 L	0.2 L	0.3 L	0.4 L	0.5 L	0.6 L	0.7 L	0.8 L	0.9 L	⊈ Pier No. 3	0.1 L	0.2 L	0.3 L	0.4 L	0.5 L	0.6 L	0.7 L	0.8 L	0.9 L	€ Brg. Abut. No. 2
A	0.000	-0.002	-0.007	-0.0/3	-0.017	-0.0/9	-0.0/8	-0.0/5	-0.0/0	-0.004	0.000	0.00/	0.00/	0.00/	0.000	-0.00/	-0.00/	-0.00/	-0.00/	-0.00/	0.000
В	0.000	-0.00/	-0.004	-0.008	-0.0/0	-0.0//	-0.0//	-0.009	-0.006	-0.003	0.000	0.00/	0.00/	0.000	0.000	-0.00/	-0.00/	-0.00/	-0.00/	-0.00/	0.000
С	0.000	-0.00/	-0.004	-0.008	-0.0/0	-0.0/2	-0.011	-0.009	-0.006	-0.003	0.000	0.00/	0.001	0.000	0.000	-0.00/	-0.00/	-0.00/	-0.00/	-0.00/	0.000
D	0.000	-0.00/	-0.004	-0.008	-0.0/0	-0.0//	-0.011	-0.009	-0.006	-0.003	0.000	0.00/	0.001	0.000	0.000	-0.00/	-0.00/	-0.00/	-0.00/	-0.00/	0.000
E	0.000	-0.002	-0.005	-0.008	-0.0//	-0.0/2	-0.012	-0.0/0	-0.006	-0.003	0.000	0.00/	0.001	0.000	0.000	-0.00/	-0.00/	-0.00/	-0.00/	-0.00/	0.000
F	0.000	-0.002	-0.007	-0.0//	-0.0/4	-0.0/6	-0.015	-0.0/2	-0.008	-0.003	0.000	0.00/	0.000	0.000	-0.00/	-0.002	-0.002	-0.002	-0.002	-0.00/	0.000



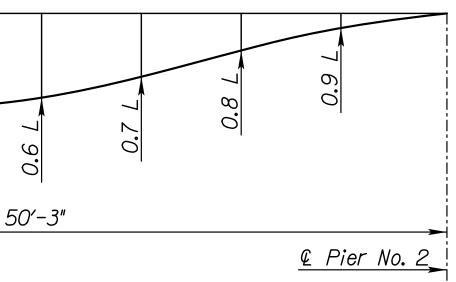
Plotted By: JEHarris	Plot Location:
File: KT A44-26-Deflections.dgn	
Plot Date: 12-SEP-2024 21:41	

# BEAM DEAD LOAD DEFLECTION DIAGRAM

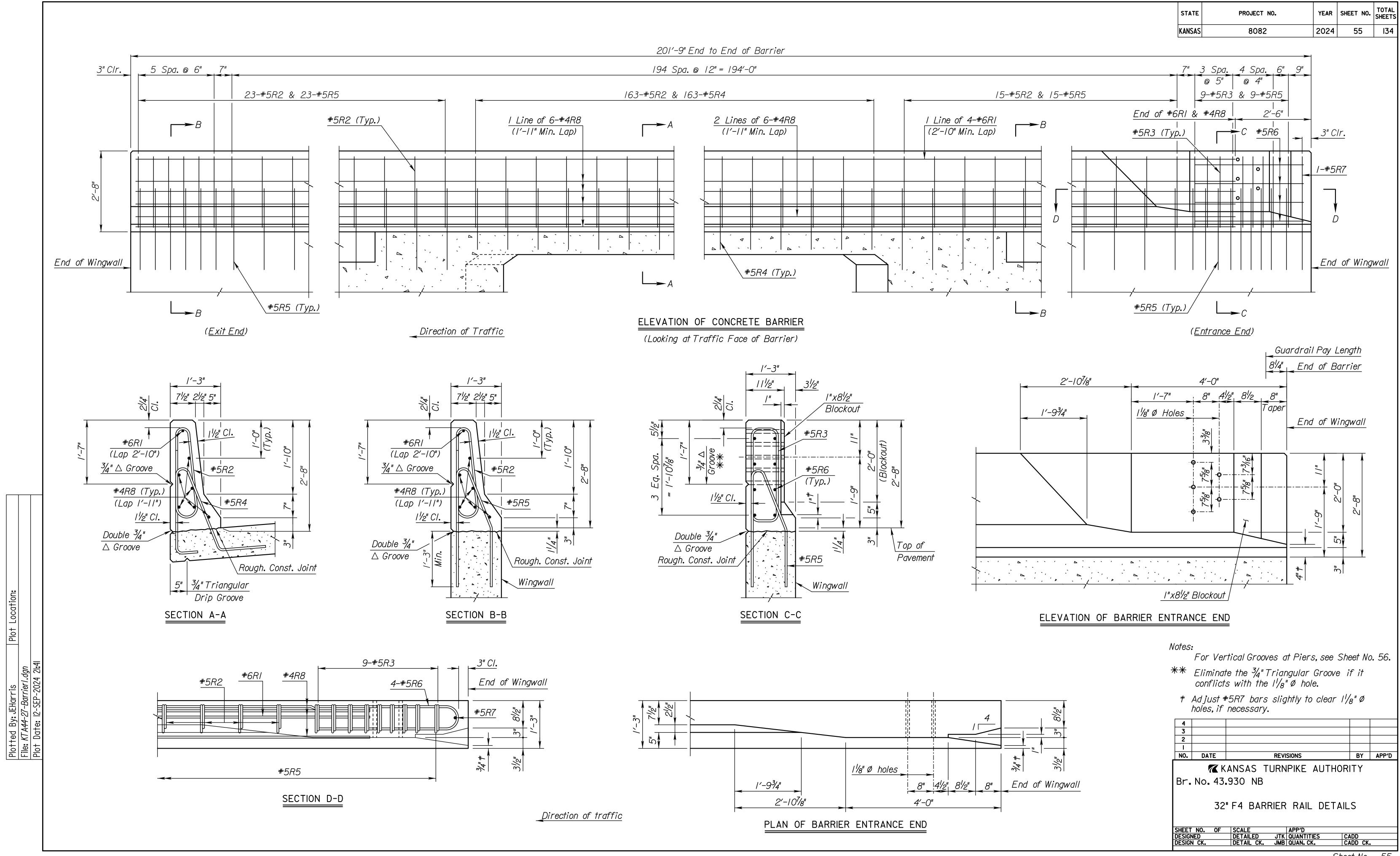
Ordinates are in feet and are at tenth points of spans, measured along & Beams.

DEFLECTION NOTES: Do not camber the new steel beams. Any natural mill camber that the beams have retained shall be placed up. Dead Load Deflection ordinates shown represent the amount of deflection due to the slab pour and barrier rails. Provide for beam deflections by adding concrete dead load deflections to plan grade. Increase or decrease the depth of concrete fillets over the beams, based on field surveys, to obtain the required roadway surface elevations.

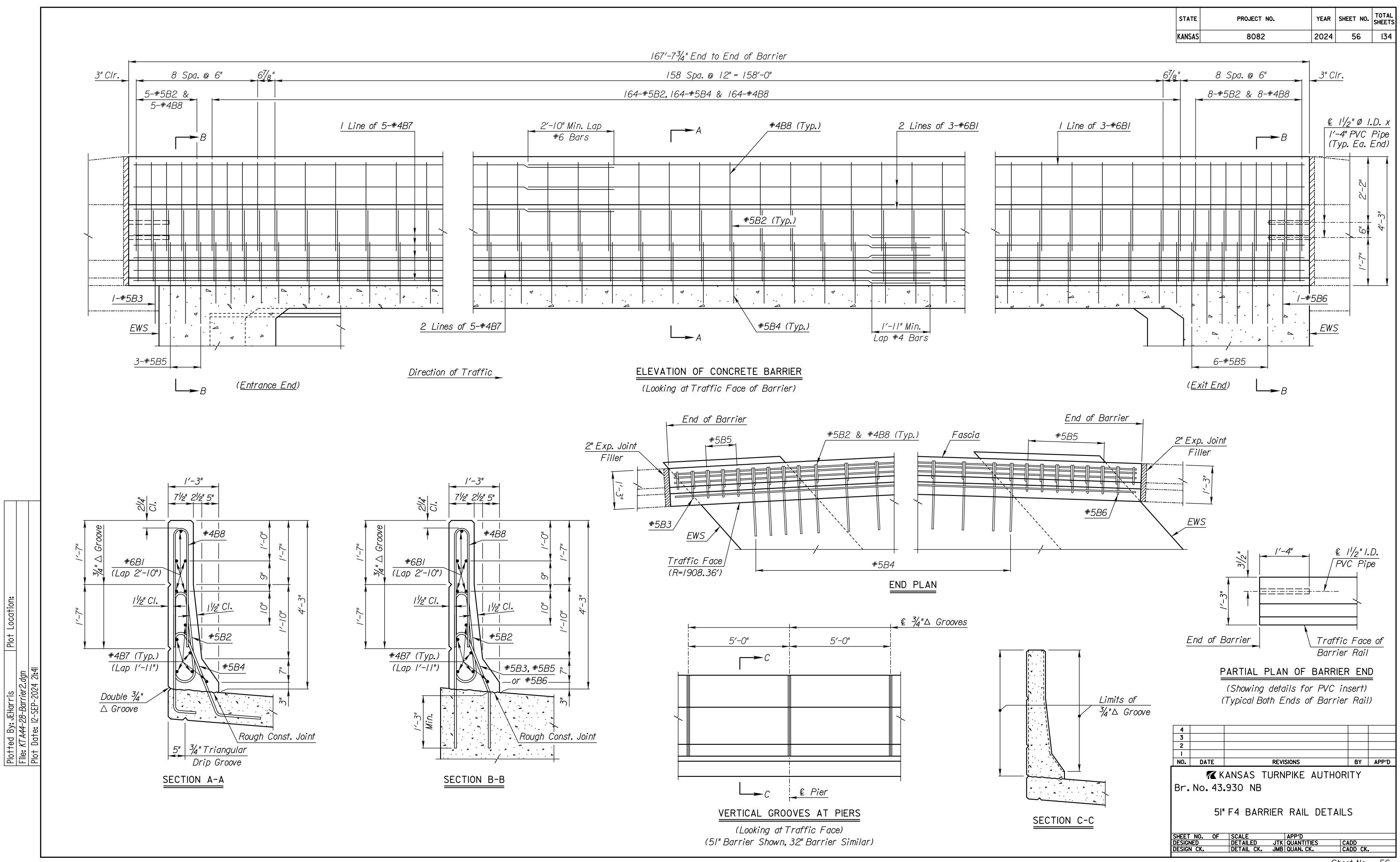
STATE	PROJECT NO.	YEAR	SHEET NO.	TOTAL SHEETS
KANSAS	8082	2024	54	134



4											
3											
2											
NO. DATE REVISIONS BY	APP'D										
KANSAS TURNPIKE AUTHORITY Br. No. 43.930 NB DEAD LOAD DEFLECTIONS											
SHEET NO. OF SCALE APP'D											
DESIGNED JWM DETAILED JTK QUANTITIES CADD											
DESIGN CK. SHH   DETAIL CK. JWM   QUAN. CK.   CADD CK.											



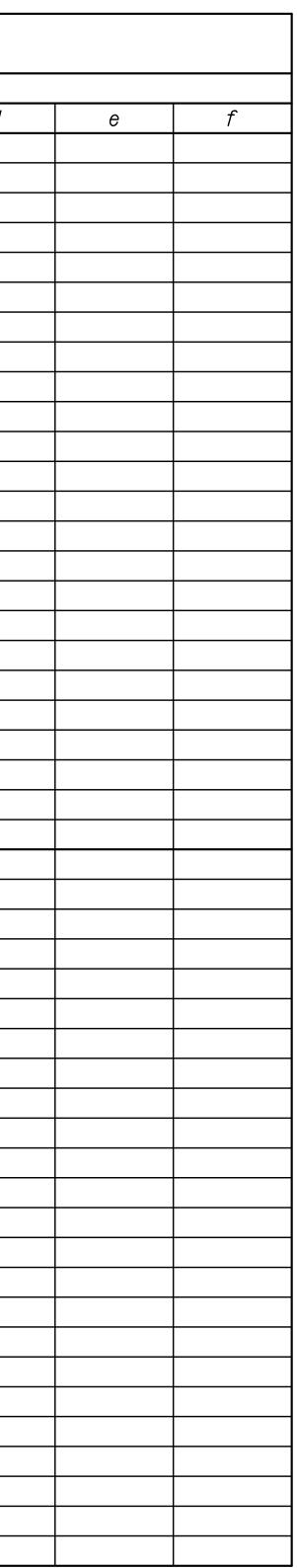
Sheet No. 55

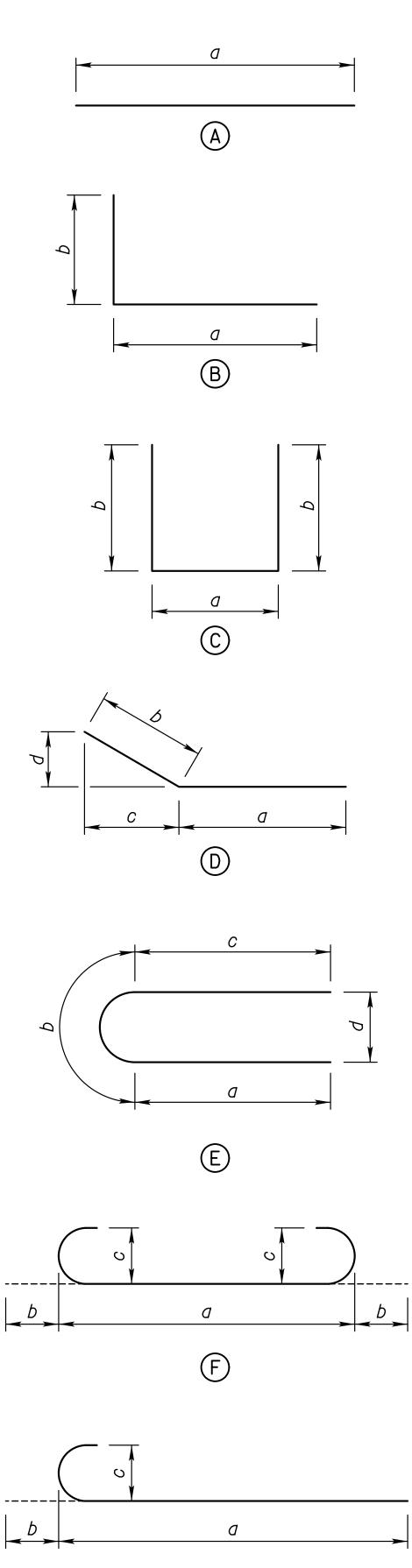


Sheet No. 56

Plotted By; JEHarris	Plot Location:
File: KTA44-29-Barlistl.dgn	
Plot Date: 12-SEP-2024 21:42	

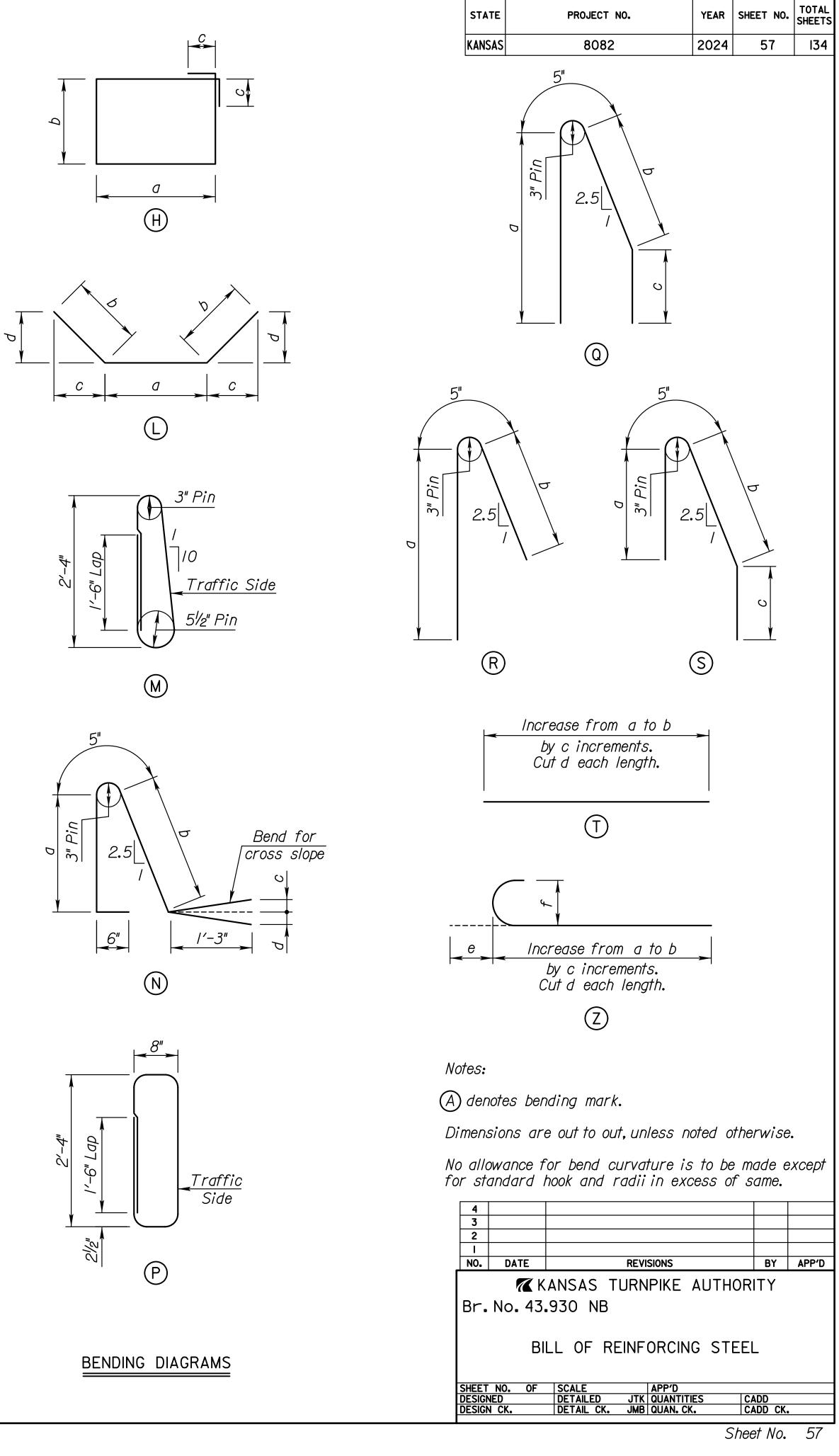
					BILL		NFORCING DE 60	STEEL	
ľ	Design	Bending						Dimer	nsiol
	Mark	Mark	Size	No.	Length	a	b	С	
	SA/	A	8	8	57′-11″	57′-11″			
-	SA25	A	7	6	7'-9"	7'-9"			
	<u> </u>			<u> </u>					
$\mathbf{r}$	SA3	A	5	6	57'-11"	57'-11"			
Ì	SA4	A	5	2	37′-9" 27′-0"	37'-9" 27'-0"			
	SA5 SA6	A A	5 5	2	<u> </u>	27 -0 16'-3"			
		A	5		5′-6″	5′-6″			
╞	SA/3	C A	5	12	<u> </u>  8'-4"	3'-6"	7′-5″	7′-5″	
	SA14	C	5	//	20'-4"	3'-6"	<i>8′–5</i> ″	<i>r 5</i> <i>8′</i> –5″	
ļ	SA/5	C	5	/3	22'-2"	3'-6"		9'-4"	
┇┝	SA16	C	5	10	23'-10"	3'-6"	10'-2"	10'-2"	
	SAI7	C	5	2	4'-4"	3'-6"	6'-10"	4'-0"	
┋┝	SA18	С С	5	2	/5′-8″	3'-6"	7′-6″	4'-8"	
	SA19	C	5	/	17'-0"	3'-6"	8'-2"	5′-4″	
	SA20	С	5	51	5'-2"	3′-6″	10"	/0"	
	SA27	A	5	5	10'-2"	10'-2"			
ľ	SA28	A	5	11	7′-8″	7′-8″			
ľ	SA29	A	5	5	6′-8″	6′-8″			
┨	NA/	A	8	16	33′-9″	33′-9″			
	NA26	A	7	6	///-6"	//′-6″			
ŀ	NA3	A	5	12	32'-10"	32'-10"			
$\left[\right]$	NA4	A	5	2	40′-3″	40′-3″			
	NA5	A	5	2	29′-6″	29′-6″			
	NA6	A	5	2	/8′-9″	18'-9"			
	NA7	A	5	4	8'-0"	8'-0"			
	NA/3	C	5	12	/8′-4″	3'-6"	7′-5″	7′-5″	
2  - -	NAI4	С	5	11	20'-4"	3'-6"	8′-5″	8′-5″	
┦	NAI5	C	5	/3	22'-4"	3'-6"	9′-5″	9′-5″	
J	NA/6	C	5	12	24'-0"	3'-6"	10'-3"	10'-3"	
2	NAI7	C	5	2	14'-6"	3'-6"	7'-0"	4'-0"	
╤┝	NAI8	C	5	2	15'-9"	3'-6"	7'-7"	4'-8"	
Į	NA19	C	5	/	17'-0"	3'-6"	8'-2"	5'-4"	
	NA20	C	5		/9'-3"	3'-6"	8'-9"	6'-0"	
Į	NA21	C	5	<u>54</u>	5'-2"	3'-6"	10"	10"	
┠	NA28	A	5	5	9'-9"	9'-9" 7'-8"			
┠	NA29 NA30	A A	5 5	 	7′-8" 6′-8"	7′-8" 6′-8"			
┠	IVAJU		<u>َن</u>	3		0-0			
┠									

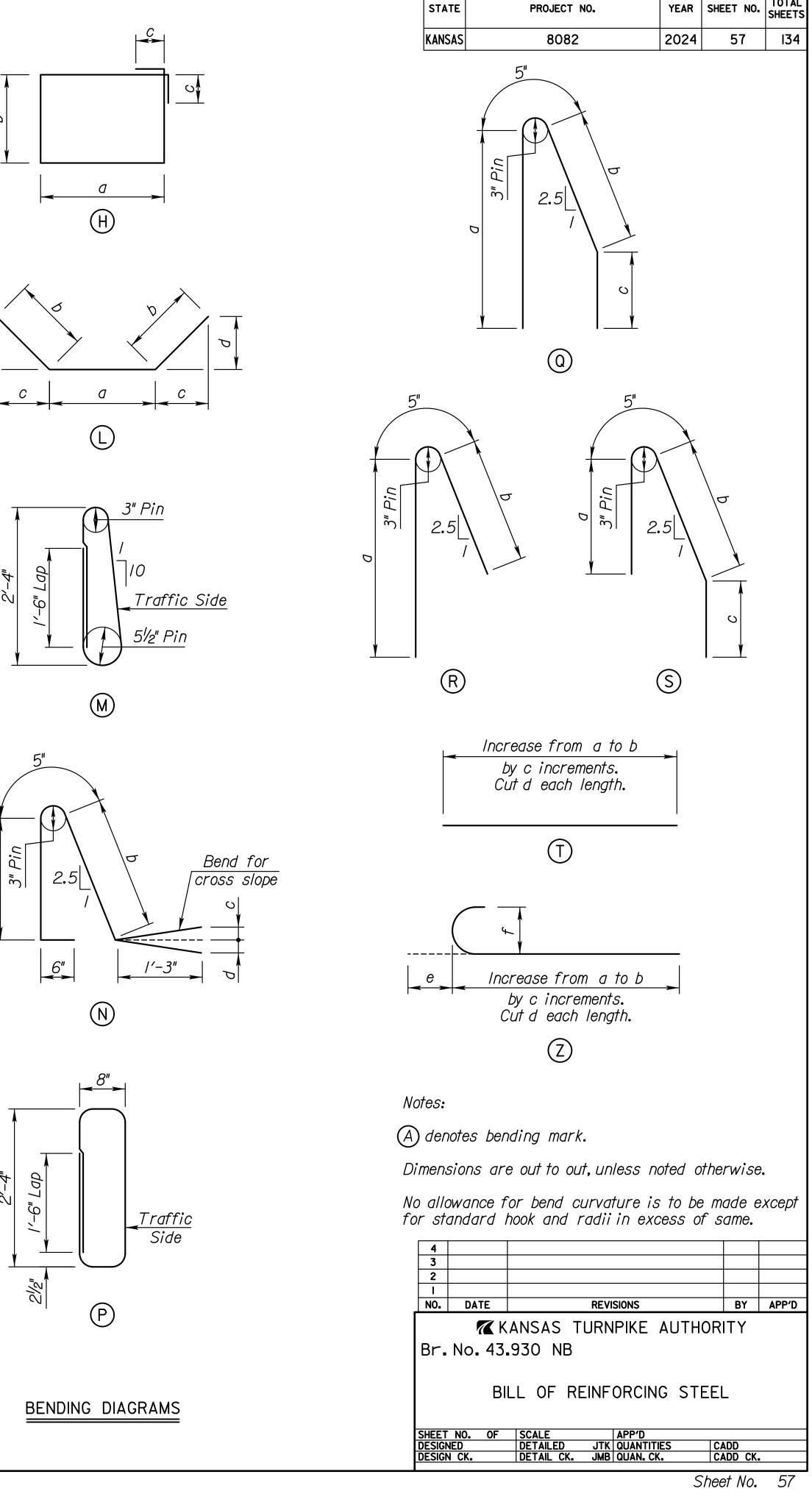


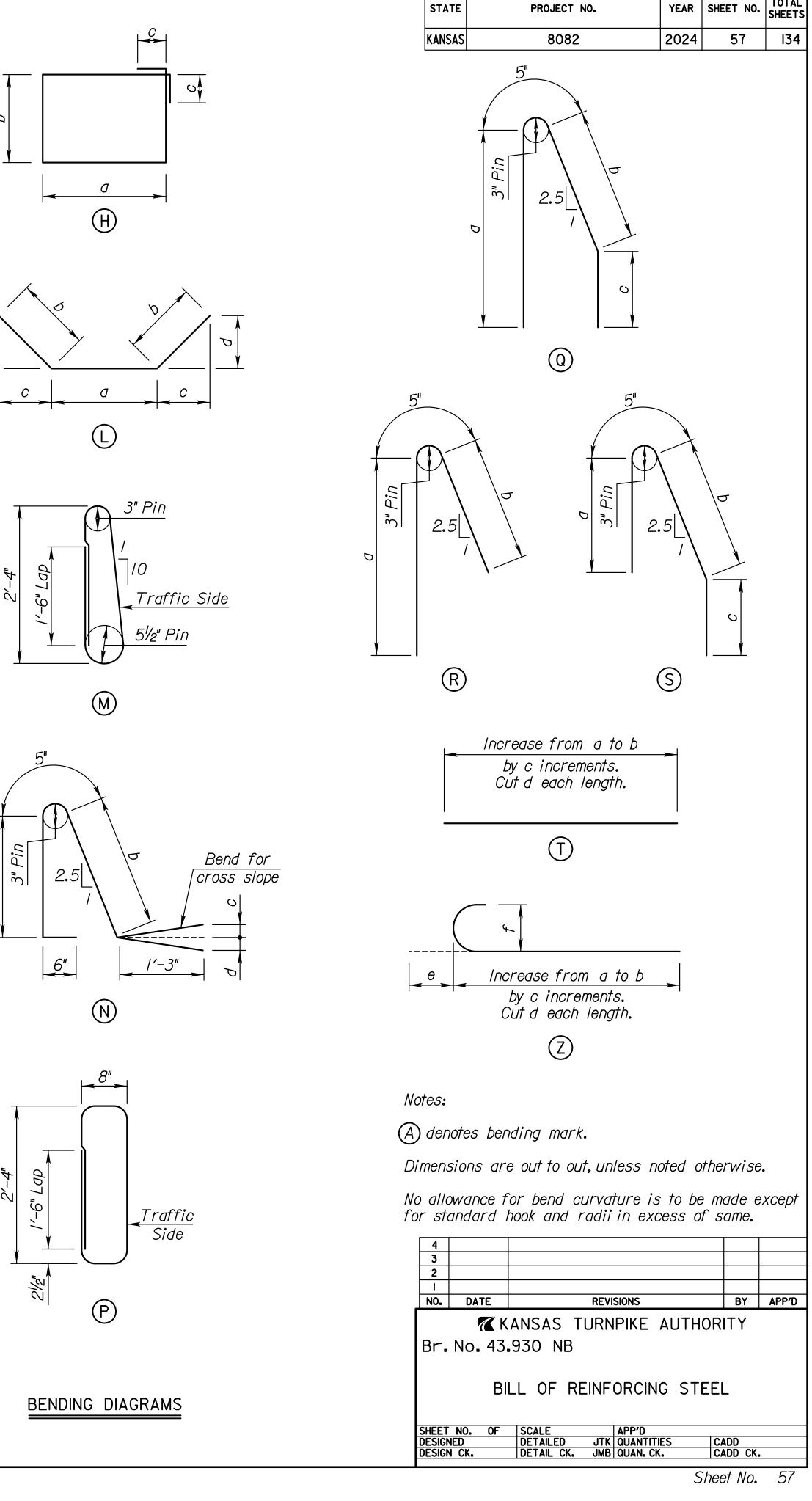


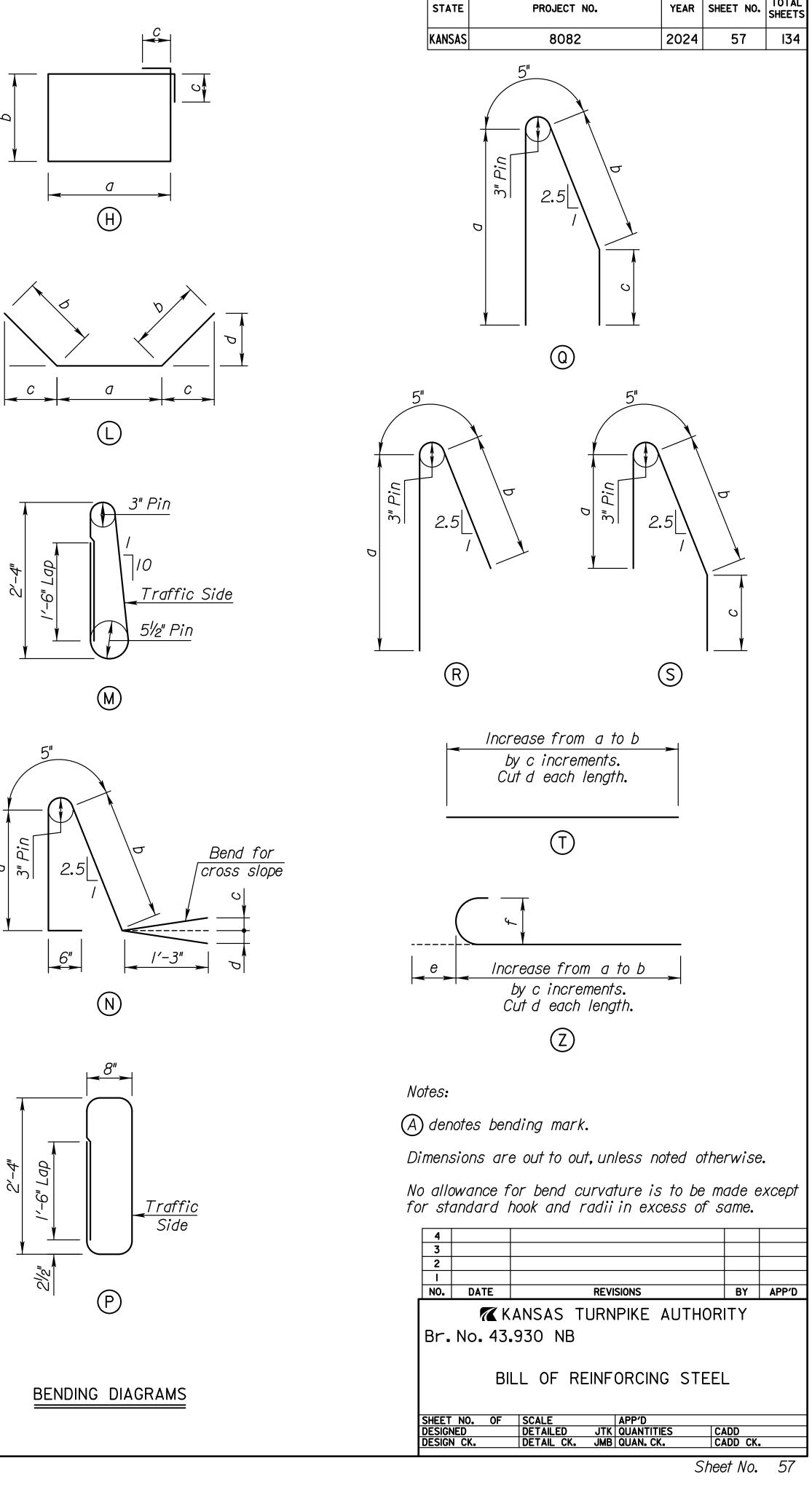
G

9





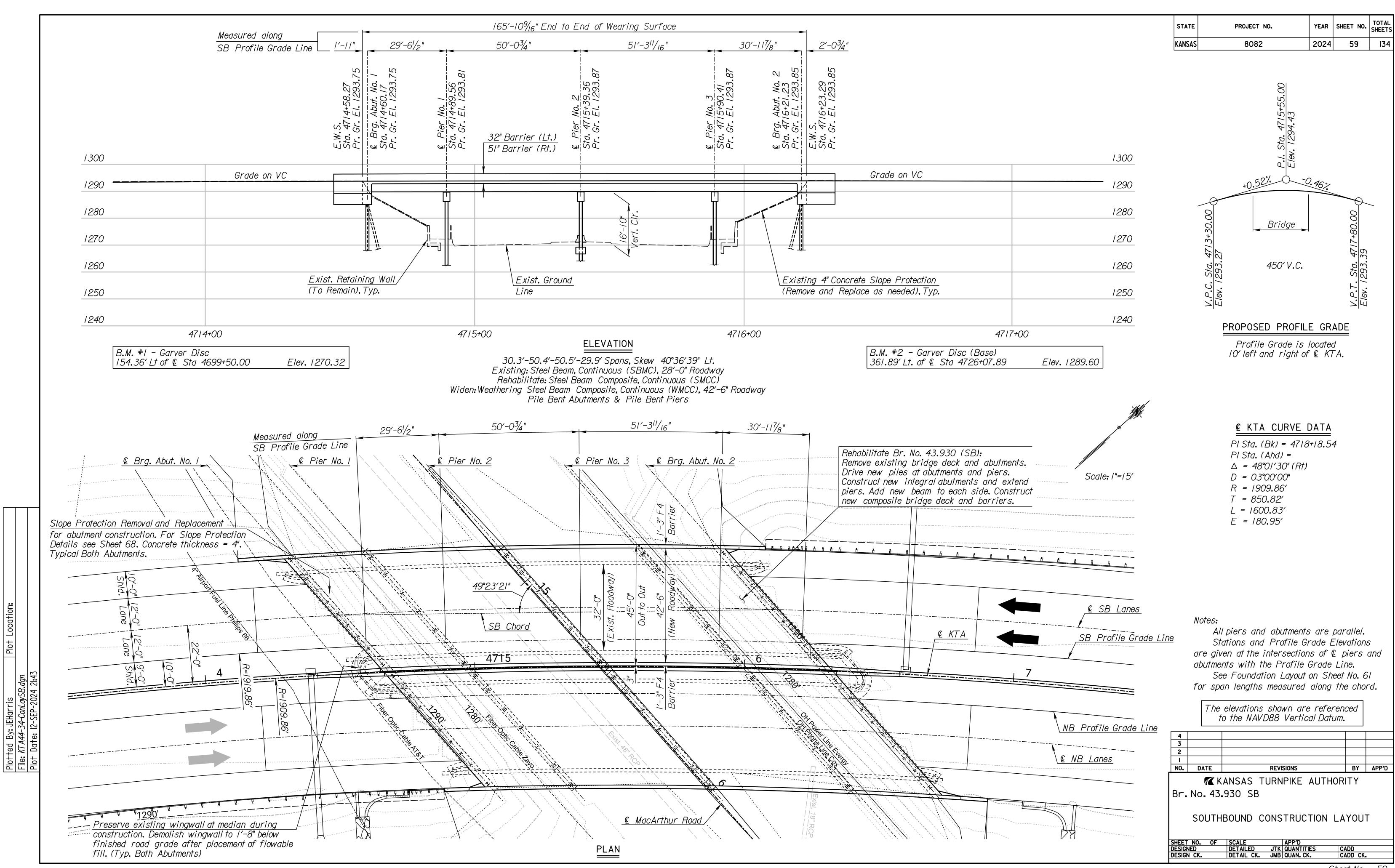




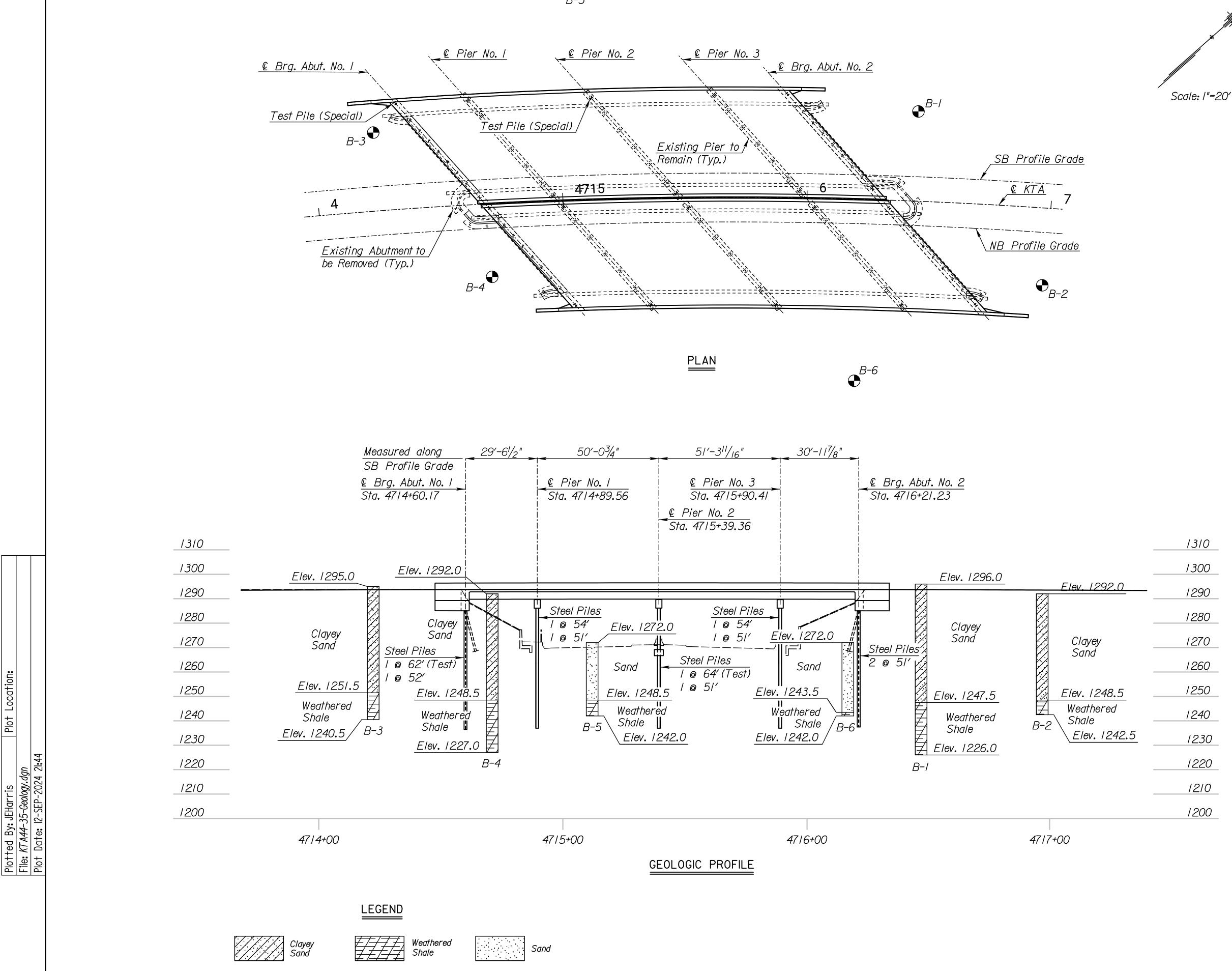
				BILL		NFORCING DE 60	STEEL			
Design	Bending						Dimen	nsion		
Mark	Mark	Size	No.	Length	а	Ь	С	d	е	f
PBI	F	8	4	///-6"	9′-8″	//"	//"			
PB2	A	8	4	9′-8″	9′-8″					
PB3	F	8	4	9′-6″	7′-8″	//"	//"			
PB4	A	8	4	7′-8″	7′-8″					
				24 01	24 0#					
	A	6	12	3'-0"	3'-0"					
PDI PB5	С	5	38	8'-8"	2'-2"	3'-3"	3′-3″			
- <u>PB6</u>	A	4	6	9′-8″	9′-8″					
PB7	A	4	8	7'-8"	7'-8"					
	С	4	14	4'-6"	2'-0"	/′–3″	/′–3"			
PBI	F	8	4	//′-6″	9′-8″	//"	//"			
PB2	A	<u> </u>	4	9′-8″	9-8 9′-8″	11				
PB3	F F	<u> </u>	4	9'0 9'-6"		//"	//"			
PB4	A	8	4	7′-8″	7′-8″					
		~	,							
	A	6	20	3'-0"	3'-0"					
C PFI	A	6	6	9′-2″	9′-2″					
PDI PFI PF2	A	6	6	8'-7"	8'-7"					
J <i>PB5</i>	С	5	38	8′-8"	2'-2"	3′-3″	3′-3″			
PB6	A	4	6	9′-8″	9′-8″					
<i>PB7</i>	A	4	8	7′-8″	7′-8″					
- PB8	С	4	4	4′-6″	2'-0"	/′-3″	/′-3″			
PF3	H	4	19	//′-/″	3′-2″	2'-0"	41/2"			
PF4	С	4	6	5′-7″	3'-/"	'-3"	/′-3"			
						1.111				
PBI PB2	F A	<u> </u>	4	//′-6" 9′-8"	9′-8″ 9′-8″	//"	//"			
PB2 PB3	A F	<u> </u>	4	9-8 9'-6"	9-8 7'-8"	//"	//"			
PB4	F     A	 	4	9-6 7'-8"	7'-8"	11				
		0				<u> </u>			<u> </u>	
PDI	A	6	12	3'-0"	3'-0"					
PDI PB5	С	5	38	8'-8"	2'-2"	3′-3″	3'-3"			
PB6	A	4	6	9′-8″	9′-8″					
<i>PB7</i>	A	4	8	7'-8"	7'-8"					
	С	4	4	4′-6"	2'-0"	'-3"	/′-3″			

Plotted By: JEHarris Plot Location: File: *KTA44-30-Barlist2.dgn* Plot Date: 12-SEP-2024 21:42

				BILL		NFORCING	STEEL				KANSAS	8082	2024	SHEET NO.	
					GRA	DE 60									
esign Iark	Bending Mark	Size	No.	Length		6	Dimer			f					
5A2	A	8	5	58'-0"	а 58'-0"	D	С	d	e	/					
VA2	A	8	10	33′-9″	33′-9″										
<u>, ,</u>															
A23	A	7	5	12'-6"	12'-6"										
A24	A	7	4	10′-6″	10′-6″										
A24	A	7	5	/ 3′-9″	/ 3′-9"										
425	A	7	4	/6′-2″	16'-2"										
BI	A	6	15	57′-10″	57′-/0″										
RI	A	6	4	51'-11"	51'-11"										
SI	A	6	/34	20'-0"	20'-0"										
B2	<u>M</u>	5	177	6'-6"	6'-6"	11 21									
B3 B4	R N	<u> </u>	/ /64	4′-3" 5′-11"	2′-7"  ′-9"	/'-3" 2'-0"		11/4"							
84 85	 	<u> </u>	- 164 - 9	5'-9"	2'-7"	<u>2'-0'</u> /'-6"	/ <i>'3"</i>	174		+					
35 36	S	5			/′-/″	//-6"	/'-3"								
R2	M	5	201	6'-6"											
R3	Р	5	9	7′-6″											
R4	N	5	163	5'-//"	/'-9"	2'-0"	11/4"								
R5	Q 	5	47	5'-11"	2'-8" 21 23/ 11	/'-6"	/'-4" 2/ 23/ #	<u></u>		<u> </u>					
R6 R7	E A	<u> </u>	4	7′-5″ 3′-10″	3'-3 <sup>3</sup> /4" 3'-10"	9 <sup>1</sup> /2"	3′-3 <sup>3</sup> ⁄4″	6 <sup>1</sup> /2"		<u> </u>					
R7 S2	A A	<u> </u>	7 270	57'-6"	57'-6"										
52 S3	A	5	54	43'-9"	43′-9"										
55 S4	F	5	249	45'-10"	44'-8"	7"	5"								
S5	A	5	250	44′-8″	44′-8"										
S6	Ζ	5	71	VARIES	2'-8"	44′-8"	7 <sup>3</sup> / <sub>16</sub> "	/	7"	5"					
S7	Z	5	84	VARIES	2'-4"	44'-6"	6 <sup>1</sup> /8"	/	7"	5"					
S8 S9	/ 	<u> </u>	71 84	VARIES VARIES	2′-6″ 2′-1″	44′-6" 44′-3"	7 <sup>3</sup> /16" 6 <sup>1</sup> /8"	/ /		<u> </u>					
59 510	 	<u> </u>	644	6'-10"	2 -1 6'-3"	44 -3 7"	5"	/		<u> </u>					
S//	B	5	90	/8′-0″	16'-0"	2'-0"									
5A8	A	5	6	58'-0"	58′-0"										
5A9	A	5	2	43′-3″	43′-3"										
AIO	A	5	2	20'-0"	20'-0"										
A//	A	5	6	12'-6"	/2'-6" 7'-6"										
AI2 A21	A C	<u> </u>	2 46	7′-6" 9′-10"	7′-6" 3′-6"	3'-2"	3'-2"								
A22 A22	B	5	5	7'-4"	3′-6"	3'-10"									
A26	A	5	4	/9′-5″	/9′-5″										
A30	A	5	20	3'-2"	3'-2"										
/A8	A	5	12	32'-10"	32'-10"					ļ					
1A9	A	5	2	45'-3"	45′-3″					<u> </u>					
AIO 'AII	A A	<u> </u>	2	22'-2" 12'-6"	22'-2" 12'-6"										
A/2	A	5	2	/2-0"	10'-0"										
A22	C	5	48	9'-/0"	3′-6"	3'-2"	3'-2"								
A23	В	5	6	7'-4"	3′-6"	3′-10″									
A27	A	5	4	/9′-9″	/9′-9″							1			-
A31	<u> </u>	5	22	3'-2"	3'-2"					ļ	4 3				ŀ
B7	A	4	30	35′-1″	35′-1″					<u> </u>	2				╞
B7 B8	E A	4	177	6'-1"	2'-9"	7"	2'-9"	41/2"			NO. DATE	REVISION		BY	Ĺ
78	A	4	36	34'-10"	34'-10"	'		'12				KANSAS TURNPI	KE AUTHO	DRITY	
											Br. No. 43	9.320 NR			
											В	ILL OF REINFOR	CING STE	EL	
											I				



Sheet No. 59



Location:

Plot



STATE	PROJECT NO.	YEAR	SHEET NO.	TOTAL SHEETS
KANSAS	8082	2024	60	134

### PILING:

HPI2x53 Piles shall be used at the abutments. HPI4xI02 Piles shall be used at the piers. All new piles shall use case steel pile points. All steel piles will be Grade 50.

Drive all piling to penetrate the mantle and achieve bearing in the weathered shale. Once sufficient resistance and penetration into competent bedrock material are achieved, driving must cease to avoid damage to the pile. Final pile tip elevations should be determined in the field using resistance calculations.

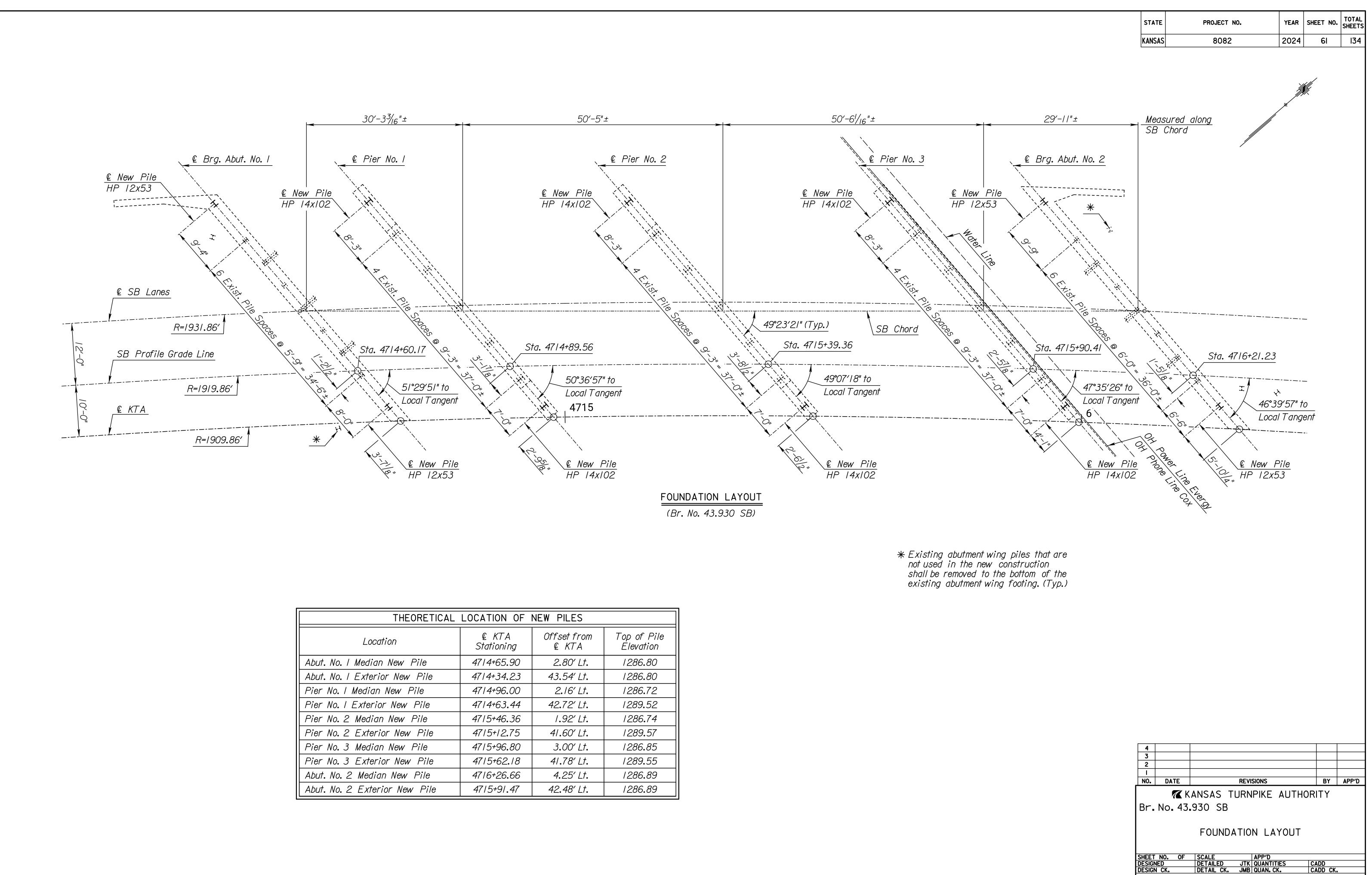
TEST PILE (SPECIAL):

One Test Pile (Special) shall be driven at Abutment No. I and Pier No. 2 as shown. Test piles shall be driven prior to production piles and furnished 10 feet longer than estimated tip elevations of the production piles shown in the plans. Test piles shall remain in place and be used as production piles. All restrikes should be performed a minimum of 24 hours after the initial advancement of the pile has ceased.

PILE DRIVING ANALYZER (PDA): All PDA testing for this project shall be performed by an independent testing firm to be hired by the Contractor. PDA testing shall be performed on each Test Pile (Special) to confirm nominal compressive resistance and develop driving criteria for production piles.

1310						
1300						
1290						
1280						
1270						
1260						
1250	No	tes:				
1240				Top of Pile Ele	evations,	see
1230			-	Sheet No. 61.		
1220	fre	om notes c	obtained in	wn on these plai the field and r	represen	nt the
1210	Ex	ploration F	Report (May	ole. Copies of the (, 2024) are avai biddoro at the k	ilable fo	
1200			•	bidders at the k ce in Wichita, Ka		
		4 3				
		2				<u> </u>
	N	O. DATE		REVISIONS	BY	APP'D
		77 K	ANSAS T	URNPIKE AUTH	ORITY	
	В	r.No.43.	930 SB			
			ENGINEE	RING GEOLOGY		
		EET NO. OF SIGNED	SCALE DETAILED	APP'D JTK QUANTITIES		
		SIGN CK.	DETAIL CK.	JMB QUAN. CK.	CADD CK	

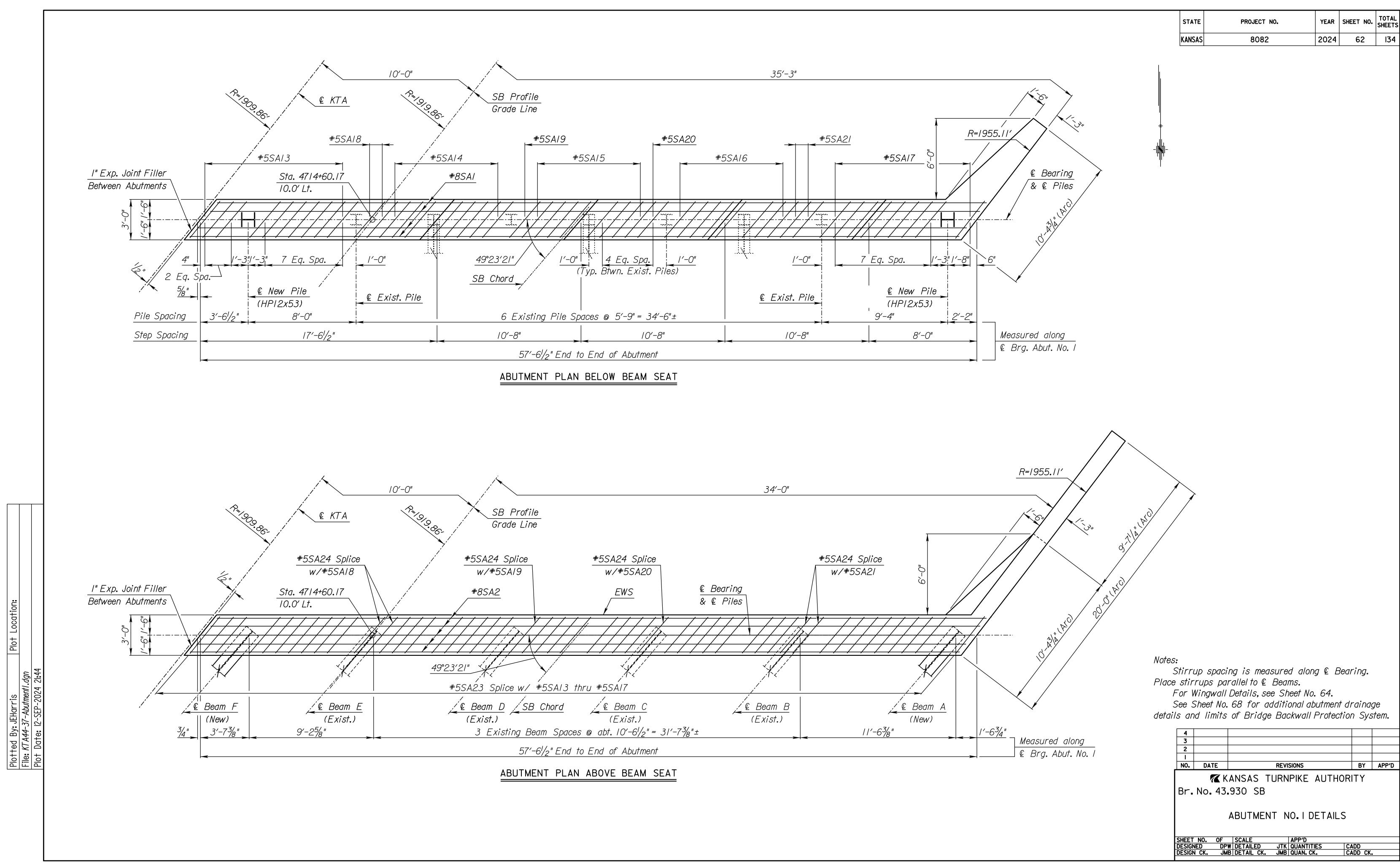
CADD CADD CK. Sheet No. 60

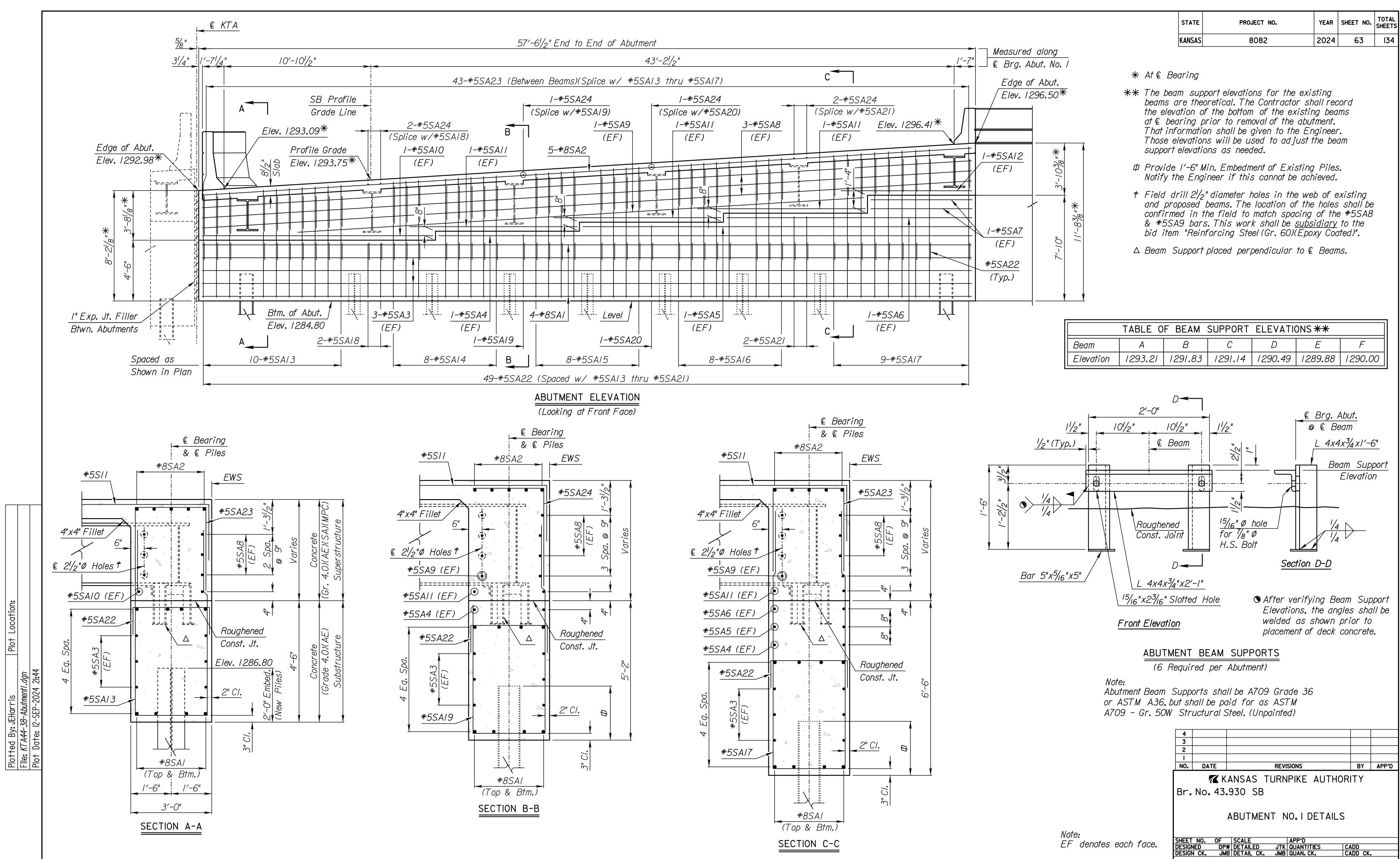


Plotted By: JEHarris	Plot Location:
File: KTA44-36-Foundation.dgn	
Plot Date: 12-SEP-2024 21:44	

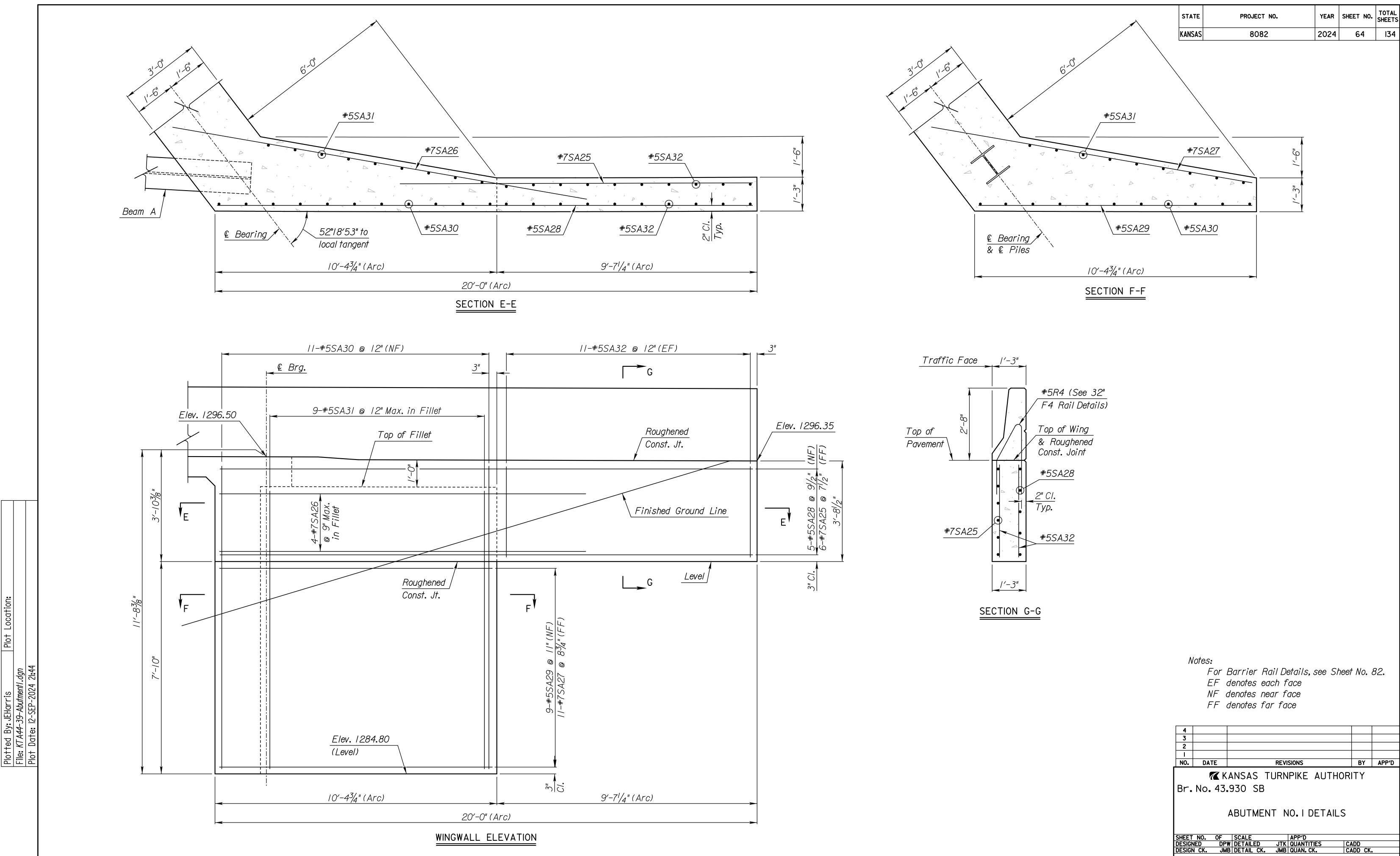
THEORETICAL LOCATION OF NEW PILES										
Location	€ KTA Stationing	Offset from ⊈ KTA	Top of Pile Elevation							
Abut. No. I Median New Pile	4714+65.90	2.80′ Lt.	1286.80							
Abut. No. I Exterior New Pile	4714+34.23	43.54′ Lt.	1286.80							
Pier No. I Median New Pile	4714+96.00	2.16′ Lt.	1286.72							
Pier No. I Exterior New Pile	4714+63.44	42.72′ Lt.	1289.52							
Pier No. 2 Median New Pile	4715+46.36	1.92′ Lt.	1286.74							
Pier No. 2 Exterior New Pile	4715+12.75	41.60′ Lt.	1289.57							
Pier No. 3 Median New Pile	4715+96.80	3.00′ Lt.	1286.85							
Pier No. 3 Exterior New Pile	4715+62.18	41.78′ Lt.	1289.55							
Abut. No. 2 Median New Pile	4716+26.66	4.25′ Lt.	1286.89							
Abut. No. 2 Exterior New Pile	4715+91.47	42.48′ Lt.	1286.89							

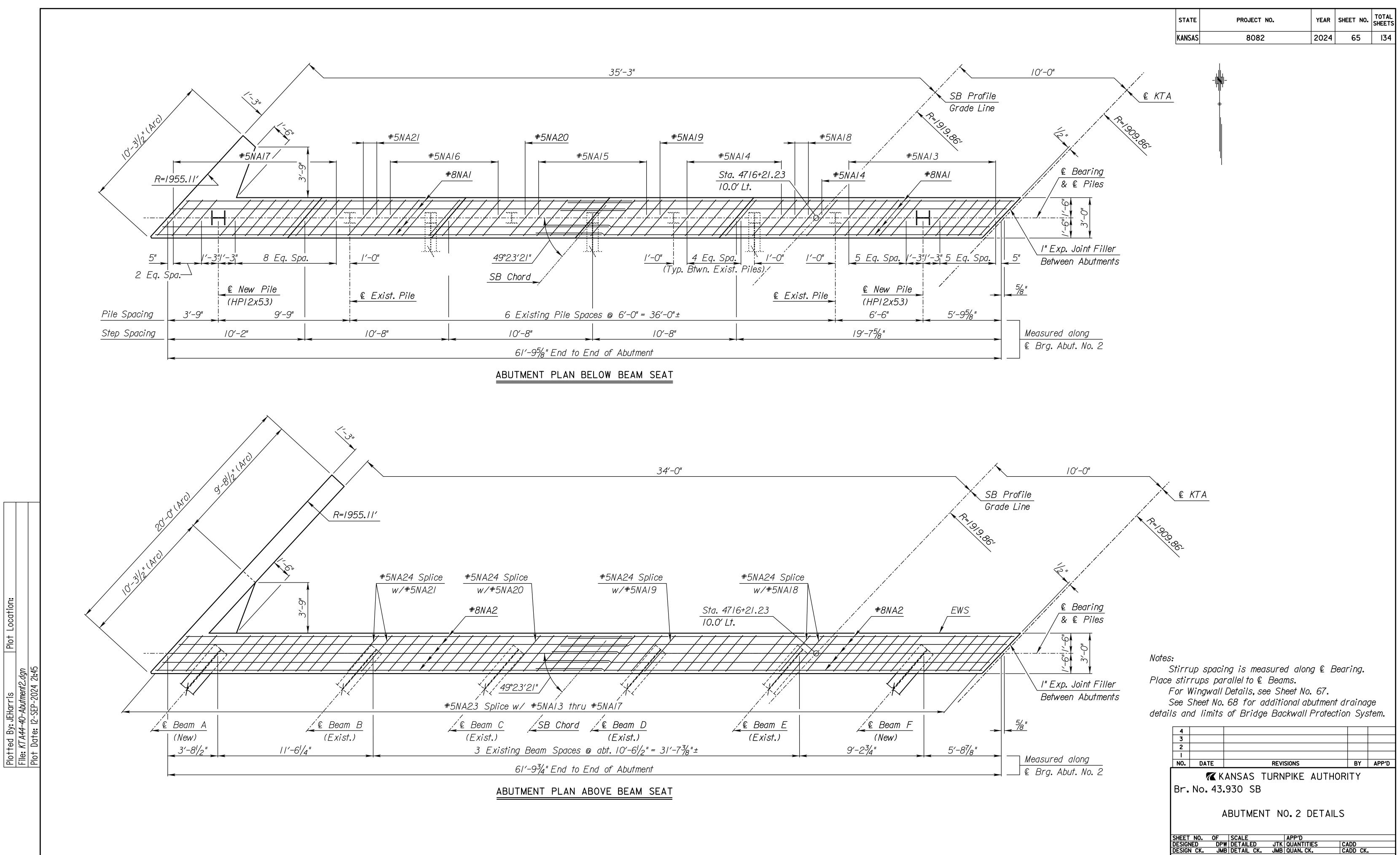
Sheet No. 61





4										
3										
2										
I										
NO.	DATE			R	EVISION	1S				BY
	774 K	ANS	١S	TU	RNPI	KE	AU	THC	)RI	ΤY
Br.	No. 43.	.930	SE	3						
		ABU	ΓΜΕ	INT	NO.		)ET		S	





Sheet No. 65

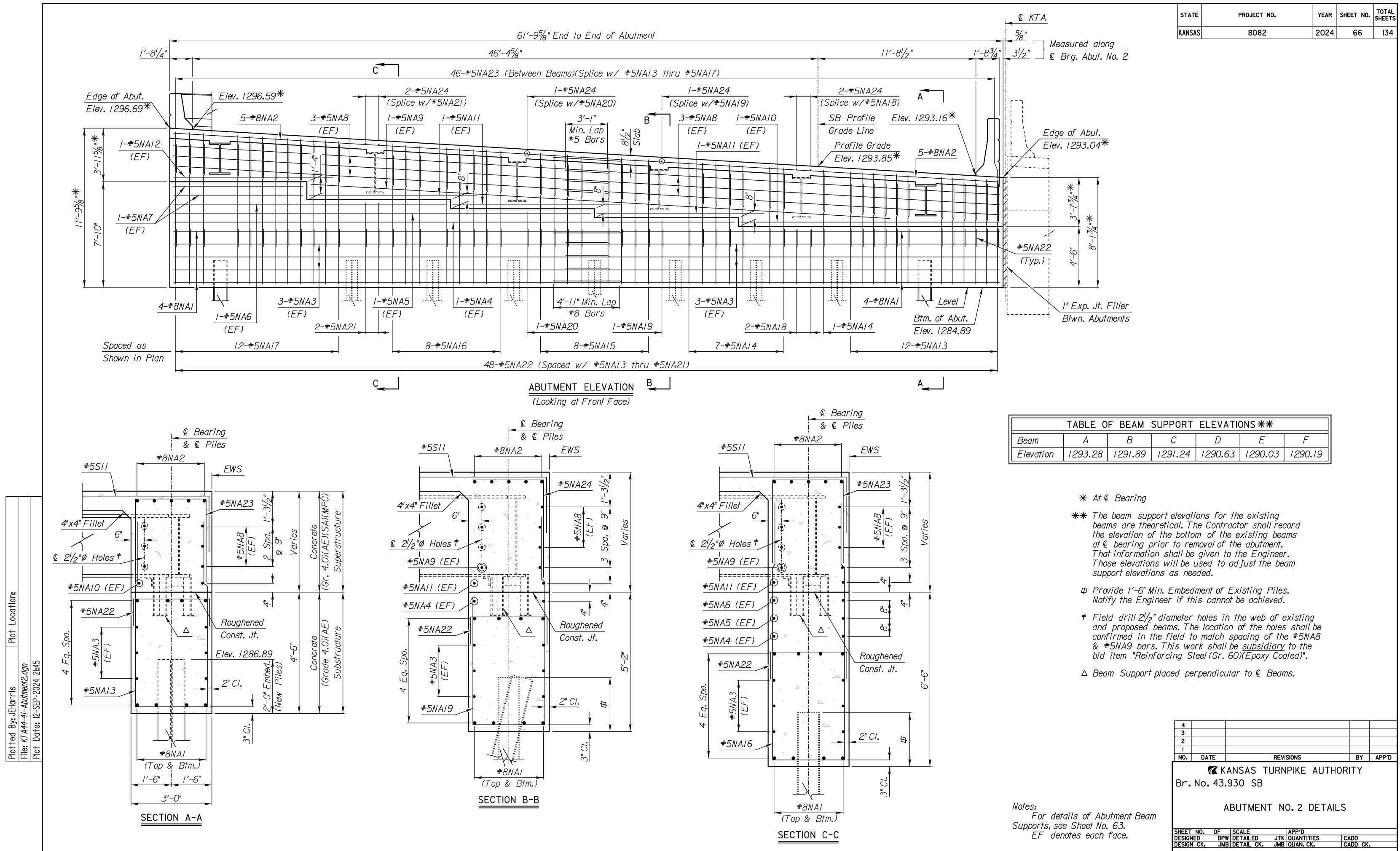
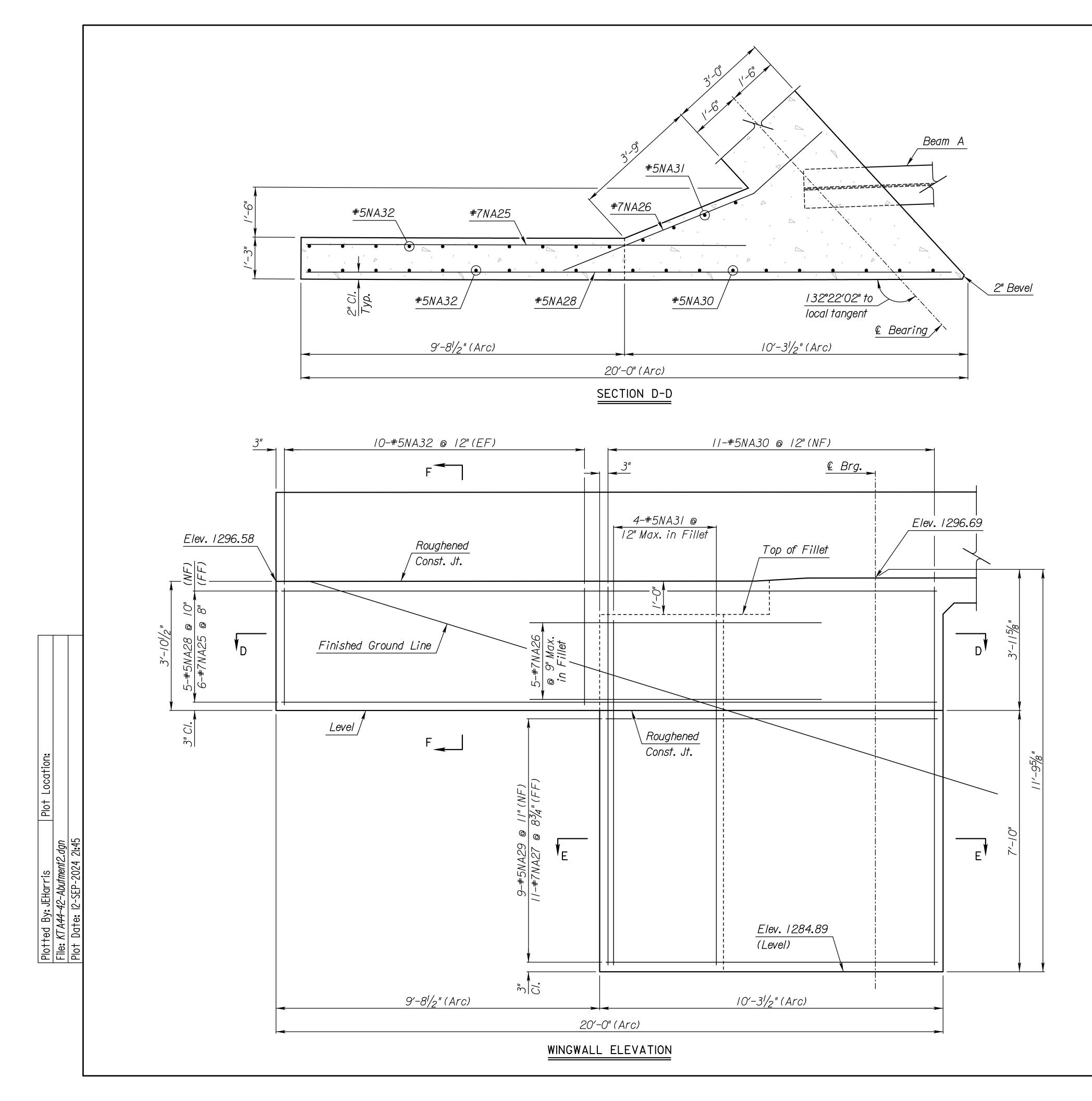
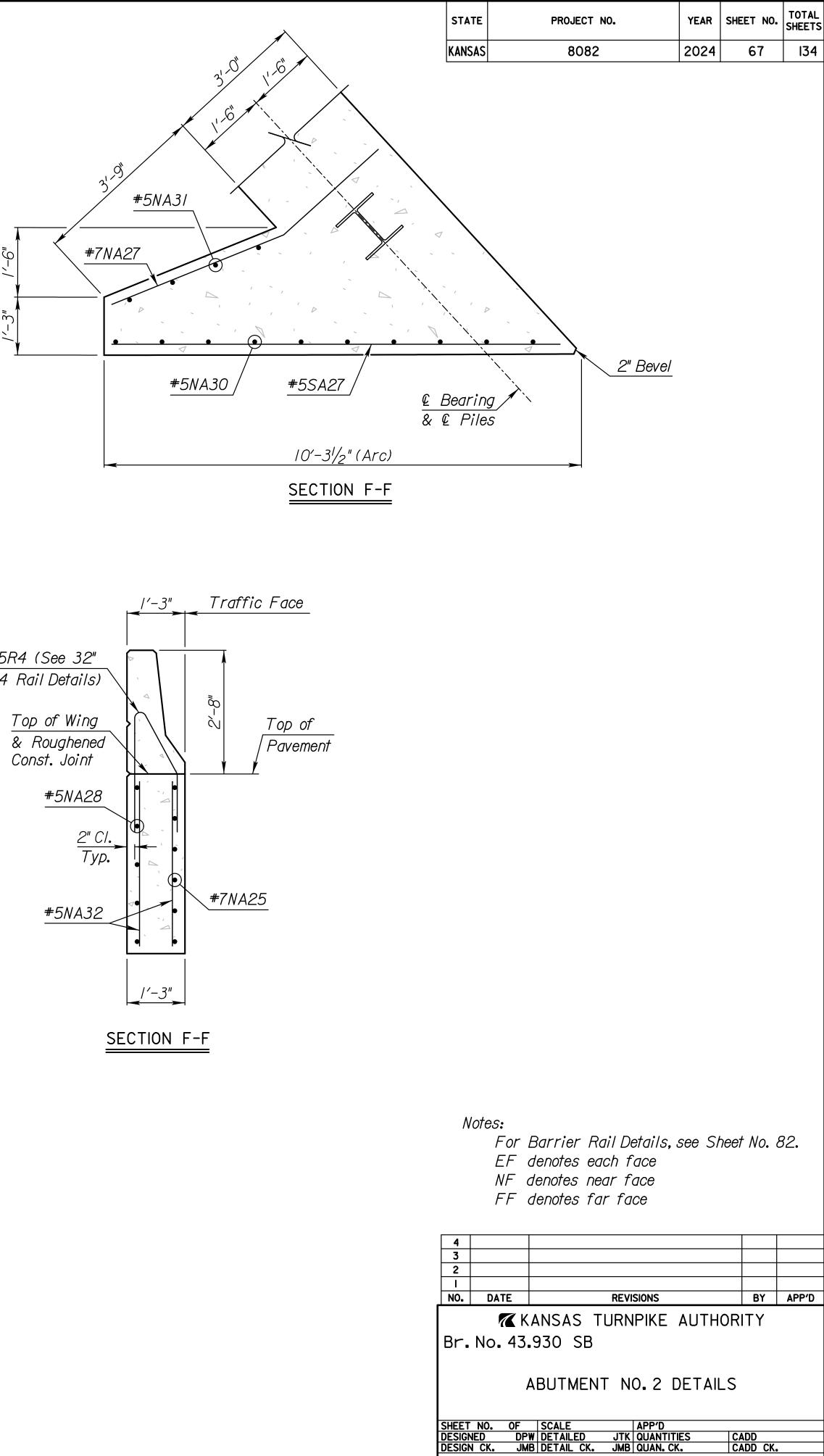


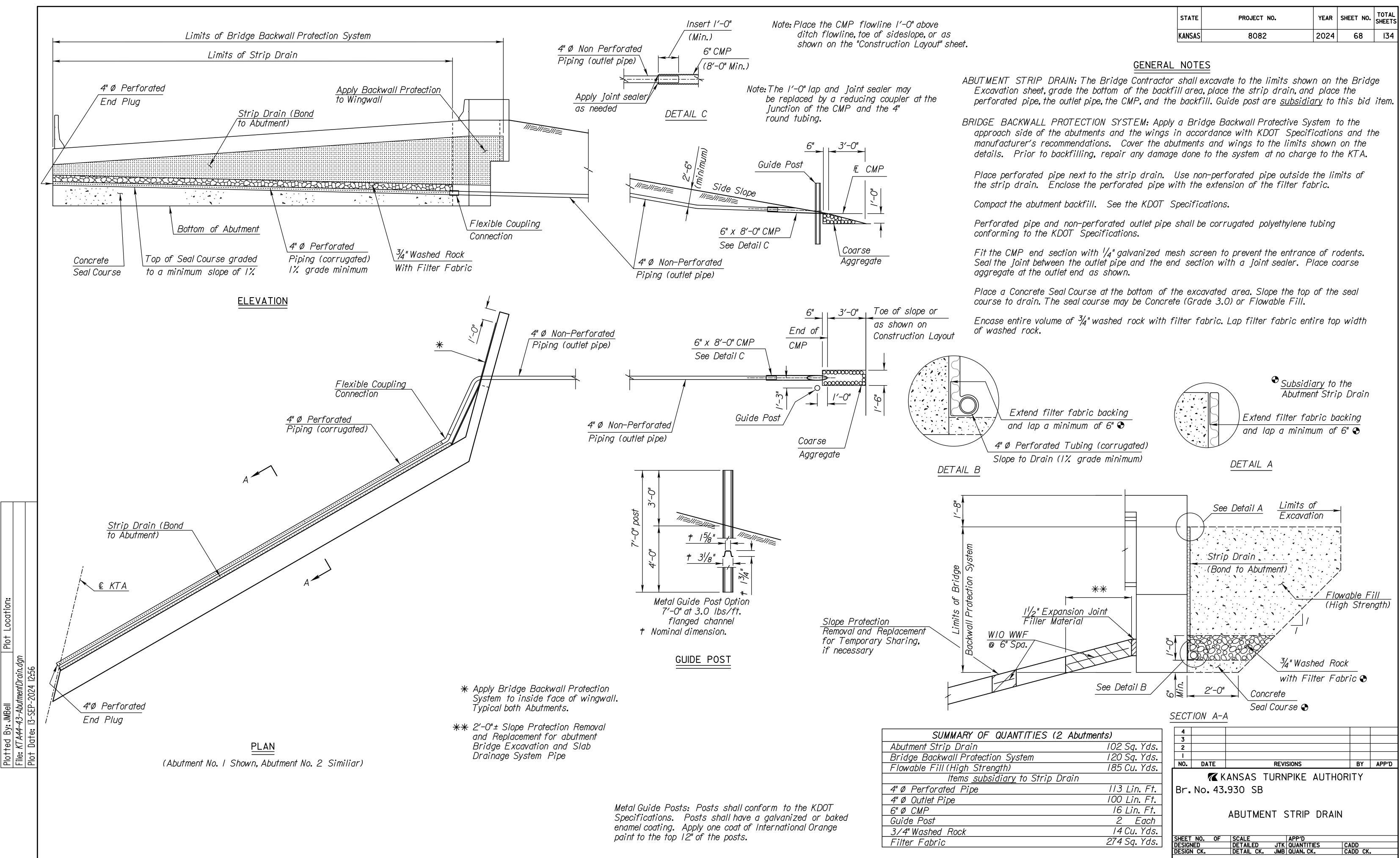
	TABLE O	F BEAM	SUPPORT	ELEVATION	ONS **	
Beam	A	В	С	D	E	F
Elevation	1293.28	1291.89	1291.24	1290.63	1290.03	1290.19

	4						
	3						
	2						
	1						
	NO.	DATE		REVISIONS		BY	APP'D
	Br.		ANSAS T 930 SB	URNPIKE	AUTHO	RITY	
s: For details of Abutment Beam orts, see Sheet No. 63.		,	ABUTMENT	NO.2	DETAILS	S	
EF denotes each face.	SHEET		SCALE	APP'D			
	DESIGN			JTK QUANT		CADD	
	DESIGN	N CK. JM	B DETAIL CK.	JMB QUAN.	CK.	CADD CK	•

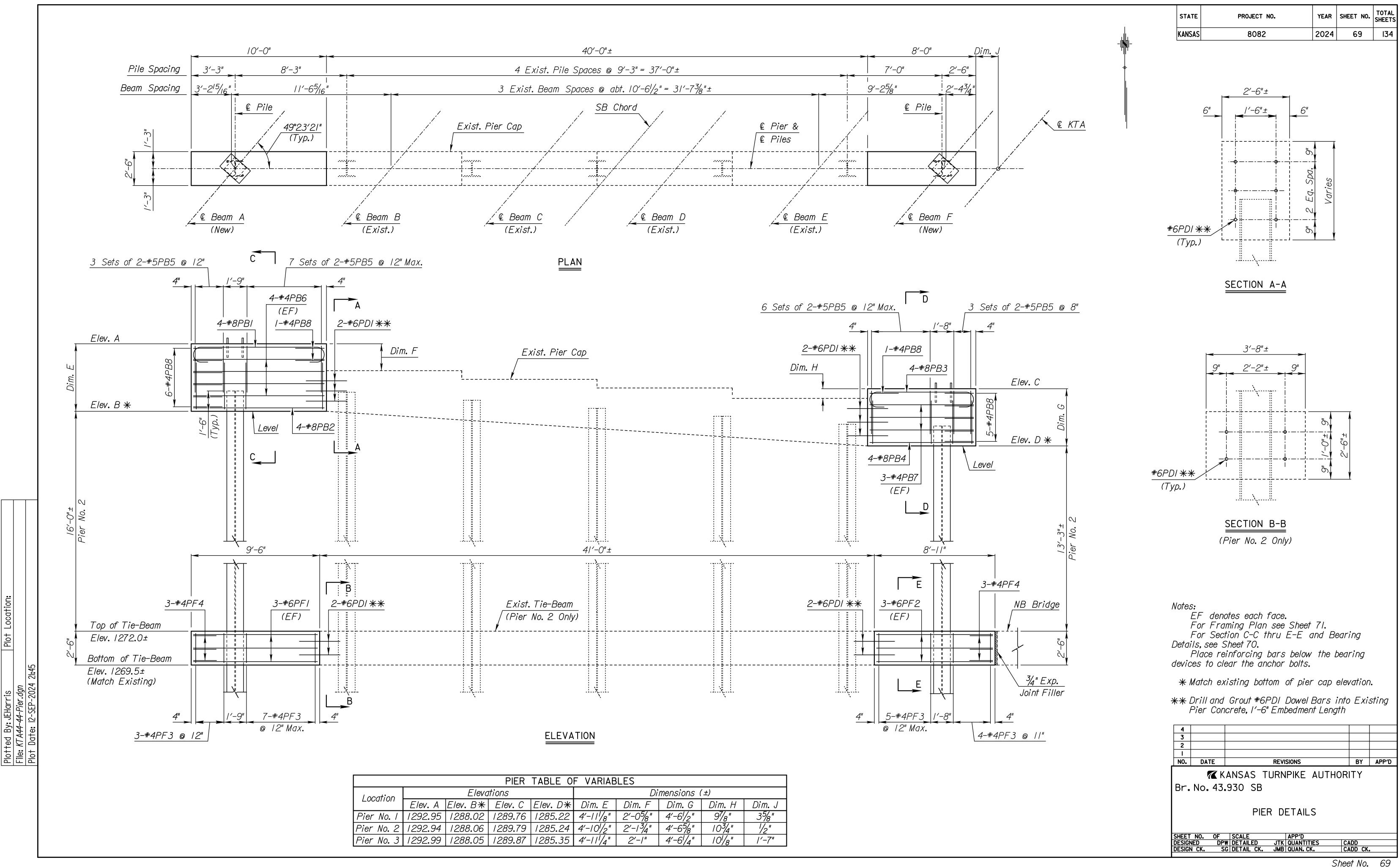




#5R4 (See 32" F4 Rail Details)



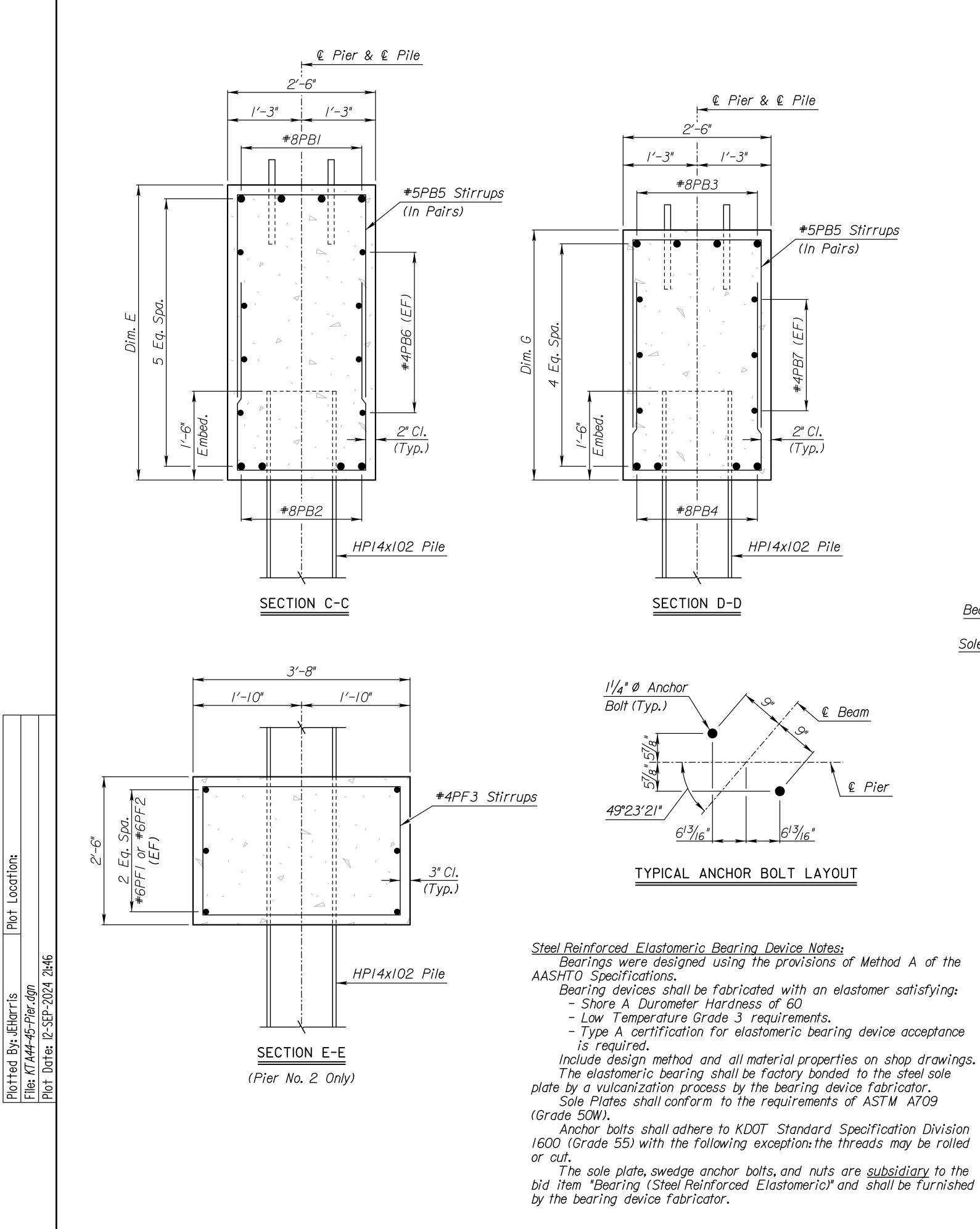
STAT	PROJECT NO.	YEAR	SHEET NO.	TOTAL SHEETS
KANSA	8082	2024	68	134

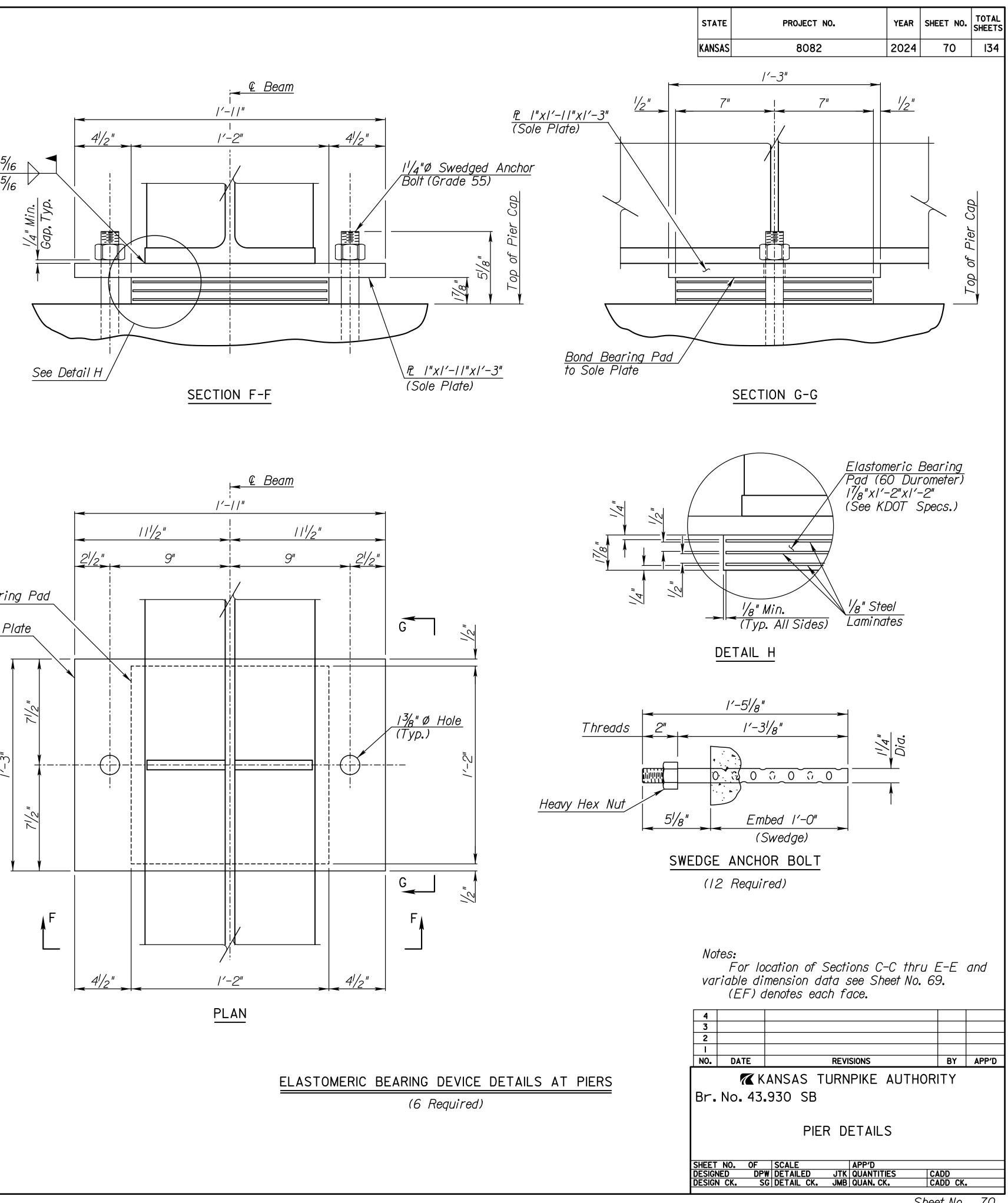


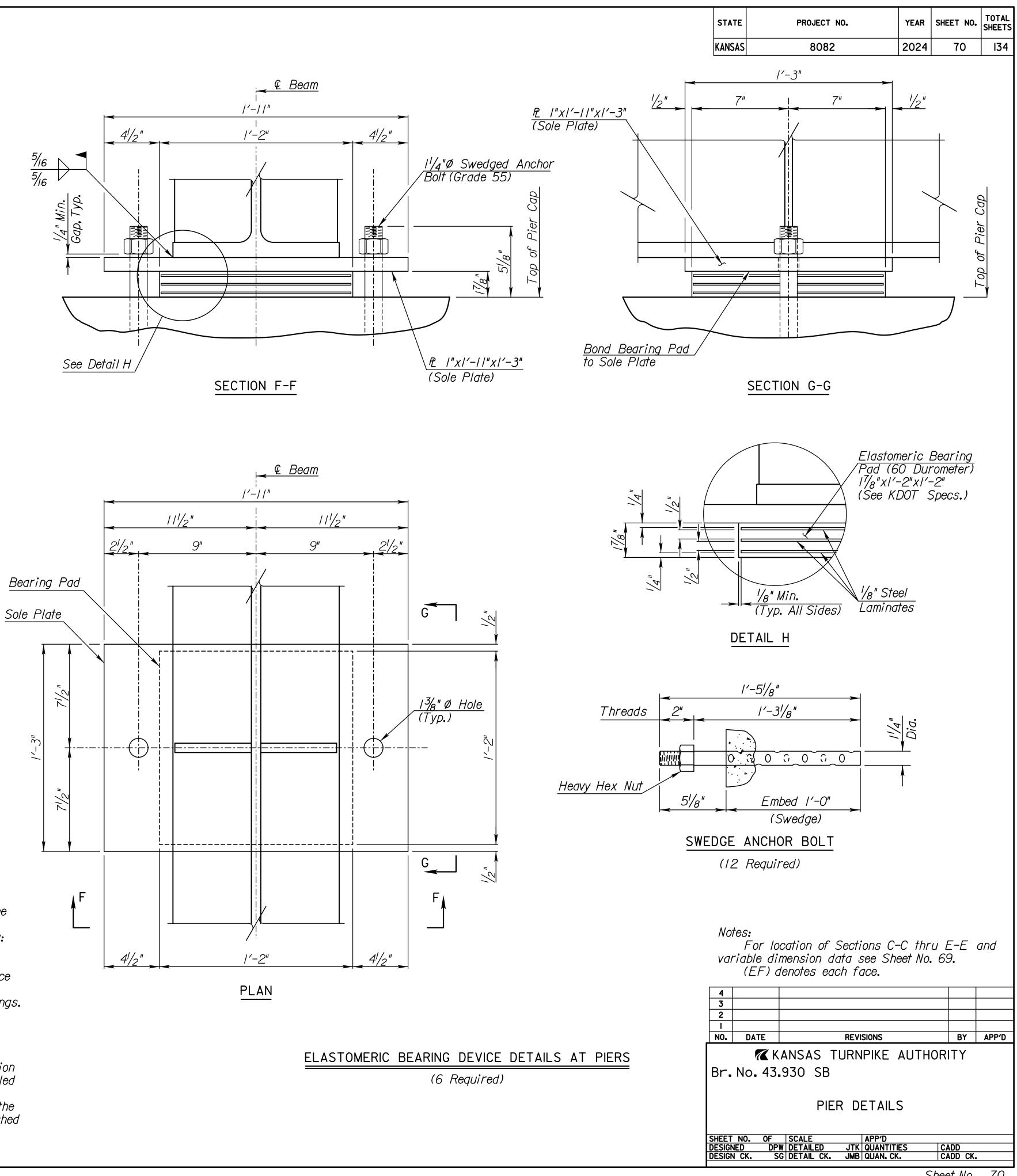
Location:

Plot

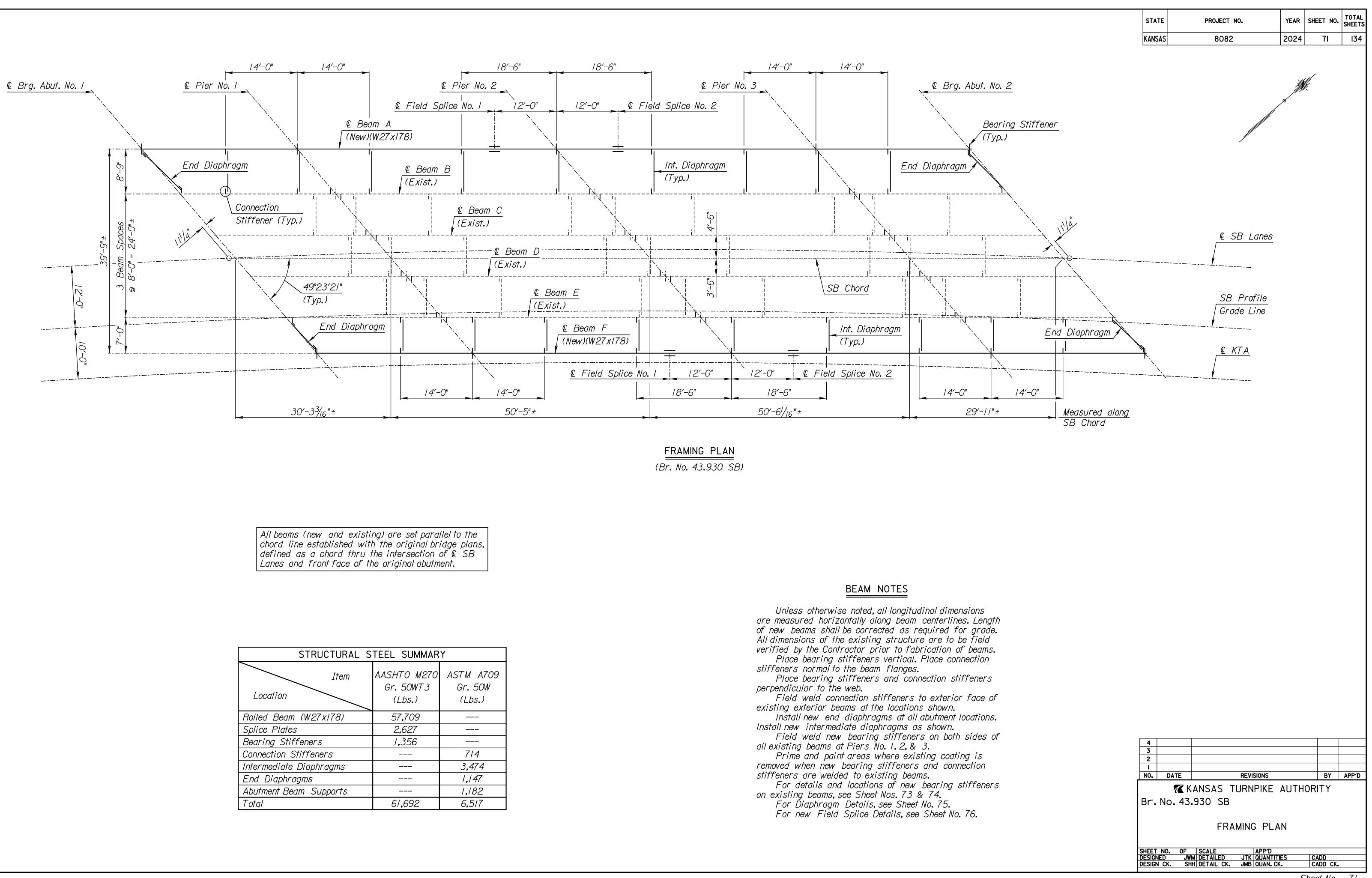
PIER TABLE OF VARIABLES							
Elevations				Di	mensions (	´±)	
<i>w.</i> B <b>米</b>	Elev. C	Elev. D*	Dim. E	Dim. F	Dim. G	Dim. H	Dim. J
88.02	1289.76	1285.22	4'-   <sup> </sup> / <sub>8</sub> "	2'-05/8"	4′-6 <sup> </sup> /2"	9 <b>%</b> "	3 <sup>5</sup> ⁄8"
88.06	1289.79	1285.24	4'-10 <sup> </sup> /2"	2'-13/4"	4′-65⁄8"	103/4"	1/2"
88.05	1289.87	1285.35	4'-   <sup> </sup> / <sub>4</sub> "	2'-1"	4′-6 <sup>1</sup> /4″	10 <sup> </sup> /8"	/′-7″







Sheet No. 70

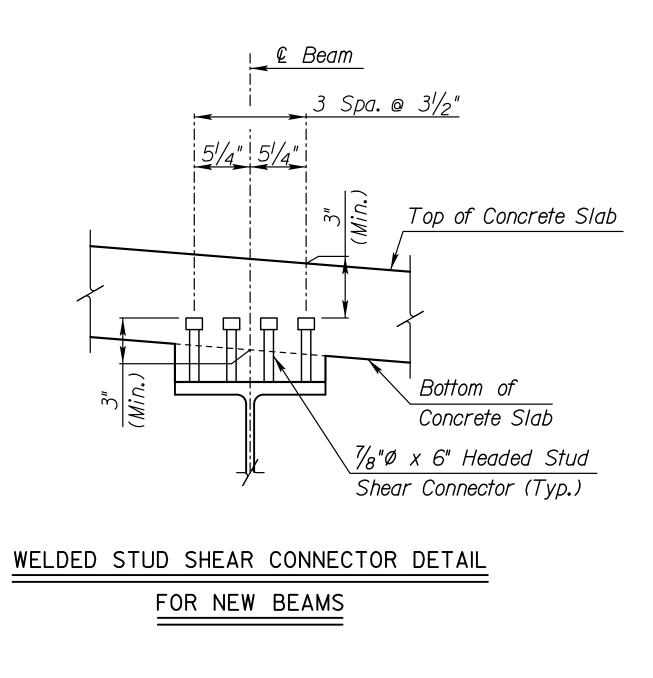


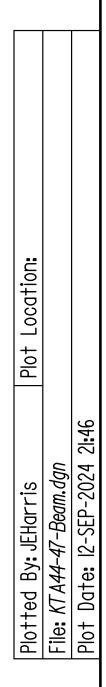
	STRUCTURAL	STEEL SUM
	Item	AASHTO M Gr. 50W7
Location		(Lbs.)
Rolled Beam	(W27x178)	57,709
Splice Plates	6	2,627
Bearing Stif	feners	1,356
Connection S	Stiffeners	
Intermediate	Diaphragms	
End Diaphro	igms	
Abutment Bed	am Supports	
Total		61,692

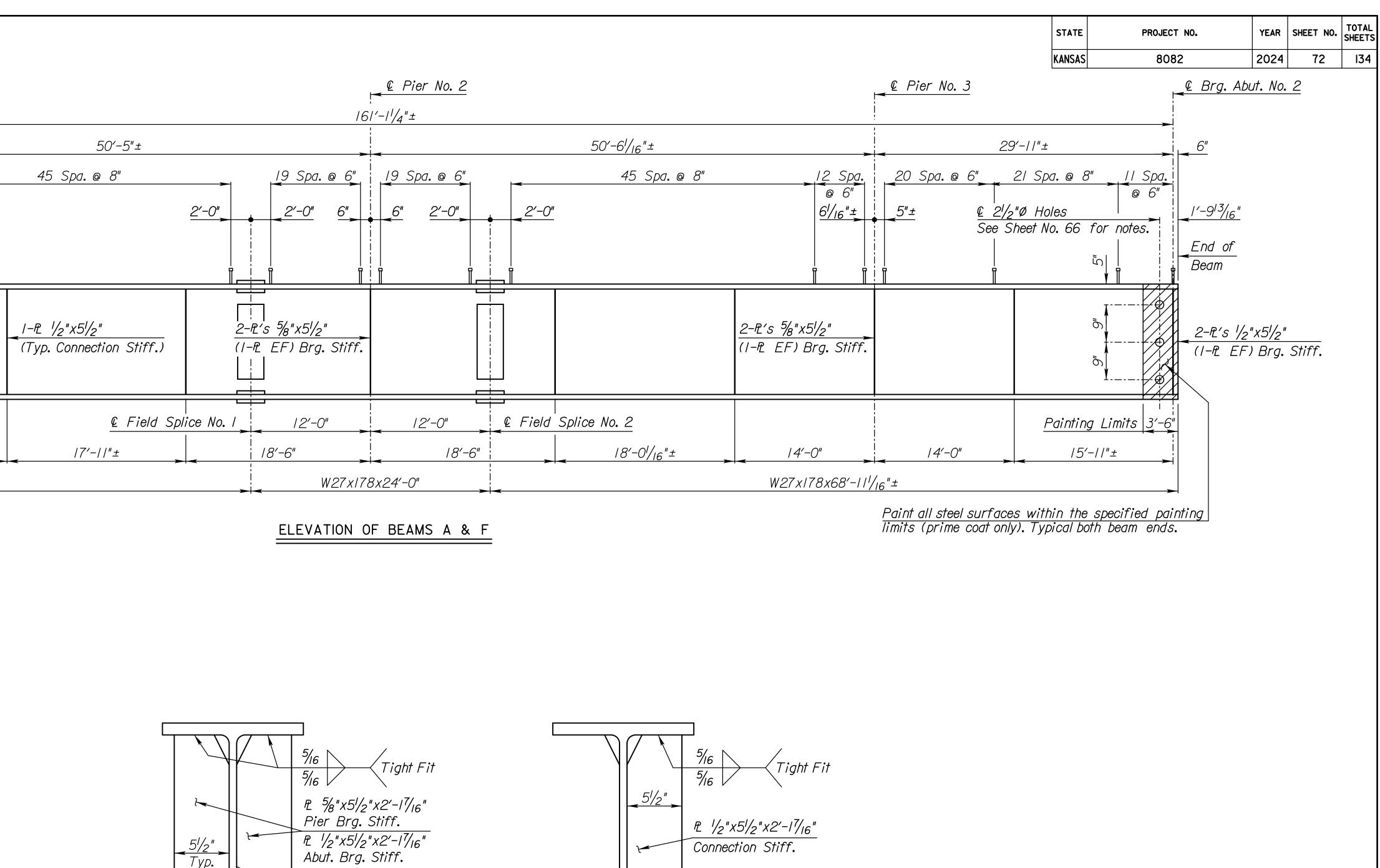
Plotted By: JEHarris	Plot Location:
File: KTA44-46-Framing.dgn	
Plot Date: 12-SEP-2024 21:46	

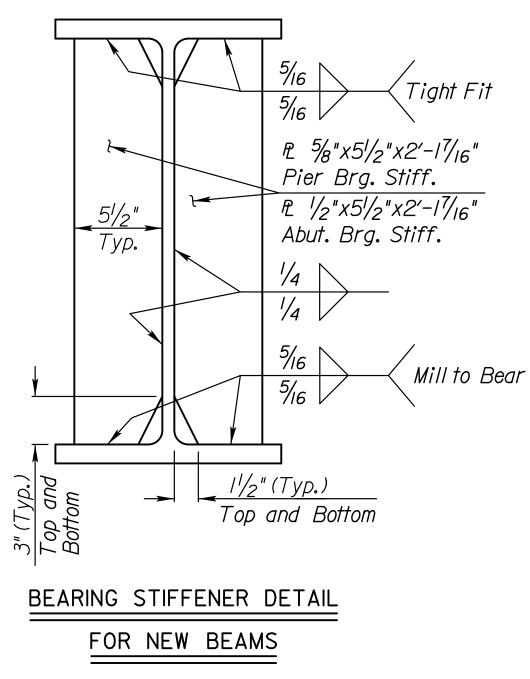
Sheet No. 71

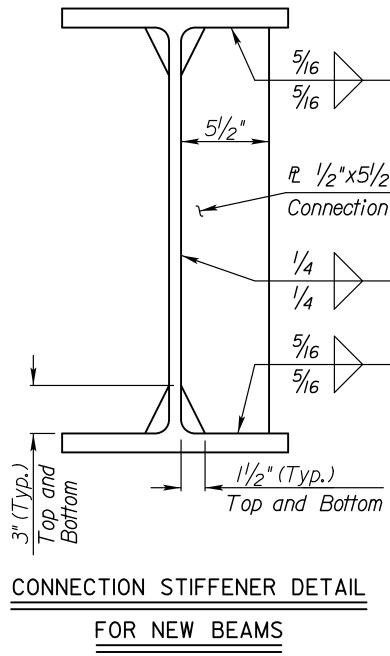
	€ Brg. Abut. No. I	€ Pier No. I
Span Lengths <u>6"</u>	30'-3 <sup>3</sup> / <sub>16</sub> "±	
Shear Connector Spacing (4 per Group) <u>I'-9<sup>I3</sup>/16</u> " End of Beam 2-FL's 1/2"x51/2"	I Spa.       20 Spa.       8"       22 Spa.       6" $@ 6"$ $\frac{5^{3}/6" \pm}{5^{1}/6" \pm}$ $5^{3}/16" \pm$ See Sheet No.       63 for notes. $5^{3}/16" \pm$ $\boxed{10}$ $\boxed{10}$ $2-\frac{p}{s} \frac{5}{8}"x5^{1}/2"$	12 Spa. @ 6" 5"±
(I-R EF) Brg. Stiff.	$\frac{2-\frac{R's}{8}x5\frac{1}{2}}{(1-\frac{R}{E})}$ $\frac{2-\frac{R's}{8}x5\frac{1}{2}}{(1-\frac{R}{E})}$ $\frac{3'-6"}{Painting Limits}$	
Stiffener Spacing	16'-3 <sup>3</sup> / <sub>16</sub> "± 14'-0"	4'-0"
Rolled Beam Sections	<b>~</b>	27x178x69'-2 <sup>3</sup> / <sub>16</sub> "±











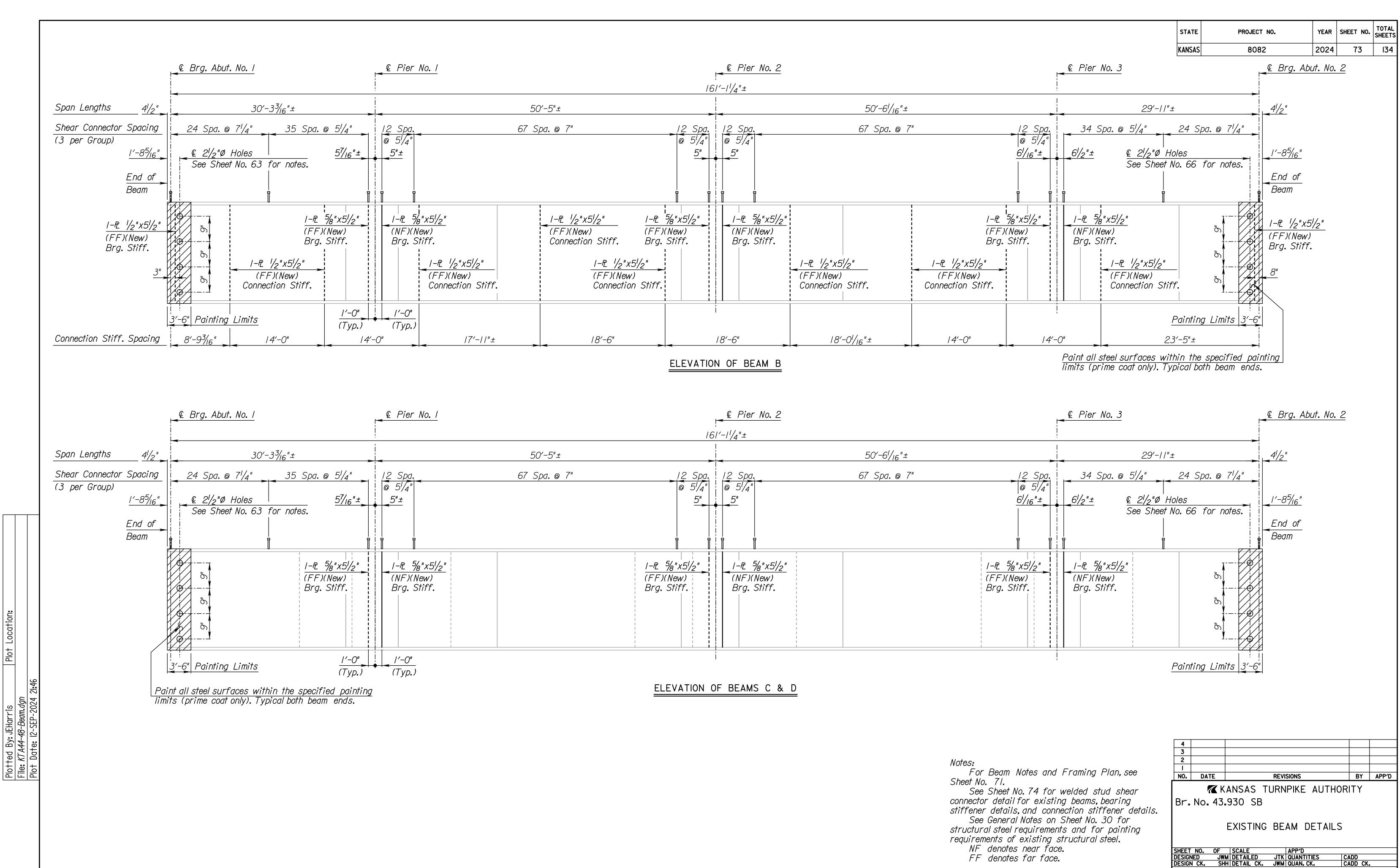
. Tight Fit

Notes:

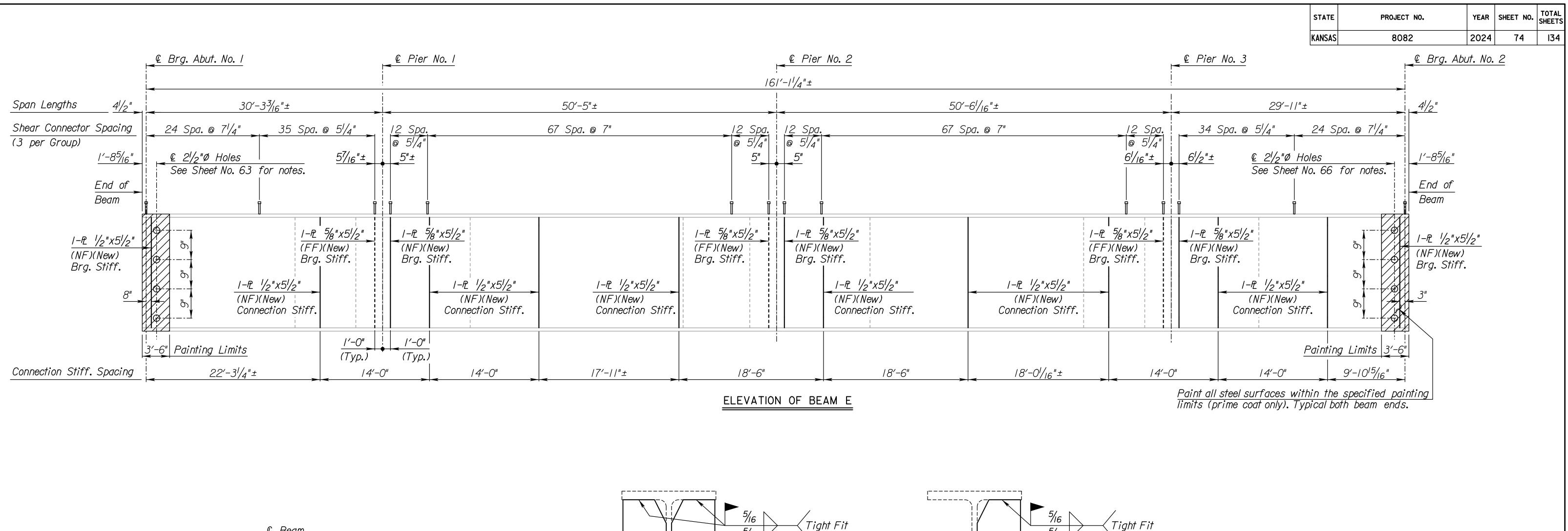
Connection stiffeners are located on the side of the web indicated on the Framing Plan. For Beam Notes and Framing Plan, see Sheet No. 71.

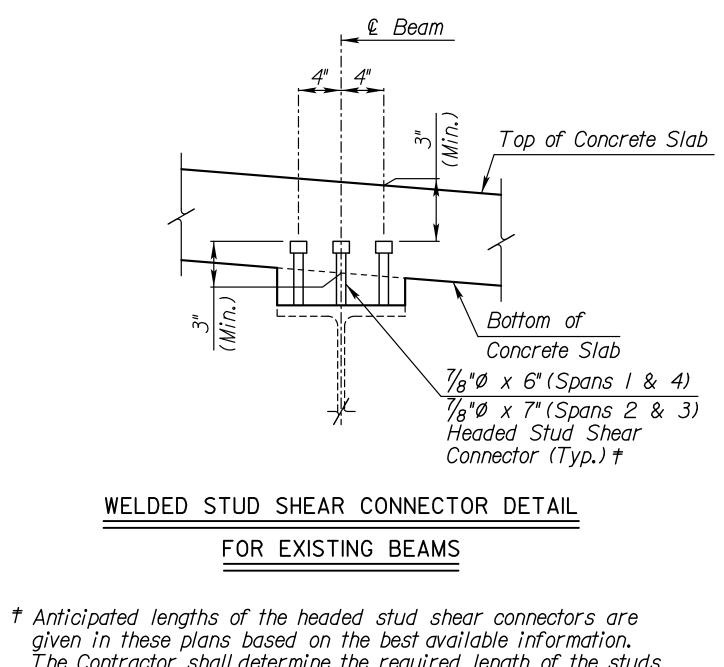
For Field Splice Details, see Sheet No. 76. Field splices shall be made only where shown on the Contract Plans as a "splice". Elimination of any "splice" may be requested. See General Notes on Sheet No. 30 for structural steel requirements and for painting requirements of new weathering steel. EF denotes each face.

4							
3							
2							
NO.	DATE		REVI	SIONS		BY	APP'D
KANSAS TURNPIKE AUTHORITY Br. No. 43.930 SB NEW BEAM DETAILS							
SHEET	NO. OF	SCALE					
DESIGN			JTK	QUANTITIES	C	ADD	
DESIGN	N CK. SH	H DETAIL CK.	JWM	QUAN. CK.	C	ADD CK.	•



SHEET NO.OFSCALEAPP'DDESIGNEDJWMDETAILEDJTKQUANTITIESDESIGNCK.SHHDETAILCK.JWMQUAN. CK.





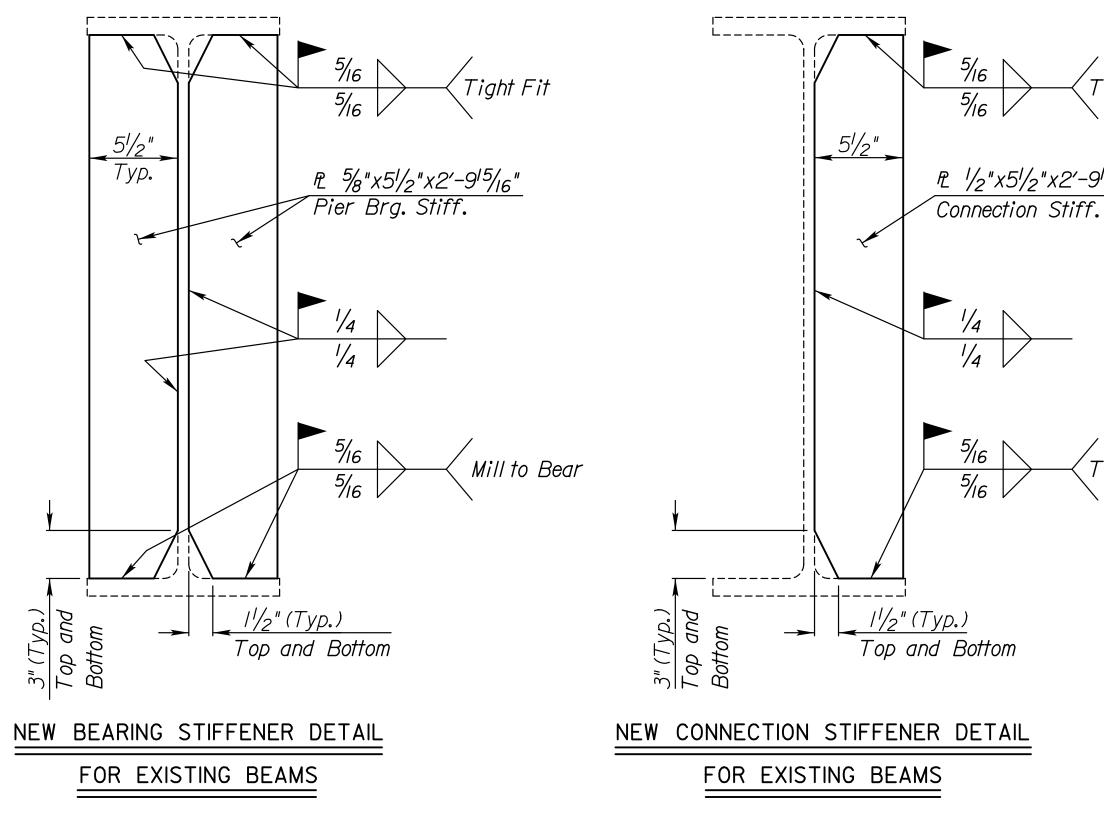
Location:

Plot

is .dgn

Plotted By: JEHarris File: KTA44-49-Beam.d Plot Date: 12-SFP-20

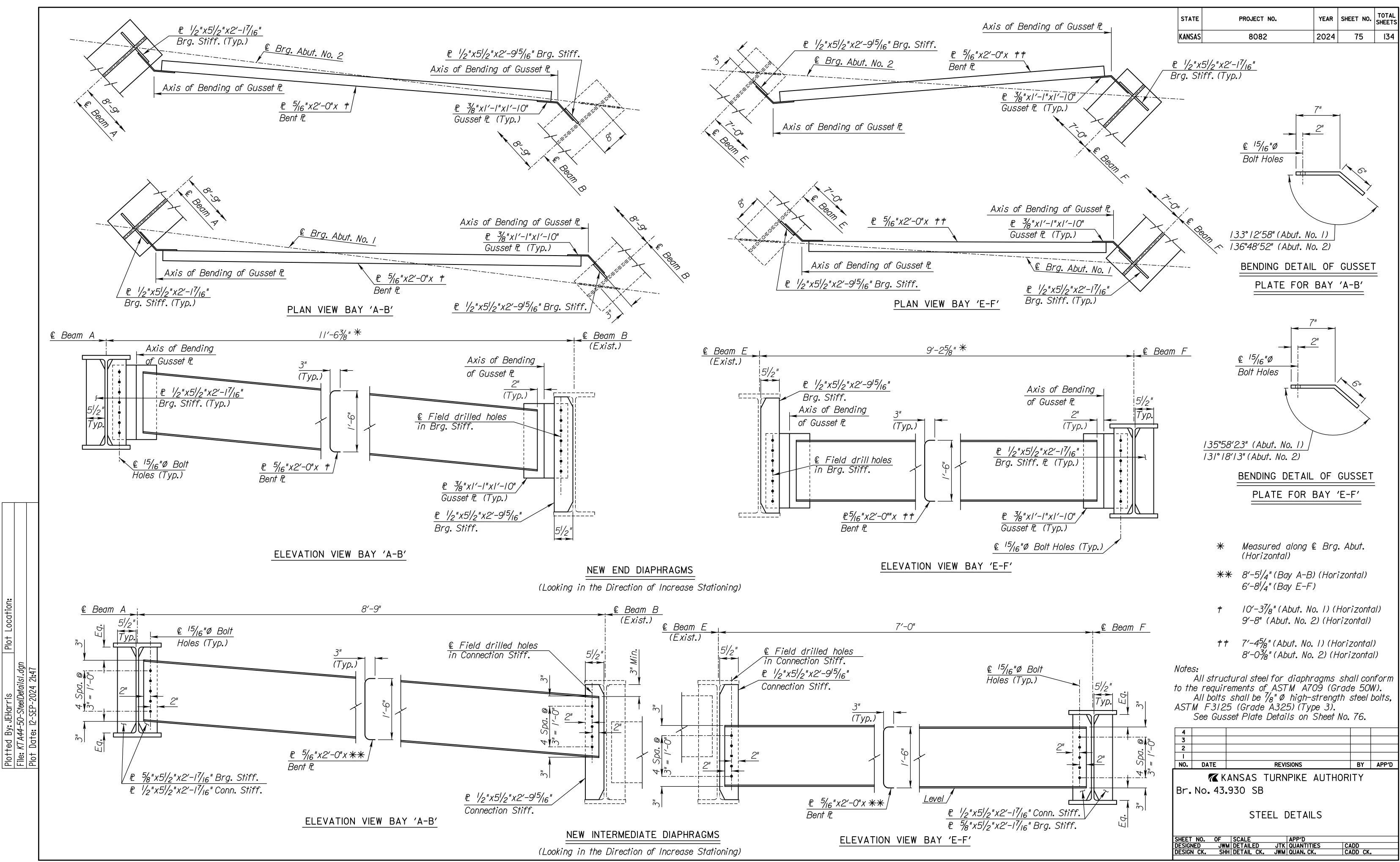
given in these plans based on the best available information. The Contractor shall determine the required length of the studs in the field after the thickness of the slab fillets above the existing beams have been determined. The length of the studs shall be such that the minimum embedment and clearance, as shown, are satisfied. Different stud lengths may be required for the different beams and/or in different regions of the beams. All studs shall be  $7/_8$ " Ø.



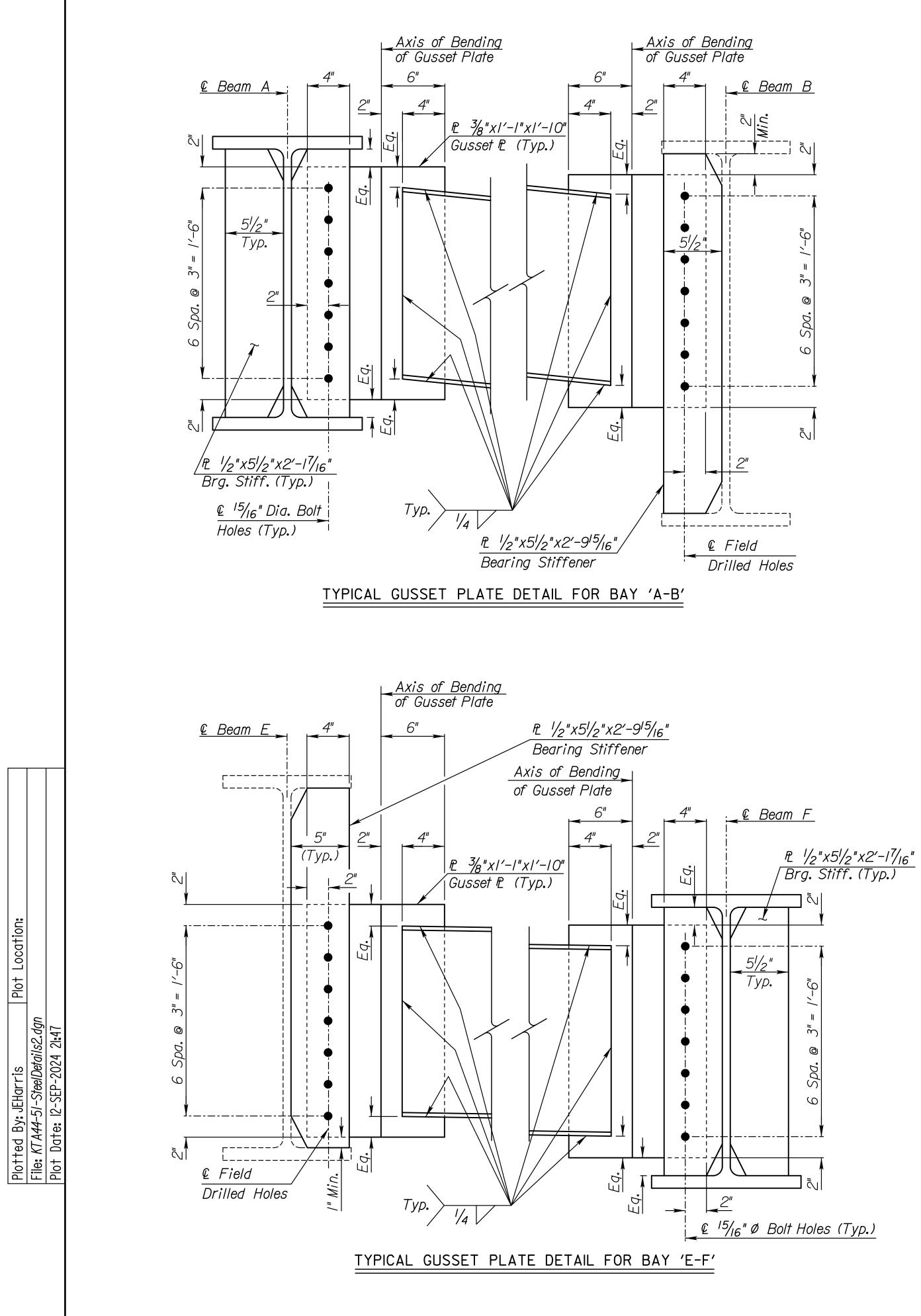
PL 1/2"x51/2"x2'-915/16"

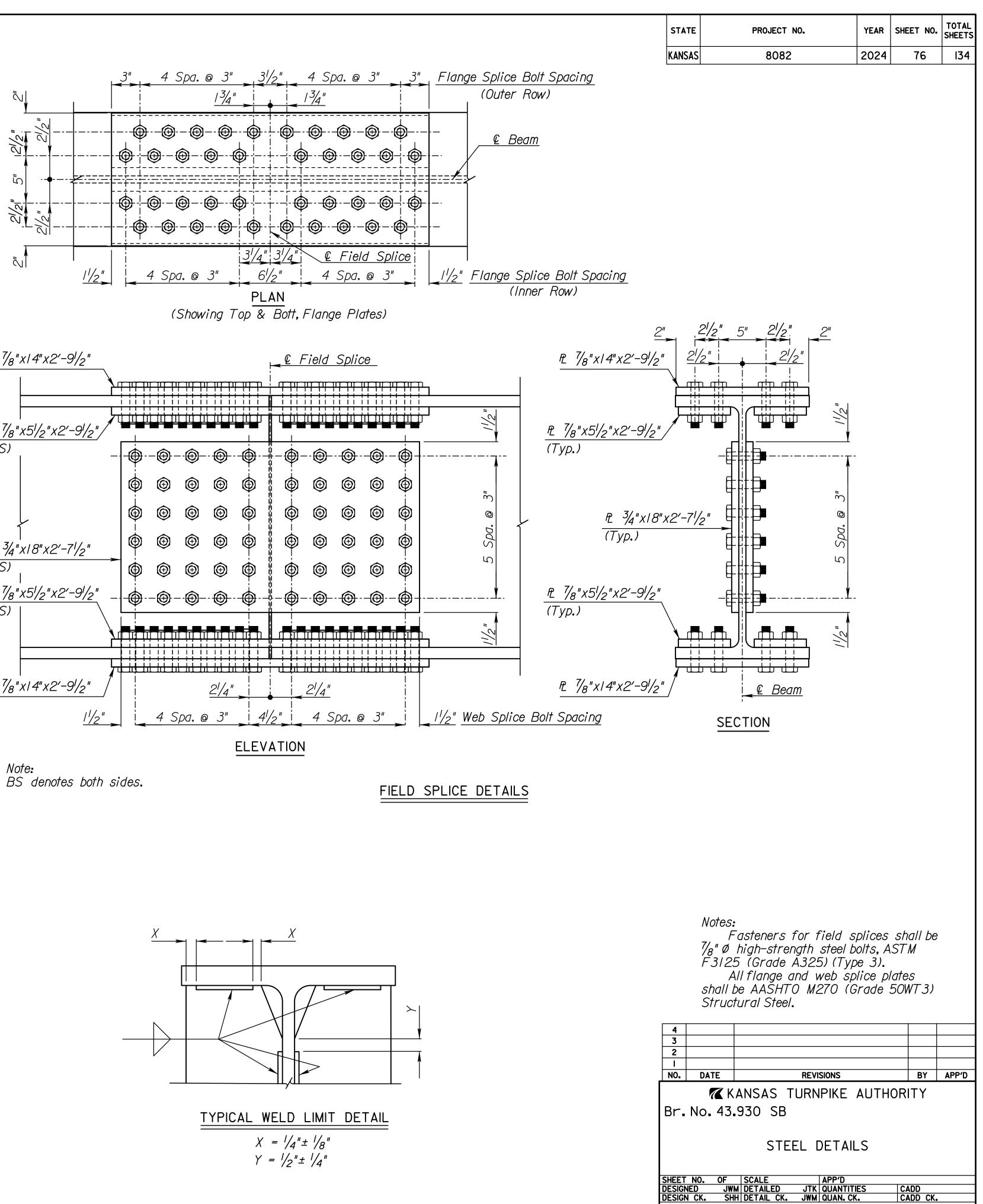
Tight Fit

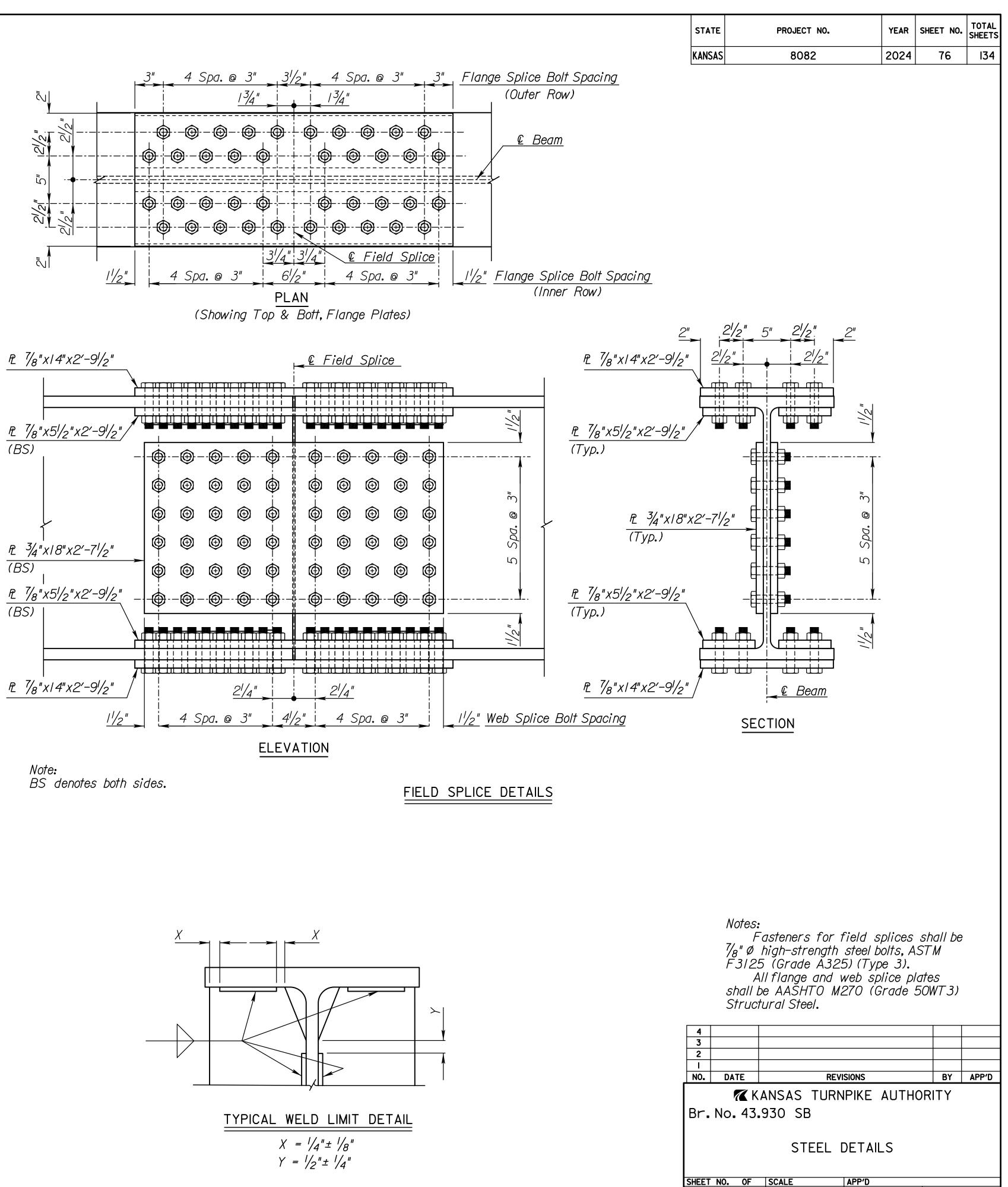
Sh sti	neet No. See Ge ructural s quirement NF de	71. eneral Notes steel require		30 f - pai	for Inting		
4							
3							
2	_						
NO.	DATE		REVISIONS		BY		
	DATE		REVISIONS		Ы	AFFU	
Br	KANSAS TURNPIKE AUTHORITY Br. No. 43.930 SB EXISTING BEAM DETAILS						
SHEE	T NO. OF	SCALE					
DESIG			JTK QUANTITIES	C	ADD		
		H DETAIL CK.	JWM QUAN. CK.		ADD CK.	•	

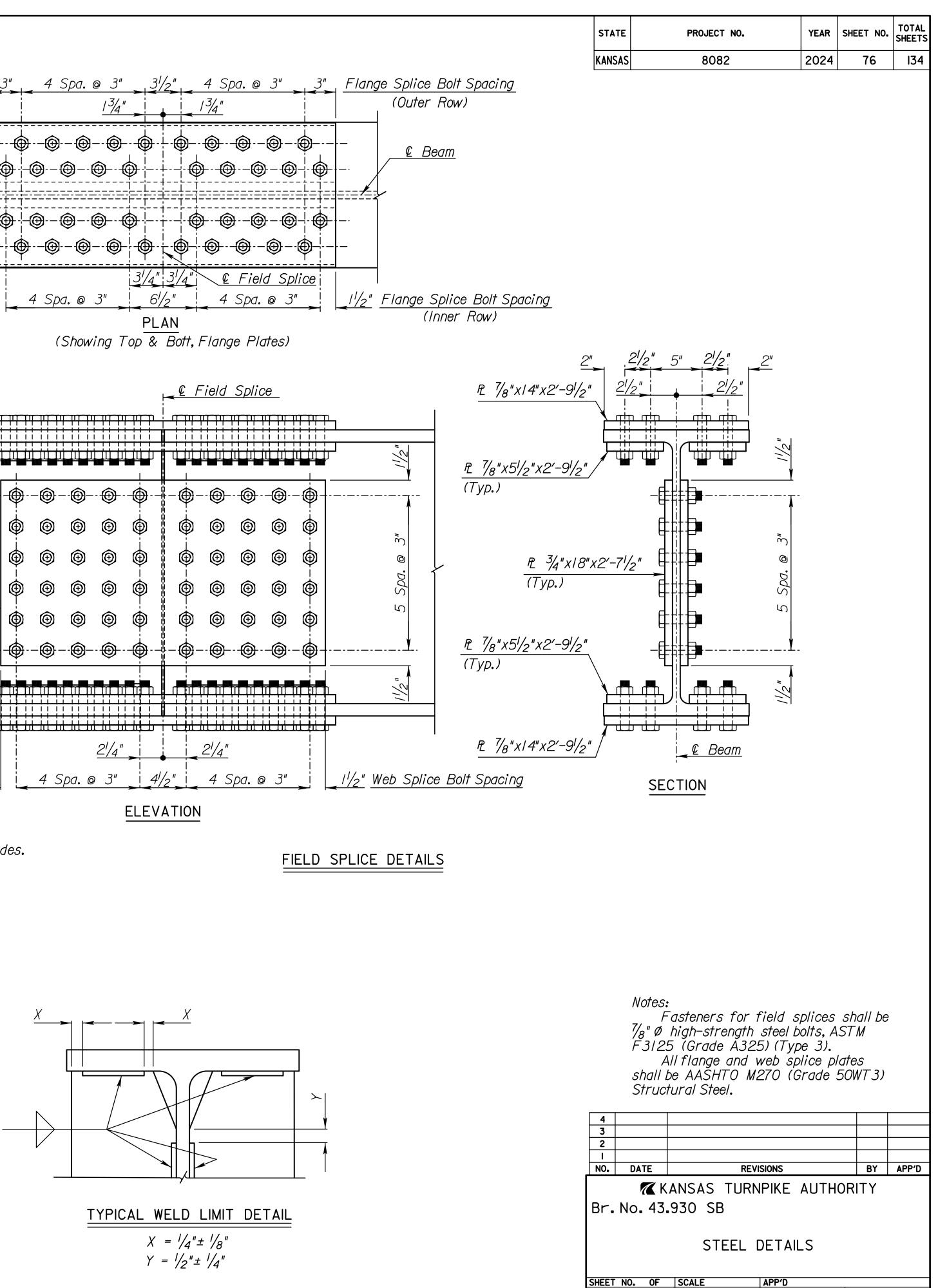


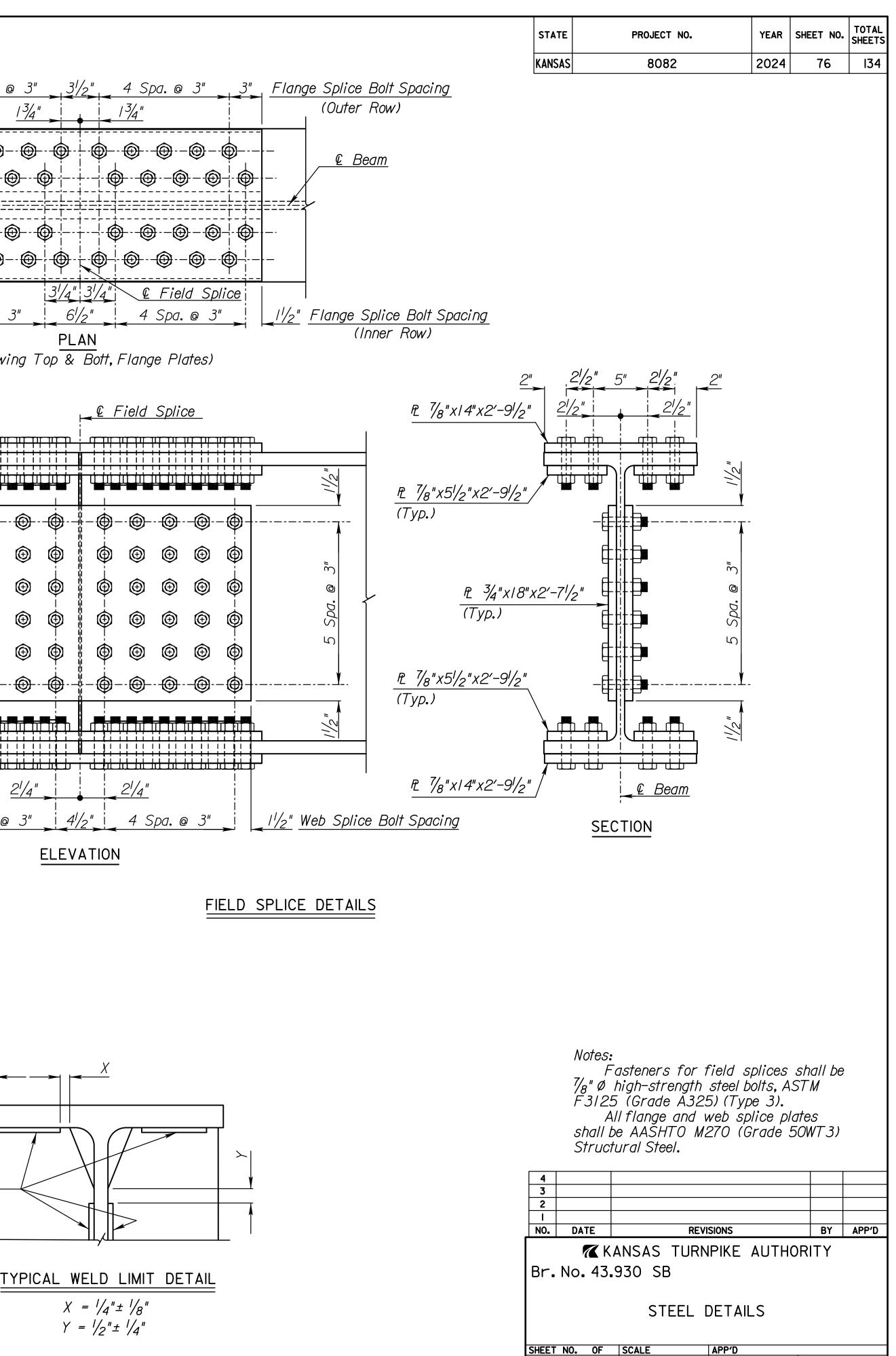
Sheet No. 75

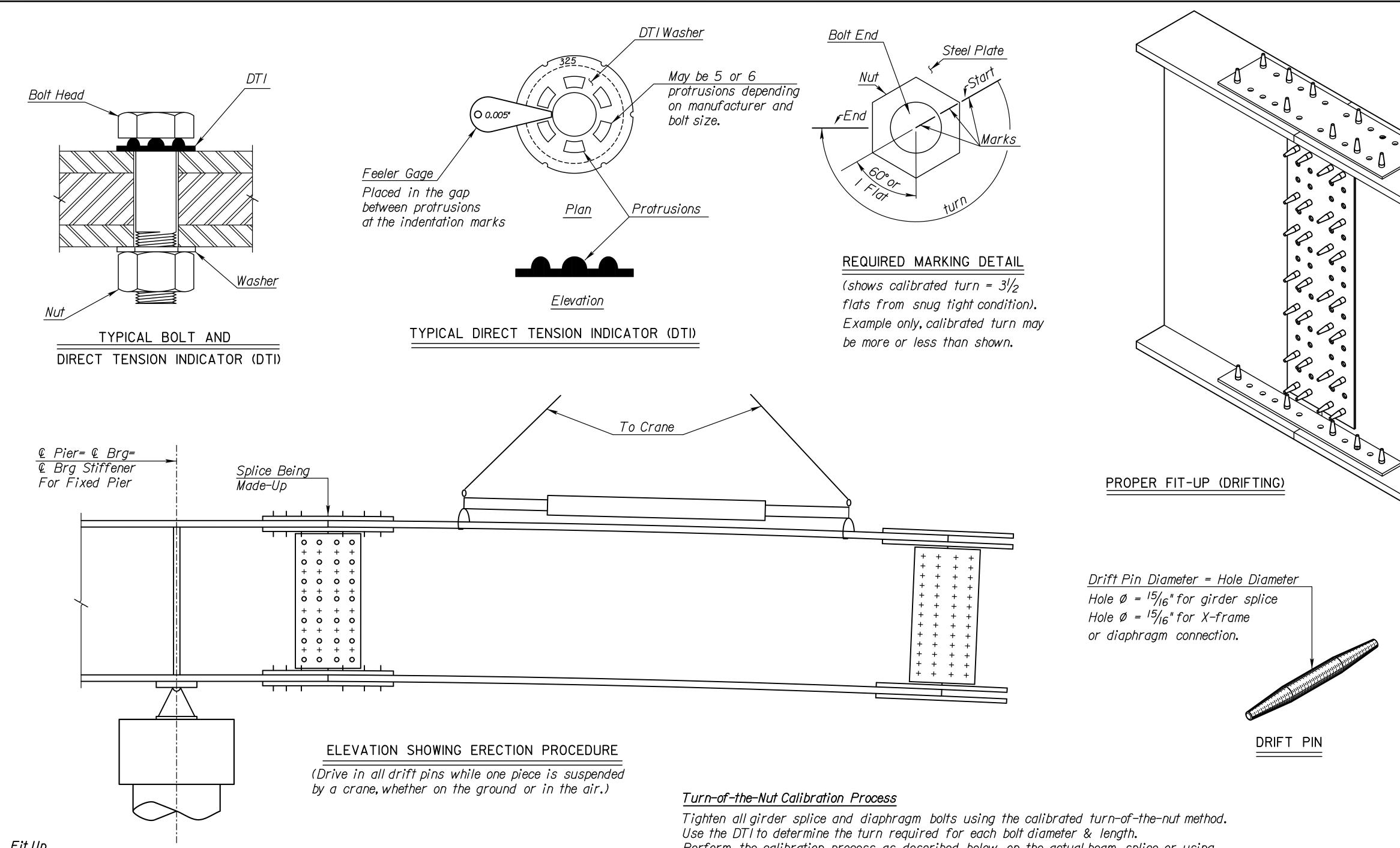












## Fit Up

Location:

Plot

Plotted By: JEH File: KTA44-52-9 Plot Date: 12-5

During the fit up, install drift pins in all corner bolt holes, plus 25 percent of the bolt holes (as a min.), evenly distributed throughout the splice. Fill at least 25 percent of the bolt holes with high strength bolts. Fully tighten these bolts by the calibrated turn-of-the-nut method before removing any drift pins or moving the members. These bolts may be either erection bolts or production bolts. Erection bolts are used during fit up, to compress the plies of the splice to achieve a snug condition. Erection bolts are the property of the Contractor and do not remain in the bridge permanently. Erection bolts must be A325, and can be reused. Erection bolts are required when the abutting plates are of different thickness and no fill plate is provided. This situation usually results in a slight bending of the splice plates. If erection bolts are not used, the DTI's may fully compress before the plates are in firm contact. This would be cause for rejecting the splice. Clearly mark the erection bolts so that they are not left in the splice.

## Erection

Two independent crews will survey the bearing seat elevations. The Engineer will verify that the results of those surveys show that the bearing seat elevations are within  $\pm \frac{1}{4}$  inch of the plan elevations before erection begins. Use the blocking diagram, as shown on the shop drawings, when erecting the beams/girders on the ground. Do not lift the assembled pieces into position until at least 25 percent of the holes are filled with fully tightened bolts. Locate the centerline of the bearing stiffener with the centerline of bearing device. Secure the beams/girders to the top of the pier cap prior to placement of the bearing device anchor bolts.

Perform the calibration process as described below on the actual beam splice or using *3* plies of steel plate with the same thickness as the actual splice.

I. Bring at least 25 percent of the bolts in the splice to a "snug-tight-condition". "Snug tight condition" is defined as (with all plies in firm contact) "the full effort of a man on a spud wrench". Usually a smaller impact gun (1/2" drive) is used to snug the splice and a larger impact gun (1" drive) is used for final tightening. This is preferred over the use of a spud wrench. Production bolting and calibration must use the same tools and lubricating procedures. If an impact wrench is used to "iron the plates" and snug the bolts for calibration, then an impact wrench must be used during the snugging process during production bolting.

2. See "Required Marking Detail" (choose a bolt at the center of the splice and recheck snug on ad jacent bolts)

- a. Mark the outside of the socket at one of the corners.
- b. Mark the bolt, plate, and nut at a corner with a start line.
- Align the mark on the socket with the start mark on the bolt end.
- d. While holding a backup wrench on the head of the bolt, turn the nut  $\frac{1}{2}$  turn (3 flats).
- Record the number of refusals. е.
- f. If all of the gaps refuse, go to another bolt and turn the nut 2 flats (1/3 turn).
- g. If there are fewer than 3 refusals turn the nut an additional  $\frac{1}{4}$  of a flat (15 degrees).
- h. Repeat step g, turning the nut 1/3 of a flat or less each time, until all of the gaps refuse the feeler gage. Record the amount required to cause all of the gaps to refuse the feeler gage. This is the target rotation.

3. Repeat this process for each bolt diameter and length.

STATE	PROJECT NO.	YEAR	SHEET NO.	TOTAL SHEETS
KANSAS	8082	2024	77	134

## Production Bolt Tightening

I. Install bolts and tighten to "snug tight" in a pattern, starting at the center of the splice and working toward the edge. On large girders this may have to be done twice, as the center bolts will become loose as plates are "Ironed out". This step is important because typically, any variation in results during production bolting is the result of a change in the materials, lubricant or equipment used to take the bolts to a "snug tight" condition during the calibration process.

2. Mark all of the bolts, nuts and the plate as shown in the marking detail. Mark the socket with a start and stop point. The stop point corresponds to the target rotation determined earlier.

3. Align the start mark on the socket with the line on the plate. While the bolt is being backed up, turn the nut until the stop mark on the socket lines up with the start mark on the plate.

4. Repeat with all bolts of the same length in the splice.

## Acceptance and Rejection of Bolts

I. The Engineer will check all bolts with a feeler gage.

2. All nuts must be turned at least the target rotation beyond "snug tight".

3. All DTI's must have at least 3 refusals of the 0.005" gage.

4. If all gaps refuse the 0.005" gage, and the nut, plate and bolt are not marked, reject the bolt.

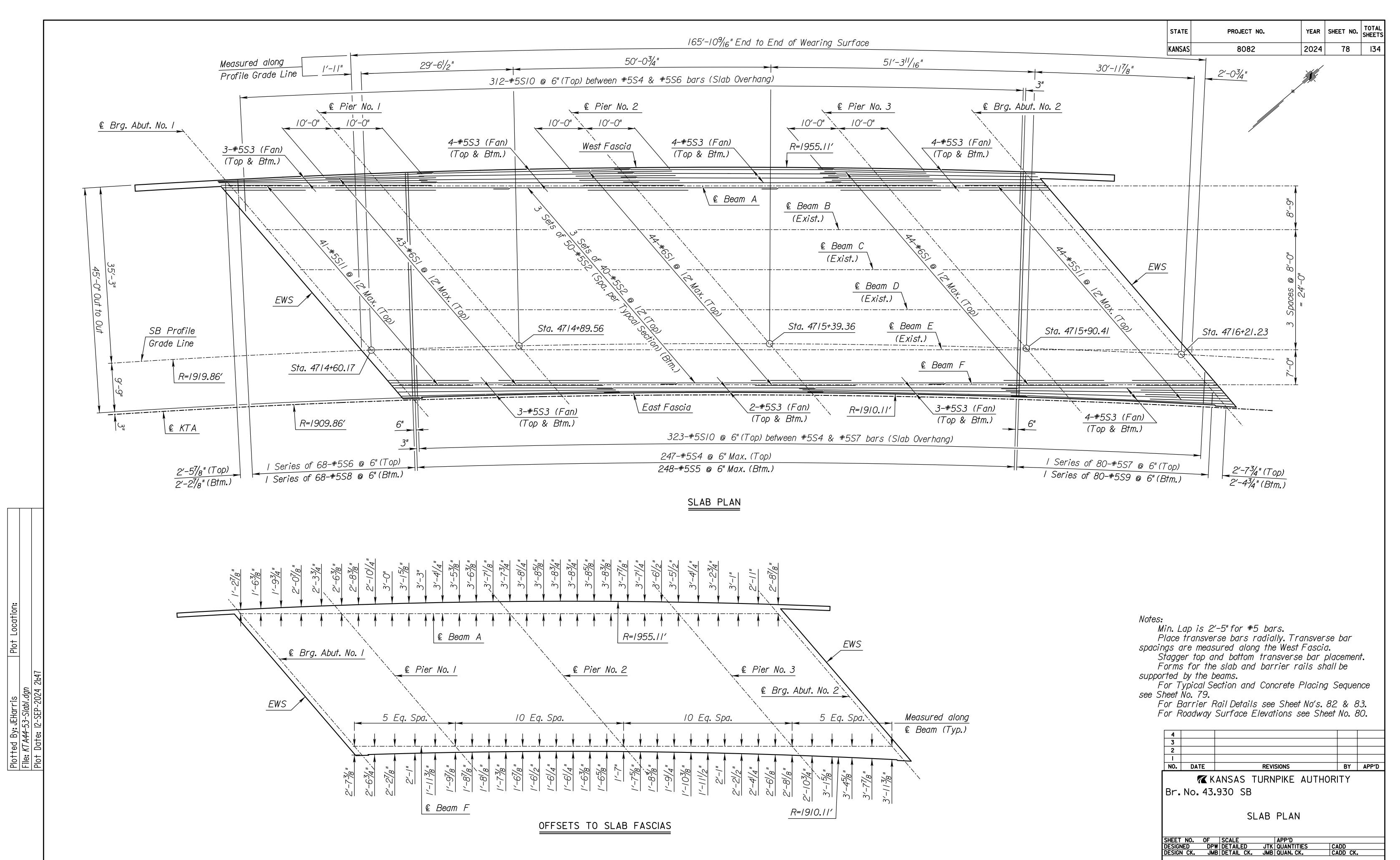
5. If all gaps refuse the 0.005" gage, and the turned element has not been rotated more than 45° beyond the calibrated turn. accept the bolt.

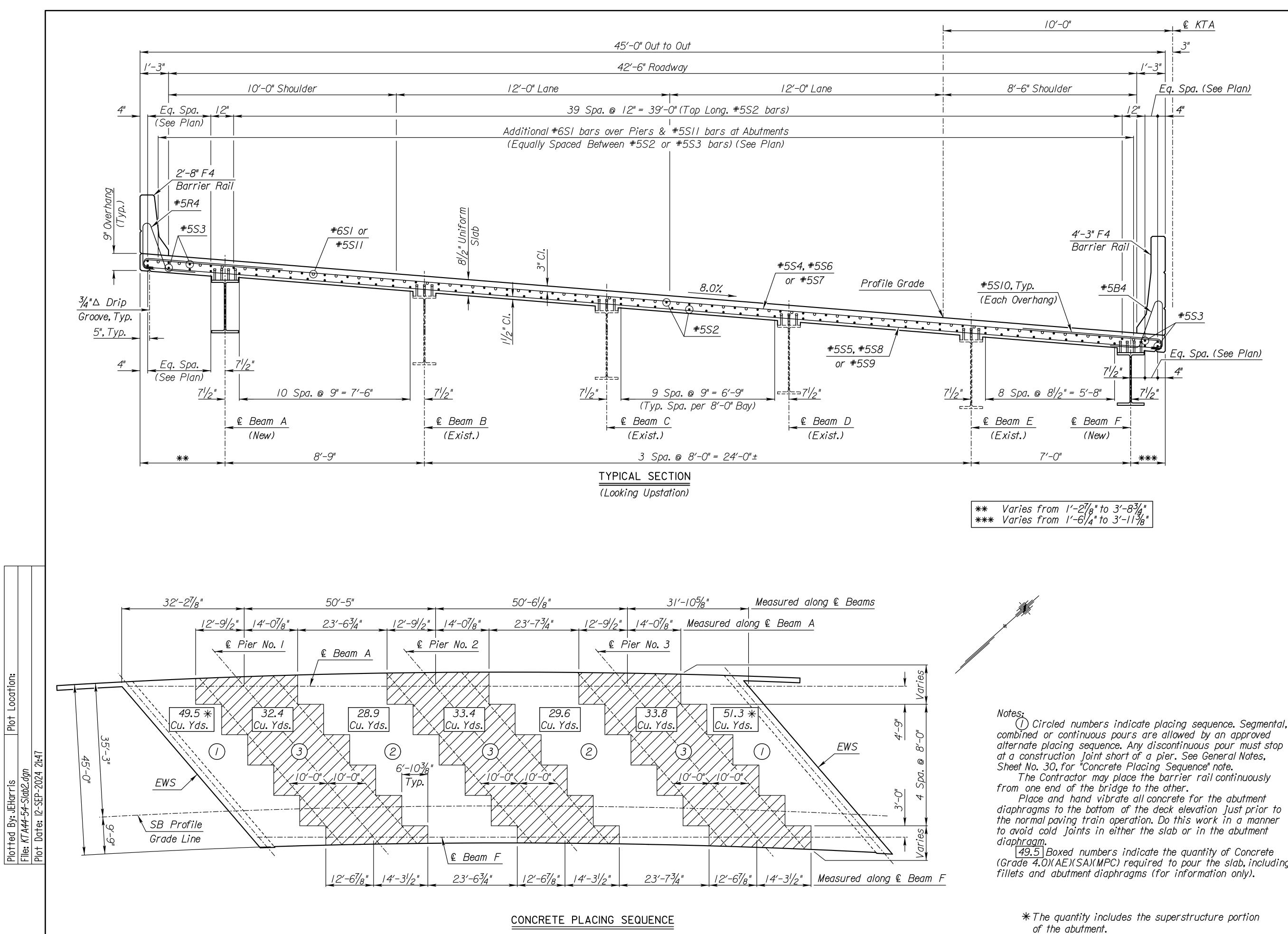
6. If all gaps refuse the 0.005" gage, and the turned element has been rotated more than 45° beyond the calibrated turn, reject the bolt.

For additional information see the structural steel section of the Bridge Construction Manual.

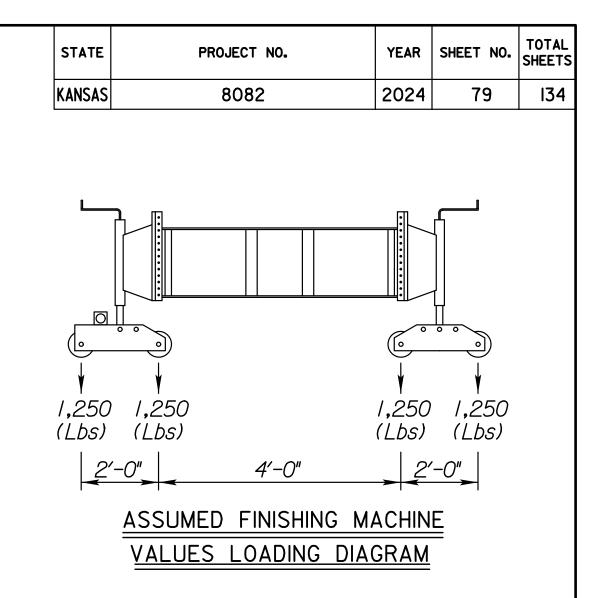
Suggested Impact wrench models: CP 611 IR 2940 Cleco WS2110 ATP 1011/1040 Norbar PT1500

4						
3						
2						
-	04/25/05	Current	Current Release			
NO.	DATE	REV	BY	APP'D		
KANSAS TURNPIKE AUTHORITY Br. No. 43.930 SB STEEL ERECTION, FIT-UP AND BOLTING PROCEDURE						
SHEET		SCALE	APP'D			
DESIGN						
DESIGN		DETAIL CK.	QUAN. CK.	CADD CK.		
			S	heet No.	77	



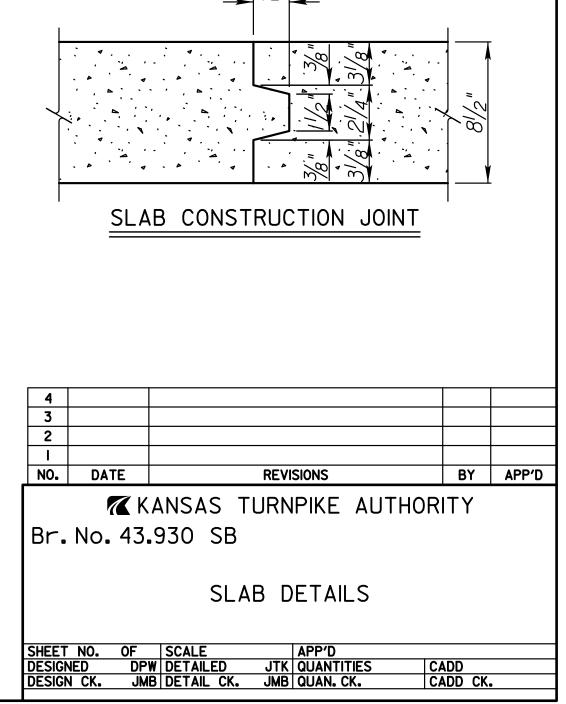


49.5 Boxed numbers indicate the quantity of Concrete (Grade 4.0)(AE)(SA)(MPC) required to pour the slab, including



Note: Rotation (maximum = 1°) in the exterior girder was calculated assuming screed wheel loads as shown and placed 3" beyond the outside of the deck. The maximum overhang bracket spacing was assumed at 4 ft. The actual screed loadings or bracket spacing will be reflected in the design calculations for a torsional analysis of the exterior girder and bracing. The design calculations shall bear the seal of a licensed Professional Engineer. Submit according to KDOT Specifications Section 700 for falsework and formwork.

Note: Provide temporary bracing at the top and bottom flanges of the exterior beams during paving operations for the deck. Place the bracing at three equal spaces between permanent diaphragms. The top flange bracing members shall be a  $\frac{1}{2}$ " Ø steel rod or greater (Min. Fy = 36 ksi). The bottom flange bracing members shall be a 4" x 4" timber post or greater. The temporary bracing and labor for installation is subsidiary to the bid item "Concrete (Grade 4.0)(AE)(SA)(MPC)". Details of proposed bracing shall be submitted with falsework plans.



				TOF	OF SLAB	ELEVATIONS				
	Tenth Point		Fascia (West)	Beam A	Beam B	Beam C	Beam D	Beam E	Beam F	Fascia (East)
€ Brg.	1.0	Station	4714+32.93	4714+33.87	4714+40.79	4714+47.18	4714+53.62	4714+60.12	4714+65.85	4714+67.94
Abut. No. /	7.0	Elevation	1296.50	1296.41	1295.70	1295.05	1294.40	1293.76	1293.20	1292.99
	1.1	Station	4714+35.79	4714+36.82	4714+43.76	4714+50.16	4714+56.62	4714+63.13	4714+68.87	4714+70.91
	/•/	Elevation	1296.51	1296.40	1295.69	1295.05	1294.40	1293.76	1293.19	1293.00
Ē	1.2	Station	4714+38.64	4714+39.78	4714+46.73	4714+53.14	4714+59.61	4714+66.14	4714+71.89	4714+73.87
	1.2	Elevation	1296.52	1296.40	1295.69	1295.05	1294.40	1293.76	1293.19	1293.00
Ē	1.3	Station	4714+41.49	4714+42.73	4714+49.70	4714+56.13	4714+62.61	4714+69.15	4714+74.91	4714+76.83
	1.0	Elevation	1296.53	1296.40	1295.69	1295.04	1294.40	1293.75	1293.19	1293.01
	1.4	Station	4714+44.35	4714+45.69	4714+52.67	4714+59.11	4714+65.61	4714+72.16	4714+77.93	4714+79.80
ONE	1.7	Elevation	1296.53	1296.39	1295.69	1295.04	1294.40	1293.75	1293.19	1293.02
0	1.5	Station	4714+47.20	4714+48.65	4714+55.64	4714+62.09	4714+68.60	4714+75.17	4714+80.96	4714+82.76
N4	1.5	Elevation	1296.54	1296.39	1295.68	1295.04	1294.40	1293.75	1293.19	1293.02
SPAN	1.6	Station	4714+50.05	4714+51.60	4714+58.61	4714+65.08	4714+71.60	4714+78.18	4714+83.98	4714+85.72
- ,	1.0	Elevation	1296.55	1296.39	1295.68	1295.04	1294.39	1293.75	1293.19	1293.03
ſ	1.7	Station	4714+52.90	4714+54.56	4714+61.58	4714+68.06	4714+74.60	4714+81.19	4714+87.00	4714+88.69
	1.1	Elevation	1296.56	1296.39	1295.68	1295.04	1294.39	1293.75	1293.19	1293.03
f	1.8	Station	4714+55.76	4714+57.52	4714+64.56	4714+71.05	4714+77.60	4714+84.20	4714+90.02	4714+91.65
	1.0	Elevation	1296.56	1296.38	1295.68	1295.03	1294.39	1293.75	1293.19	1293.04
f	10	Station	4714+58.61	4714+60.48	4714+67.53	4714+74.03	4714+80.59	4714+87.21	4714+93.05	4714+94.62
	1.9	Elevation	1296.57	1296.38	1295.68	1295.03	1294.39	1293.75	1293.19	1293.04
⊈ Pier	2.0	Station	4714+61.46	4714+63.43	4714+70.50	4714+77.02	4714+83.59	4714+90.22	4714+96.07	4714+97.58
No. /	2.0	Elevation	/296.58	1296.38	1295.68	1295.03	1294.39	1293.75	1293.19	/293.05
	0.1	Station	4714+66.29	4714+68.36	4714+75.45	4714+81.99	4714+88.59	4714+95.24	4715+01.10	4715+02.60
	2.1	Elevation		1296.38	1295.67	1295.03	1294.39	1293.75	1293.19	/293.05
Ē	0.0	Station	4714+71.12	4714+73.29	4714+80.41	4714+86.97	4714+93.58	4715+00.26	4715+06.14	4715+07.63
	2.2	Elevation		1296.37	1295.67	1295.03	1294.39	1293.75	1293.19	1293.06
-	0.2	Station	4714+75.95	4714+78.22	4714+85.36	4714+91.94	4714+98.58	4715+05.27	4715+11.18	4715+12.65
	2.3	Elevation		1296.37	1295.67	1295.03	1294.39	1293.75	1293.19	1293.07
-	0.4	Station	4714+80.78	4714+83.16	4714+90.31	4714+96.92	4715+03.58	4715+10.29	4715+16.21	4715+17.67
OMI	2.4	Elevation		1296.37	1295.67	1295.03	1294.39	1293.75	1293.20	1293.07
	0.5	Station	4714+85.61	4714+88.09	4714+95.27	4715+01.89	4715+08.57	4715+15.31	4715+21.25	4715+22.70
AN I	2.5	Elevation		1296.37	1295.67	1295.03	1294.39	1293.76	1293.20	1293.08
SPAN	0.0	Station	4714+90.44	4714+93.02	4715+00.22	4715+06.87	47/5+/3.57	4715+20.33	4715+26.29	4715+27.72
•,	2.6	Elevation		1296.37	1295.67	1295.03	1294.40	1293.76	1293.20	1293.08
-	0.7	Station	4714+95.27	4714+97.95	4715+05.18	4715+11.85	4715+18.57	4715+25.35	4715+31.32	4715+32.75
	2.7	Elevation		1296.37	1295.67	1295.03	1294.40	1293.76	1293.21	1293.09
ŀ	0.0	Station	47/5+00.10	4715+02.89	47/5+/0./4	4715+16.82	4715+23.57	4715+30.37	4715+36.36	4715+37.77
	2.8	Elevation		1296.37	1295.67	1295.04	1294.40	1293.77	1293.21	1293.09
-	0.0	Station	4715+04.93	47/5+07.82	4715+15.09	4715+21.80	4715+28.56	4715+35.38	47/5+4/.40	4715+42.79
	2.9	Elevation		1296.37	1295.68	1295.04	1294.40	1293.77	1293.22	1293.09
⊈ Pier	2.0	Station	47/5+09.76	4715+12.75	4715+20.05	4715+26.78	4715+33.56	47/5+40.40	47/5+46.44	4715+47.82
No. 2	3.0	Elevation		1296.38	1295.68	1295.04	1294.41	1293.78	1293.22	1293.10

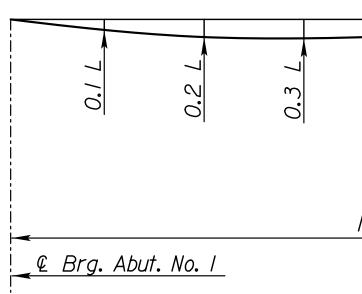
Plotted By: JEHarris Plot Location: File: KTA44-55-SlabElevations.dgn Plot Date: 12-SEP-2024 21:48

				TOF	OF SLAB	ELEVATIONS				
	Tenth Point		Fascia (West)	Beam A	Beam B	Beam C	Beam D	Beam E	Beam F	Fascia (East)
⊈ Pier	3.0	Station	4715+09.76	47/5+/2.75	4715+20.05	4715+26.78	4715+33.56	4715+40.40	4715+46.44	47/5+47.82
No. 2	0.0	Elevation	1296.66	1296.38	1295.68	1295.04	1294.41	1293.78	1293.22	1293.10
	3./	Station	4715+14.70	4715+17.70	4715+25.01	4715+31.76	4715+38.57	4715+45.43	4715+51.48	4715+52.97
	0.1	Elevation	1296.67	1296.38	1295.68	1295.05	1294.41	1293.78	1293.23	1293.10
	3.2	Station	4715+19.64	4715+22.64	4715+29.98	4715+36.75	4715+43.57	4715+50.46	4715+56.53	4715+58.12
	J.L	Elevation	1296.67	1296.38	1295.69	/295.05	1294.42	1293.79	1293.23	1293.10
	3.3	Station	4715+24.58	4715+27.58	4715+34.95	4715+41.74	4715+48.58	4715+55.48	4715+61.57	4715+63.27
	0.0	Elevation	1296.68	1296.38	1295.69	/295.06	1294.42	1293.79	1293.24	1293.10
FE	3.4	Station	4715+29.53	4715+32.53	4715+39.91	4715+46.72	4715+53.59	4715+60.51	4715+66.62	4715+68.42
THREE	J. 1	Elevation	1296.68	1296.39	/295.69	/295.06	1294.43	1293.80	1293.25	/293./0
	3.5	Station	4715+34.47	4715+37.47	4715+44.88	4715+51.71	4715+58.59	4715+65.54	4715+71.66	4715+73.57
4N	5.5	Elevation	1296.69	1296.39	1295.70	1295.07	1294.44	1293.81	/293.26	1293.10
SPAN	3.6	Station	4715+39.41	4715+42.41	4715+49.84	4715+56.69	4715+63.60	4715+70.56	4715+76.70	4715+78.72
,	0.0	Elevation	1296.69	1296.40	1295.71	1295.07	1294.44	1293.82	1293.27	1293.10
	3.7	Station	4715+44.36	4715+47.35	4715+54.81	4715+61.68	4715+68.60	4715+75.59	4715+81.75	4715+83.88
	J.1	Elevation	1296.69	1296.40	1295.71	/295.08	1294.45	1293.82	1293.27	1293.10
	3.8	Station	4715+49.30	4715+52.30	4715+59.77	4715+66.66	4715+73.61	4715+80.61	4715+86.79	4715+89.03
	5.0	Elevation	1296.70	1296.41	1295.72	1295.09	1294.46	/293.83	1293.28	1293.09
	3.9	Station	4715+54.24	4715+57.24	4715+64.73	4715+71.65	4715+78.61	4715+85.64	4715+91.83	4715+94.18
	5.5	Elevation	1296.70	1296.42	1295.73	1295.10	1294.47	1293.84	1293.29	1293.09
€ Pier	4.0	Station	47/5+59./8	47/5+62./8	4715+69.70	47/5+76.63	4715+83.62	4715+90.66	47/5+96.87	4715+99.33
No. 3	7.0	Elevation	1296.70	1296.42	1295.73	1295.11	1294.48	/293.85	1293.30	1293.09
	4.1	Station	4715+62.17	4715+65.11	4715+72.64	4715+79.58	4715+86.58	4715+93.63	4715+99.85	4716+02.44
	7.1	Elevation	1296.70	1296.43	1295.74	1295.11	1294.48	1293.86	1293.31	1293.09
	4.2	Station	47/5+65./5	4715+68.04	4715+75.58	4715+82.53	4715+89.54	4715+96.61	4716+02.84	4716+05.55
	7.2	Elevation	1296.70	1296.43	1295.74	1295.12	1294.49	1293.86	1293.32	1293.08
	4.3	Station	4715+68.13	4715+70.96	4715+78.52	4715+85.48	4715+92.50	4715+99.58	4716+05.82	4716+08.67
	7.J	Elevation	1296.70	1296.44	1295.75	1295.12	1294.50	1293.87	1293.32	1293.08
9-	4.4	Station	4715+71.11	4715+73.89	4715+81.46	4715+88.43	4715+95.47	4716+02.56	4716+08.81	4716+11.78
100	<b>7.7</b>	Elevation	1296.70	1296.44	1295.75	1295.13	1294.50	1293.88	1293.33	1293.08
	4.5	Station	4715+74.09	4715+76.81	4715+84.39	4715+91.38	4715+98.43	4716+05.53	4716+11.79	47/6+/4.89
4/	7.5	Elevation	1296.70	1296.45	1295.76	1295.13	1294.51	1293.88	1293.34	1293.08
SPAN	4.6	Station	4715+77.07	4715+79.74	4715+87.33	4715+94.33	4716+01.39	4716+08.50	47/6+/4.77	4716+18.00
-,	7.0	Elevation	1296.70	1296.45	1295.77	1295.14	1294.52	1293.89	1293.35	1293.07
l T	4.7	Station	4715+80.05	4715+82.67	4715+90.27	4715+97.28	4716+04.35	4716+11.47	4716+17.76	4716+21.11
	7.1	Elevation	1296.70	1296.46	1295.77	1295.15	1294.52	1293.90	/293.35	1293.07
l ľ	4.8	Station	4715+83.04	4715+85.59	4715+93.21	4716+00.23	4716+07.31	4716+14.45	4716+20.74	4716+24.23
	7.0	Elevation	1296.70	1296.46	1295.78	1295.15	1294.53	1293.91	1293.36	1293.07
l f	4.9	Station	4715+86.02	4715+88.52	4715+96.15	4716+03.18	4716+10.27	4716+17.42	4716+23.72	4716+27.34
	イ・フ	Elevation	1296.70	1296.47	1295.78	1295.16	1294.54	1293.91	1293.37	1293.06
€ Brg.	5.0	Station	4715+89.00	4715+91.44	4715+99.08	4716+06.13	4716+13.23	4716+20.39	4716+26.70	4716+30.45
Abut. No. 2	5.0	Elevation		1296.47	1295.79	1295.17	1294.54	1293.92	1293.38	1293.06

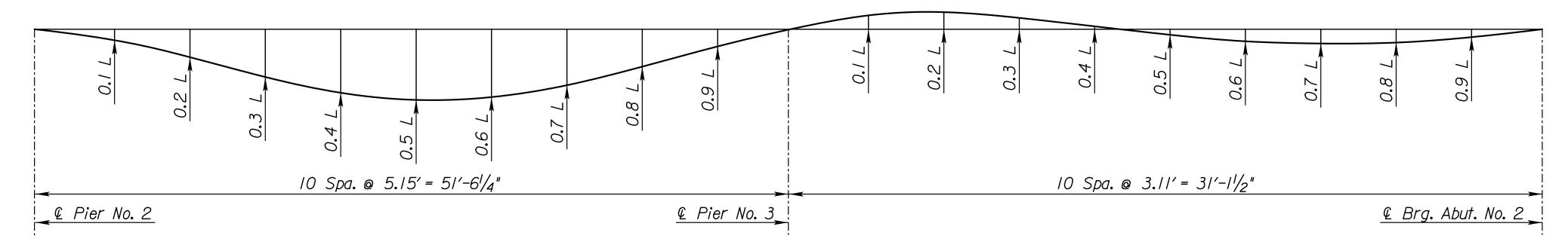
STATE	PROJECT NO.	YEAR	SHEET NO.	TOTAL SHEETS	
KANSA	8082	2024	80	134	
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4						
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NO.	DATE		REVISIO	NS	BY	APP'D
	No. 43 ROA	ANSAS T 930 SB DWAY SL				
SHEET		SCALE		P'D		
DESIGN				JANTITIES	ADD	
DESIGN	NCK. JM	B DETAIL CK.	JWM QL	JAN. CK.	ADD CK.	

									DEA	D LOAD	DEFLECT	IONS									
Beam	€ Brg. Abut. No. I	0.1 L	0.2 L	0.3 L	0.4 L	0.5 L	0.6 L	0.7 L	0.8 L	0.9 L	© Pier No. I	0.1 L	0.2 L	0.3 L	0.4 L	0.5 L	0.6 L	0.7 L	0.8 L	0.9 L	© Pier No. 2
A	0.000	-0.00/	-0.001	-0.00/	-0.001	-0.00/	0.000	0.00/	0.00/	0.00/	0.000	-0.004	-0.009	-0.0/3	-0.016	-0.0/7	-0.0/5	-0.012	-0.007	-0.002	0.000
В	0.000	-0.00/	-0.00/	-0.00/	-0.00/	-0.00/	0.000	0.000	0.00/	0.00/	0.000	-0.002	-0.006	-0.009	-0.0//	-0.0//	-0.0/0	-0.007	-0.004	-0.00/	0.000
С	0.000	-0.00/	-0.00/	-0.00/	-0.00/	-0.00/	0.000	0.000	0.000	0.000	0.000	-0.002	-0.005	-0.008	-0.0/0	-0.0//	-0.009	-0.007	-0.004	-0.00/	0.000
D	0.000	-0.00/	-0.00/	-0.00/	-0.00/	-0.00/	0.000	0.000	0.000	0.00/	0.000	-0.002	-0.005	-0.008	-0.0/0	-0.0//	-0.009	-0.007	-0.004	-0.00/	0.000
Ε	0.000	-0.00/	-0.00/	-0.00/	-0.00/	-0.00/	0.000	0.000	0.000	0.00/	0.000	-0.002	-0.005	-0.008	-0.0/0	-0.0/0	-0.009	-0.007	-0.004	-0.00/	0.000
F	0.000	-0.00/	-0.00/	-0.002	-0.002	-0.00/	-0.00/	0.000	0.000	0.001	0.000	-0.003	-0.006	-0.0/0	-0.0/2	-0.0/3	-0.0//	-0.008	-0.005	-0.00/	0.000
		0.1 L	0.2 L	0.3 L	0.4 L	0.5 L	0.6 L	0.7 L	0.8 L	0.9 L		0.1 L	0.2 L	0.3 L	0.4 L	0.5 L	0.6 L	0.7 7	0.8 L	7 6.0	
		0.1 L	0.2 L	0.	1 <del>7</del>		I	0.7 L	0.8 L	0.9 L		0.1 L		0.3 L	0	- - - - - - - - - - - - - - - - - - -	I	0.7 4	0.8 L	7 6.0	



									DEA	D LOAD	DEFLECT	IONS									
Beam	© Pier No. 2	0.1 L	0.2 L	0.3 L	0.4 L	0.5 L	0.6 L	0.7 L	0.8 L	0.9 L	⊈ Pier No. 3	0.1 L	0.2 L	0.3 L	0.4 L	0.5 L	0.6 L	0.7 L	0.8 L	0.9 L	€ Brg. Abut. No. 2
A	0.000	-0.002	-0.007	-0.0/3	-0.017	-0.018	-0.0/8	-0.0/4	-0.009	-0.004	0.000	0.001	0.00/	0.00/	0.000	-0.00/	-0.00/	-0.00/	-0.00/	-0.00/	0.000
В	0.000	-0.00/	-0.004	-0.008	-0.0/0	-0.0//	-0.0//	-0.009	-0.006	-0.003	0.000	0.00/	0.00/	0.000	0.000	-0.00/	-0.00/	-0.00/	-0.00/	0.000	0.000
С	0.000	-0.00/	-0.004	-0.007	-0.0/0	-0.0//	-0.0/0	-0.009	-0.006	-0.003	0.000	0.00/	0.00/	0.000	0.000	-0.00/	-0.00/	-0.00/	-0.00/	0.000	0.000
D	0.000	-0.00/	-0.004	-0.007	-0.0/0	-0.0//	-0.0/0	-0.009	-0.006	-0.003	0.000	0.00/	0.001	0.000	0.000	-0.00/	-0.00/	-0.00/	-0.00/	0.000	0.000
E	0.000	-0.00/	-0.004	-0.007	-0.009	-0.0/0	-0.0/0	-0.008	-0.005	-0.002	0.000	0.00/	0.00/	0.000	0.000	-0.00/	-0.00/	-0.00/	-0.00/	0.000	0.000
F	0.000	-0.002	-0.006	-0.0/0	-0.0/3	-0.014	-0.0/3	-0.0//	-0.007	-0.003	0.000	0.001	0.000	0.000	-0.00/	-0.00/	-0.002	-0.002	-0.00/	-0.00/	0.000



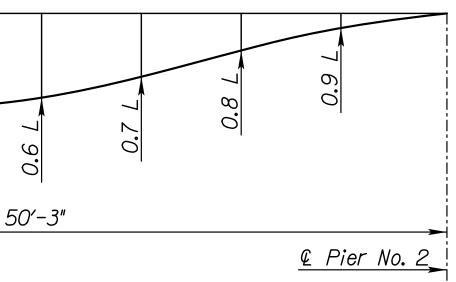
Plotted By: JEHarris	Plot Location:
File: KT A44-56-Deflections.dgn	
Plot Date: 12-SEP-2024 21:48	

# BEAM DEAD LOAD DEFLECTION DIAGRAM

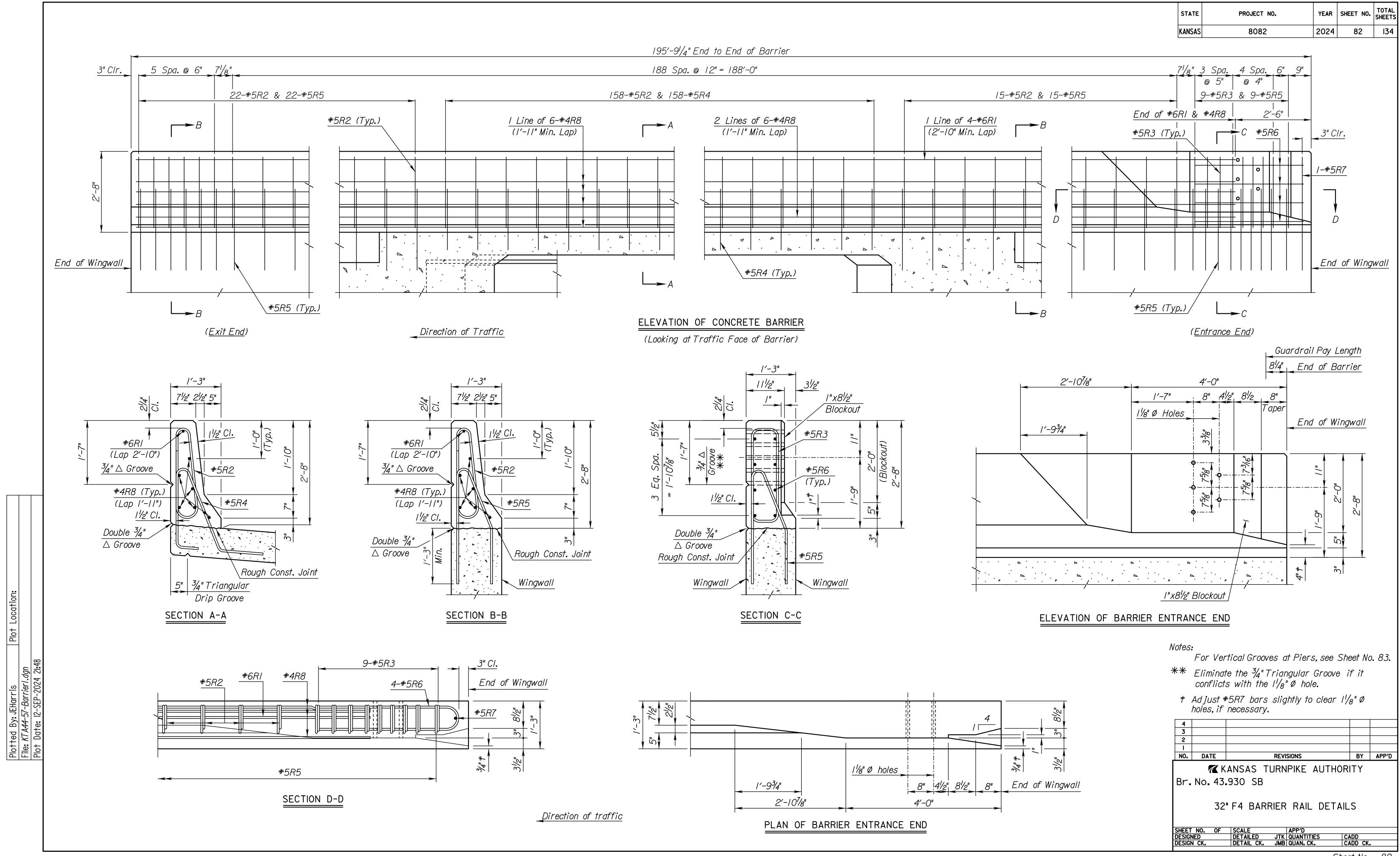
Ordinates are in feet and are at tenth points of spans, measured along & Beams.

DEFLECTION NOTES: Do not camber the new steel beams. Any natural mill camber that the beams have retained shall be placed up. Dead Load Deflection ordinates shown represent the amount of deflection due to the slab pour and barrier rails. Provide for beam deflections by adding concrete dead load deflections to plan grade. Increase or decrease the depth of concrete fillets over the beams, based on field surveys, to obtain the required roadway surface elevations.

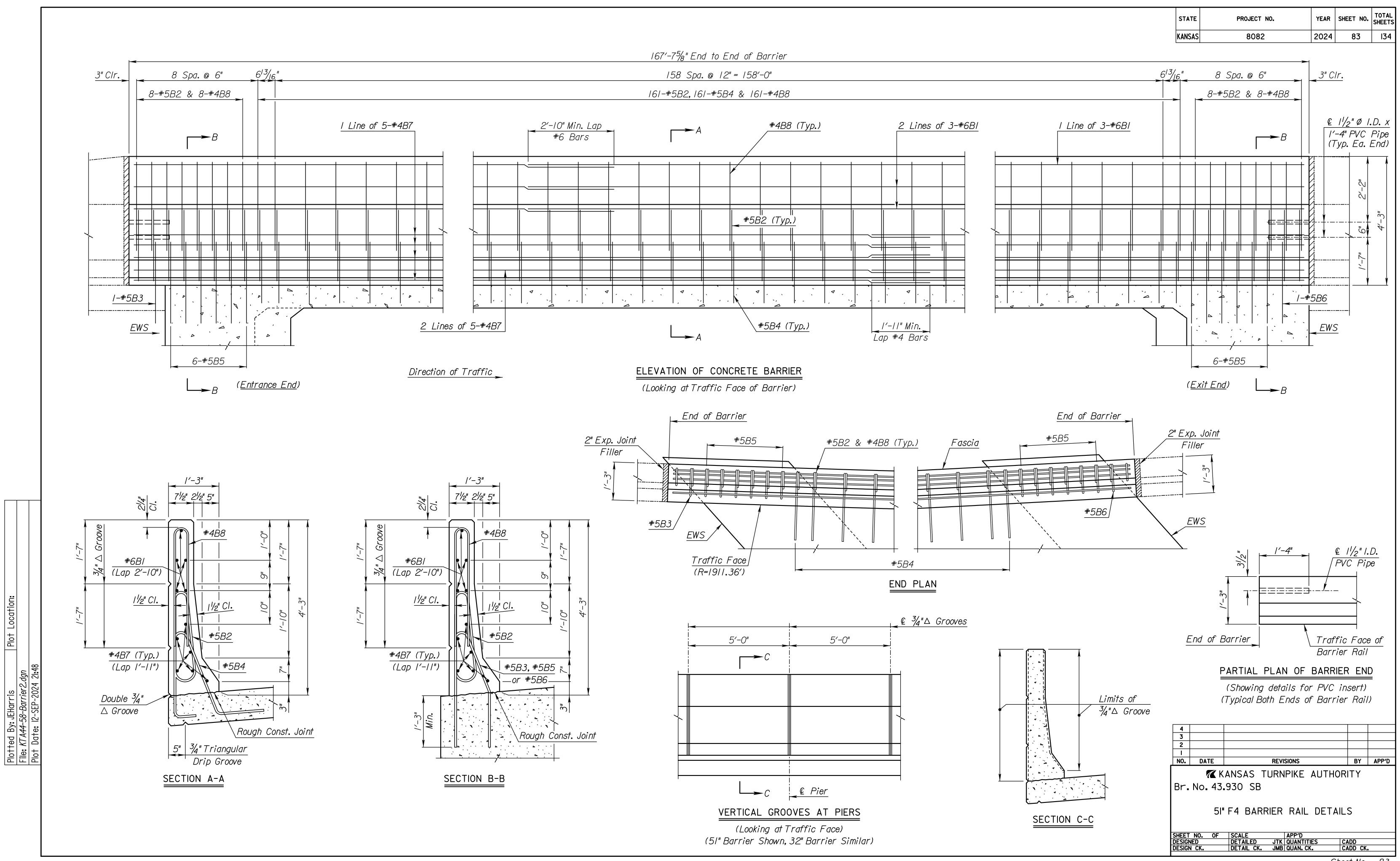
STATE	PROJECT NO.	YEAR	SHEET NO.	TOTAL SHEETS
KANSAS	8082	2024	81	134



4						
3						
2						
NO.	DATE		REVI	SIONS	BY	APP'D
	No. 43	.930 S	SB	PIKE AUTHO		
SHEET		SCALE		APP'D		
DESIGN						
DESIGN	N CK. SH	IH   DETAIL	CK. JWM	QUAN. CK.	CADD CK	•

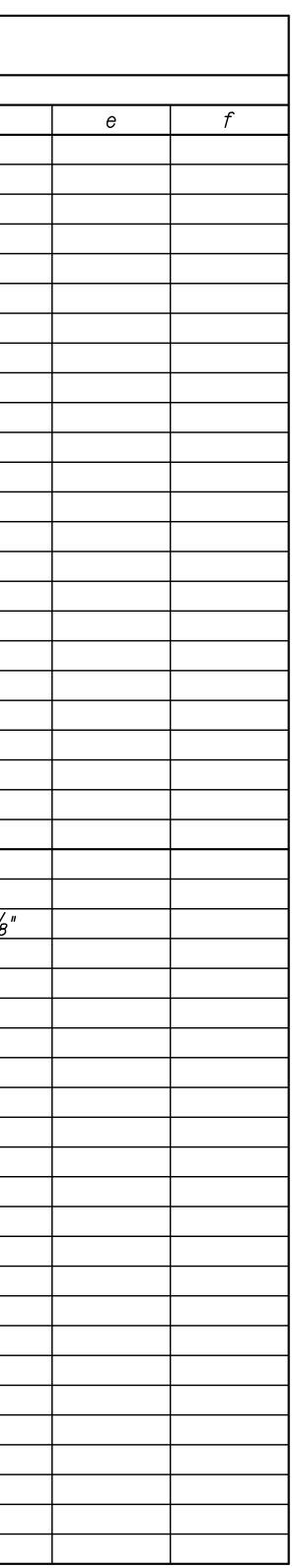


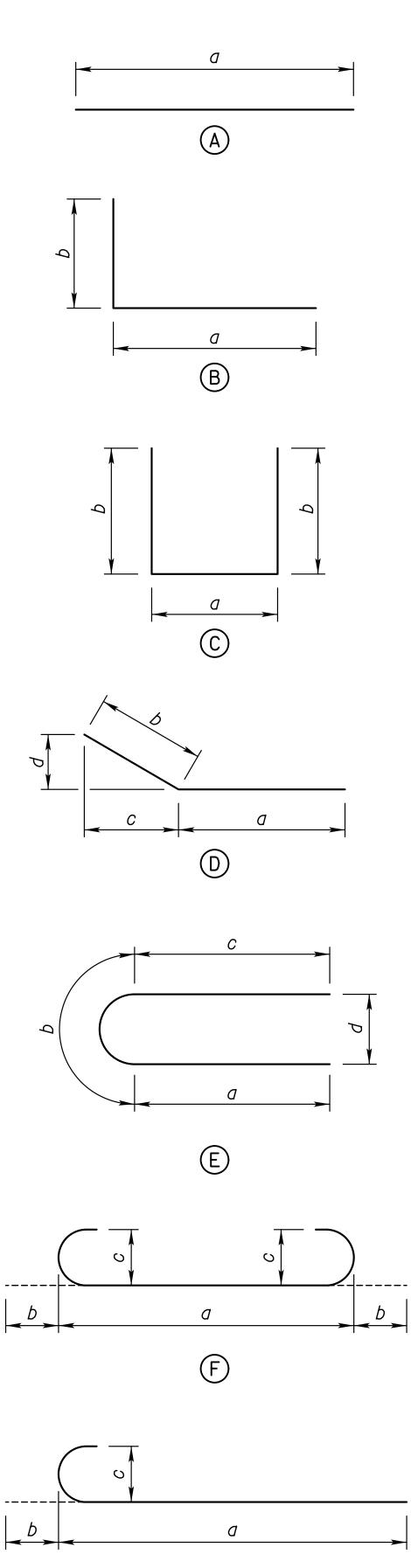
Sheet No. 82



Sheet No. 83

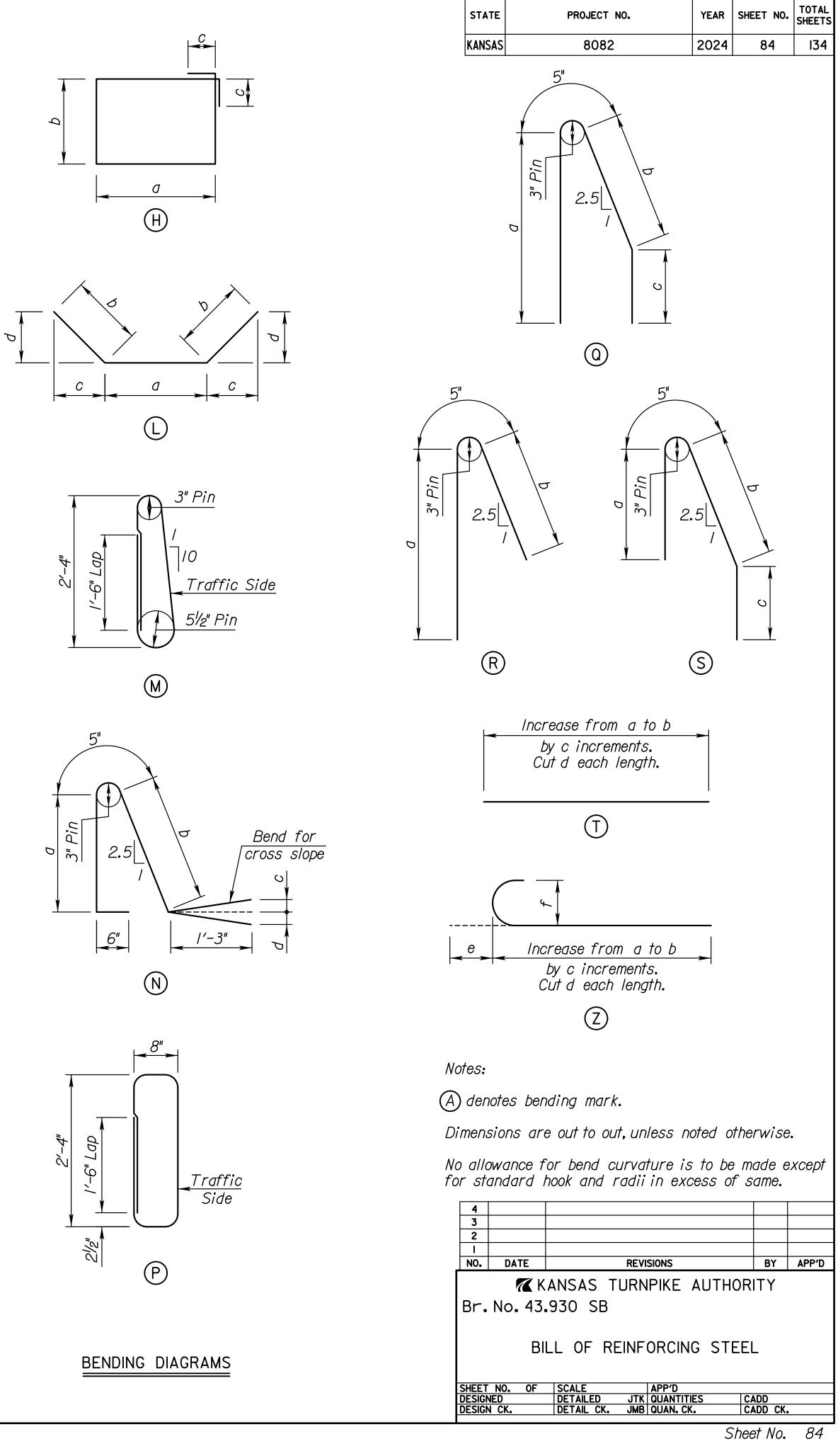
					BILL		NFORCING DE 60	STEEL	
ľ	Design	Bending						Dime	nsion
	Mark	Mark	Size	No.	Length	а	b	С	đ
	SAI	A	8	8	57′-0"	57'-0"			
	SA27	A	7	//	///-8"	//′-8"			
	SA3	A	5	6	57'-0"	57'-0"			
	SA4	A	5	2	39′-6″	39′-6″			
- -	SA5	A	5	2	28'-10"	28'-10"			
5 S	SA6	A	5	2	/8'-2"	18'-2"			
	SA7	A	5	4	7′-6″	7'-6"			
	SA/3	C	5	10	/8′-6″	3'-6"	7'-6"	7′-6″	
	SA/4	С	5	8	20'-0"	3′-6″	8'-3"	8′-3″	
-	SA/5	C	5	8	21'-4"	3'-6"	8'-//"	8'-//"	
	SAI6	C	5	8	22'-6"	3'-6"	9'-6"	9'-6"	
	SAI7	C	5	9	24'-0"	3'-6"	10'-3"	/0′-3″	
	SA/8	C	5	2	/4'-5"	3'-6"	6'-//"	4'-0"	
	SA/9	С	5	/	/5′-8″	3'-6"	7′-6″	4'-8"	
	SA20	С	5	/	16'-11"	3'-6"	8'-/"	5'-4"	
۲	SA2I	С	5	2	/8′-4"	3′-6″	8'-10"	6'-0"	
	SA22	C	5	49	5'-2"	3'-6"	10"	10"	
	SA29	A	5	9	9′-9″	9′-9″			
	SA30	A	5		11'-2"	11'-2"			
	SA31	A	5	9	/0′-3″	10'-3"			
	NA/	A	8	16	33'-/"	33′-/"			
	NA27	D	7	//	6′-9″	4'-0"	2'-9"	2'-7"	//3
	ΝΑΖΙ		/	11	0-9	4-0	2-9		117
	NA3	A	5	12	32'-2"	32'-2"			
	NA4	A	5	2	4/′-7"	41′-7″			
	NA5	A	5	2	30'-11"	30'-//"			
Ę	NA6	A	5	2	20'-3"	20'-3"			
A つつ	NA7	A	5	4	9′-7″	9′-7″			
-	NA/3	С	5	12	/8′-4"	3′-6"	7′-5″	7′-5″	
	NA/4	С	5	8	/9′-/0″	3′-6"	8'-2"	8'-2"	
	NA/5	С	5	8	21'-2"	3′-6″	8'-10"	8'-10"	
J	NA/6	С	5	8	22'-6"	3′-6″	9′-6″	9′-6″	
	NAI7	С	5	12	24'-2"	3′-6"	10′-4″	10'-4"	
-	NAI8	С	5	2	4'-5"	3′-6"	6'-11"	4'-0"	
	NAI9	С	5	1	/5′-8″	3′-6"	7′-6″	4′-8″	
	NA20	С	5	/	/6′-//″	3′-6"	8'-/"	5′-4″	
	NA2I	С	5	2	18'-4"	3′-6″	8'-10"	6'-0"	
Ŧ	NA22	С	5	54	5'-2"	3′-6″	10"	10"	
	NA29	A	5	9	9′-8″	9′-8″			
	NA30	A	5	11	/'-4"	//′-4″			
	NA31	A	5	4	10'-4"	/0′-4″			

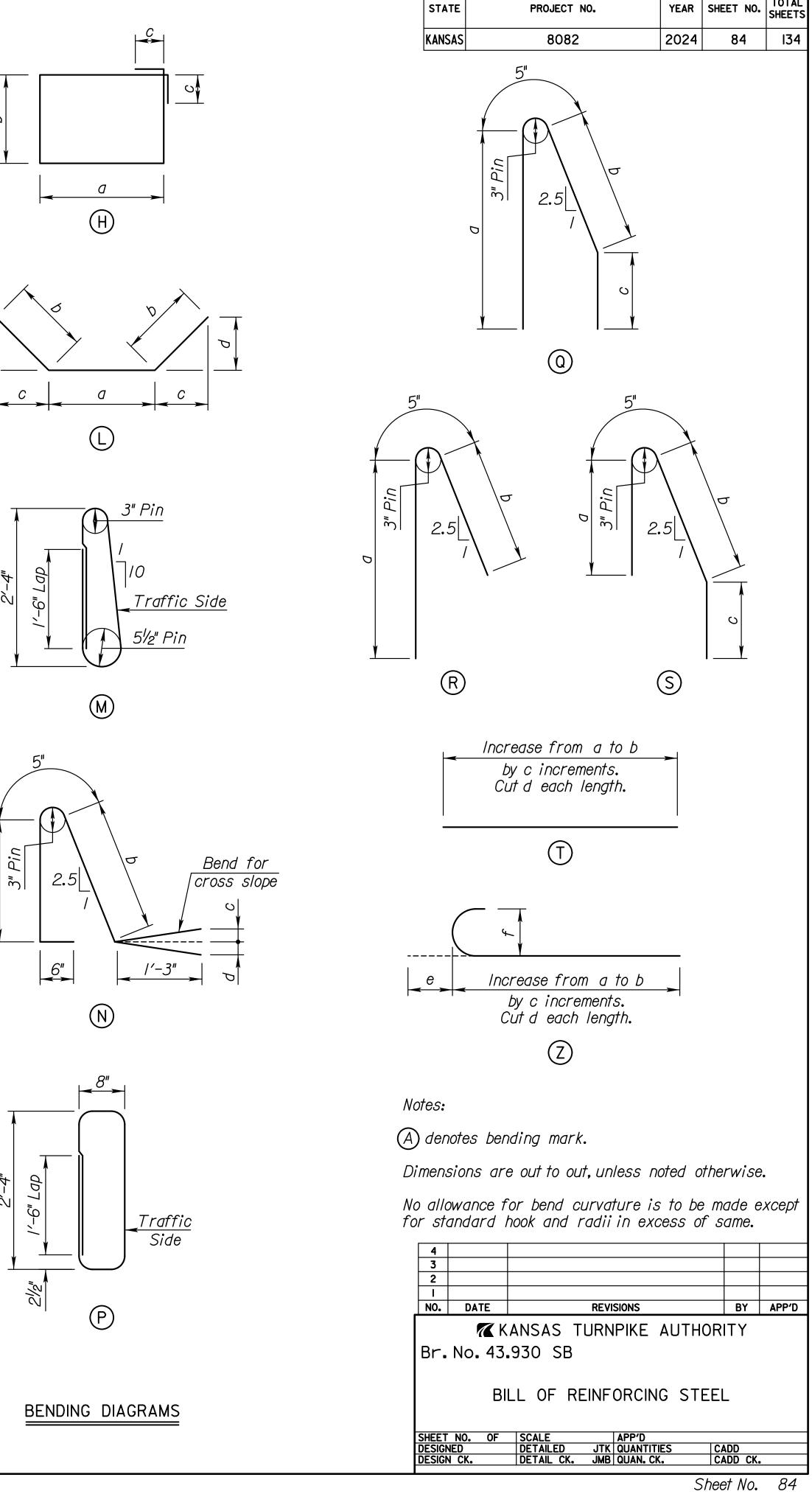


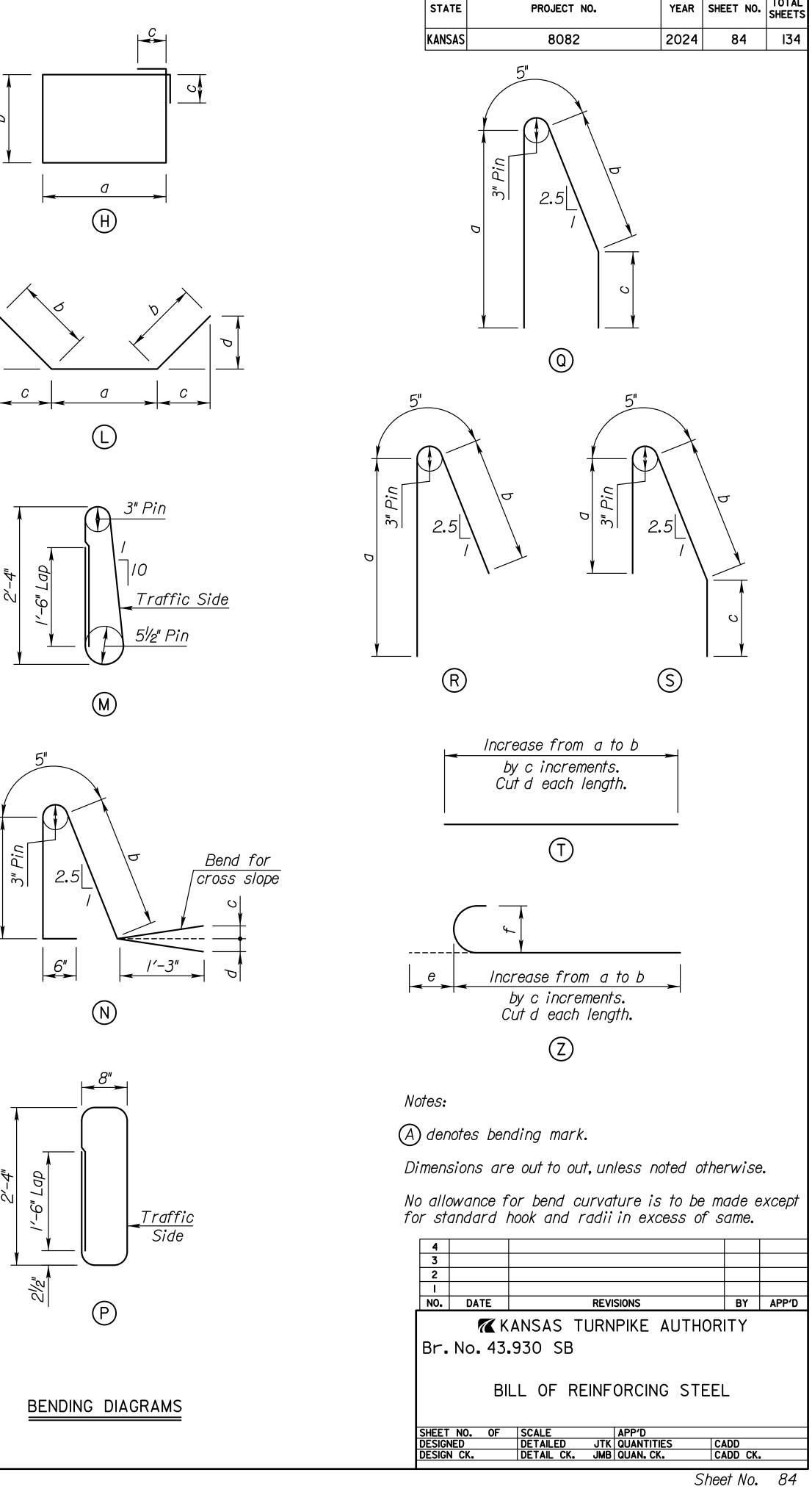


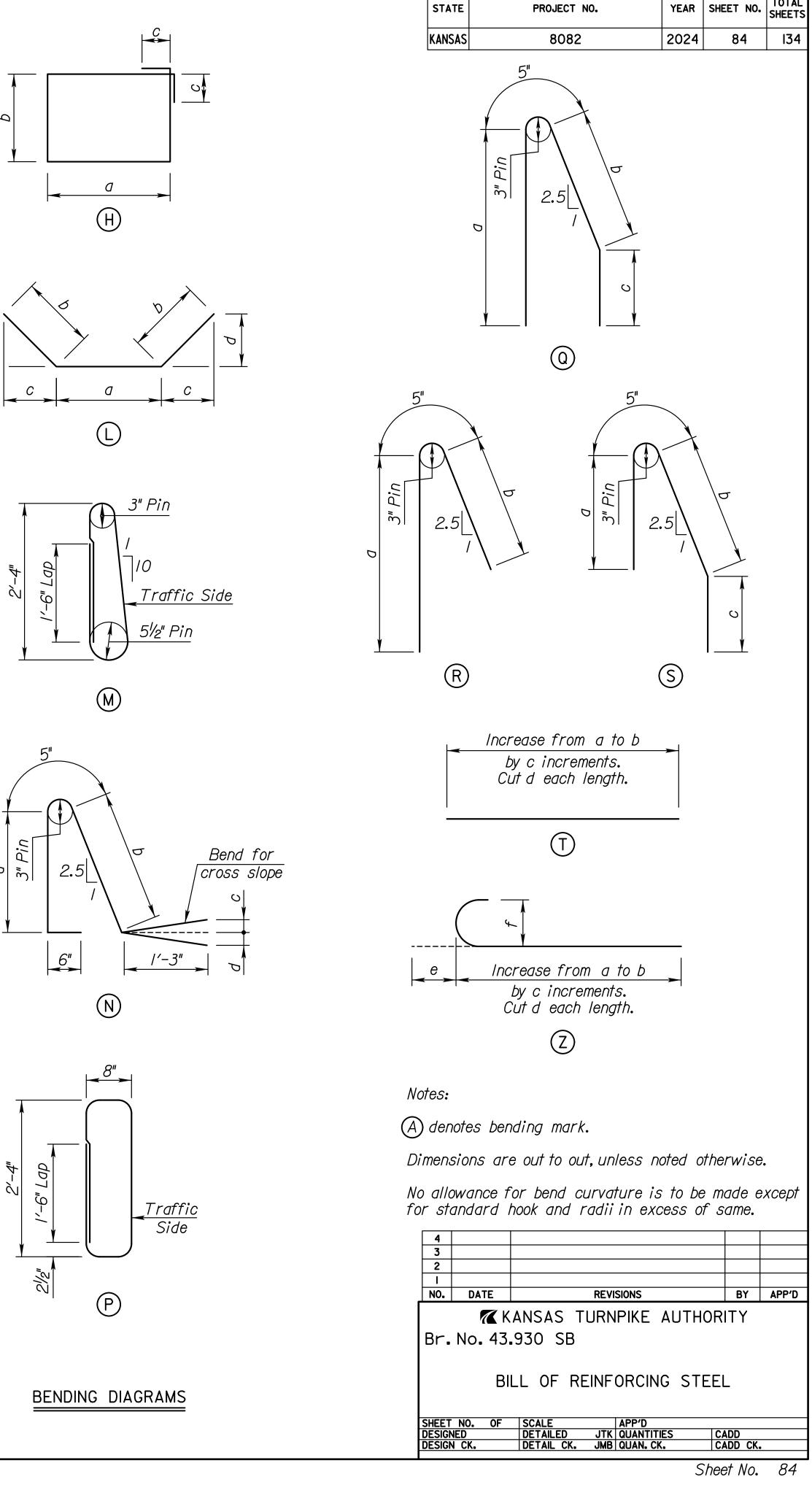
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	BILL OF REINFORCING STEEL GRADE 60 Design Bending												
Γ	Design	Bending						Dimer	nsion				
$\bot$	Mark	Mark	Size	No.	Length	а	Ь	С	d	е	f		
	PBI	F	8	4	11′-6″	9′-8″	//"	//"					
	PB2	A	8	4	9′-8″	9′-8″							
	PB3	F	8	4	9′-6″	7′-8″	//"	//"					
╞	PB4	A	8	4	7′-8"	7′-8″							
₅⊦						24 01							
	PDI	A	6	12	3'-0"	3'-0"							
5	PB5	С	5	38	9′-0″	2'-2"	3′-5″	3′-5″					
	1 00		5	50	9-0	2-2	<u> </u>	<u> </u>					
ᆉ	PB6	A	4	8	9′-8″	9′-8″							
	PB7	A	4	6	7′-8″	7′-8″							
	PB8	C	4	/4	4'-6"	2'-0"	/′-3″	/′-3″					
	. 20		,										
- -													
F													
F													
ſ													
Ī	PBI	F	8	4	//′-6″	9′-8″	//"	//"					
	PB2	A	8	4	9′-8″	9′-8″							
	PB3	F	8	4	9′-6″	7′-8"	//"	//"					
	PB4	A	8	4	7′-8"	7′-8″							
╗┝													
ᆈ	PDI	A	6	20	3'-0"	3'-0"							
A   D	PFI	A	6	6	9'-2"	9'-2"							
	PF2	A	6	6	8′-7"	8′-7"							
		<u> </u>	5	20			31 51	31 51					
∨	PB5	С	5	38	9′-0″	2'-2"	3′-5″	3′-5″					
	PB6	A	4	8	9′-8″	9′-8″							
	PB7	A	4	6	7′-8″	7′-8″							
┋┝	PB8	C	4	14	4'-6"	/ 0 2'-0"	/′-3"	/′-3″					
┢	PF3	H	4	19	///-/"	3'-2"	2'-0"	41/2"					
F	PF4	C	4	6	5′-7″	3'-/"	 /′-3"	/′−3″					
F													
_													
T	PBI	F	8	4	//′-6″	9′-8″	//"	//"					
	PB2	A	8	4	9′-8″	9′-8″							
	PB3	F	8	4	9′-6″	7′-8″	//"	//"					
	PB4	A	8	4	7′-8″	7′-8″							
5													
	PDI	A	6	12	3'-0"	3'-0"							
A V	~~~					04 0"	<u> </u>	2/ 5"					
붉	PB5	С	5	38	9′-0″	2'-2"	3′-5″	3′-5″					
			Λ	0									
າ •	PB6	A	4	8 6	9′-8" 7′-8"	9'-8" 7'-8"							
	PB7 PB8	A C	4	6 14	/ -8 4′-6"	7'-8" 2'-0"	/′-3″	/′-3″					
╘┞	00 ו		7	14	J - U		1 - 5						
┢													
┢													
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F													

Plot Location: Plotted By: JEHarris File: *KTA44-60-Barlist2.dgn* Plot Date: 12-SEP-2024 21:49

				BILL	OF REIN	NFORCING	STEEL				KANSAS	8082	2024	SHEET NO. 85	+
						DE 60									
esign E Mark	Bending Mark		No	Longth		L	Dimer								
		Size	No.	Length	a 57/ /"	Ď	С	d	e	f					
5A2 VA2	A A	<u>8</u> 8	5 10	57'-1" 33'-2"	57'-1" 33'-2"										
		0	10	55 2	Z										
A25	A	7	6	3'-9"	3′-9"										
A26	A	7	4	16'-2"	16'-2"										
A25	A	7	6	13'-2"	13'-2"										
A26	D	7	5	8'-//"	6'-2"	2'-9"	2′-7"	<sup>3</sup> /8"							
BI	A	6	15	57′-10″	57′-10″										
RI	A	6	4	50'-5"	50′-5″										
SI	A	6	131	20'-0"	20'-0"										
B2	M	5	177	6'-6"	6'-6"	1/ 7/				<u> </u>					
B3 B4	R N	5 5	  6	4′-3″ 5′-11″	2′-7"  ′-9"	/'-3" 2'-0"				<u> </u>					
B4 B5	 	5 5	161	5'-11" 5'-9"	2'-7"	2'-0" 1'-6"	//4"  '-3"								
B6	S	5	/		/′-/″	/ 6	/'-3"								
R2	M	5	/95	6'-6"											
R3	Р	5	9	7′-6"											
R4	N	5	157	5'-11"	/'-9"	2'-0"		11/4"							
R5 PC	Q E	5	46	5'-9" 7'-5"	2'-7" 3'_ 33/."	//-6"	/'-3" 3'_33'."	<u>c</u> 1/ "							
R6 R7	<u>Е</u> А	5 5	4	7′-5″ 3′-10″	3'-3 <sup>3</sup> /4" 3'-10"	9 <sup>1</sup> /2"	3′-3 <sup>3</sup> ⁄4″	6 <sup>1</sup> /2"		<u> </u>					
π/ S2	A	5	270	56'-6"	56′-6″					<u> </u>					
S3	A	5	54	43'-0"	43'-0"										
S4	F	5	247	45'-10"	44′-8"	7"	5"								
S5	Α	5	248	44′-8"	44′-8"										
S6	Ζ	5	68	VARIES	2'-9"	44'-8"	71/2"	/	7"	5"					
S7	$\frac{Z}{\tau}$	5	80	VARIES	2'-4"	44'-4"	6 <del>%</del> "	/	7"	5"					
S8 S9	/ 	5 5	68 80	VARIES VARIES	2'-5" 2'-0"	44'-4" 44'-0"	7 <sup>1</sup> /2" 6 <sup>3</sup> /8"	/ /		<u> </u>					
59 510	, D	5	635	6'-10"	2-0 6'-3"	7"	5"	1		<u> </u>					
S//	B	5	85	/8′-0″	16'-0"	2'-0"	-		1						
5A8	А	5	6	57′-/″	57′-/″										
SA9	A	5	2	42'-0"	42'-0"										
AIO	A	5	2	7'- "	7'- "					ļ					
A//	A	5 5	6	2'-5" 9'-8"	2'-5" 9'-8"										
AI2 A23	A C	5 5	2 43	9'-8" 9'-6"	<u> </u>	3'-0"	3'-0"								
A23 A24	B	5	6	7'-4"	3′-6"	3'-10"									
A28	A	5	5	/9′-9″	/9′-9″										
4 <i>32</i>	Α	5	22	3′-4"	3′-4"										
1A8	A	5	12	32'-3"	32'-3"										
1A9	A	5	2	43'-0"	43'-0"				-						
A/O A//	A A	5 5	2	/9′-2" /2′-5"	<i> 9'-2"</i> <i> 2'-5</i> "					<u> </u>					
AI2	A	5	2	12-5	11'-10"					<u> </u>					
A23	C	5	48	9'-6"	3′-6″	3'-0"	3'-0"								
A24	В	5	6	7'-4"	3′-6"	3′-10″									
A28	A	5	5	/9′-4″	/9′-4″										
A32	A	5	20	3′-6″	3′-6"					<u> </u>	4 3				╞
B7	A	4	30	35′-1″	35′-1″					<u> </u>	2				f
B8	E A	4	177	6'-1"	2'-9"	7"	2'-9"	4 <sup>1</sup> /2"			NO. DATE			BY	
R8	A	4	36	33'-10"	33'-10"			-12				KANSAS TURNPI 3.930 SB	KE AUTHC	DRITY	
									I	<u> </u>		BILL OF REINFOF	RCING STE	EL	
											I I				